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HUGO GERNSBACK, Editor-in-chief

test FM Stereo
ultiplex Schematics

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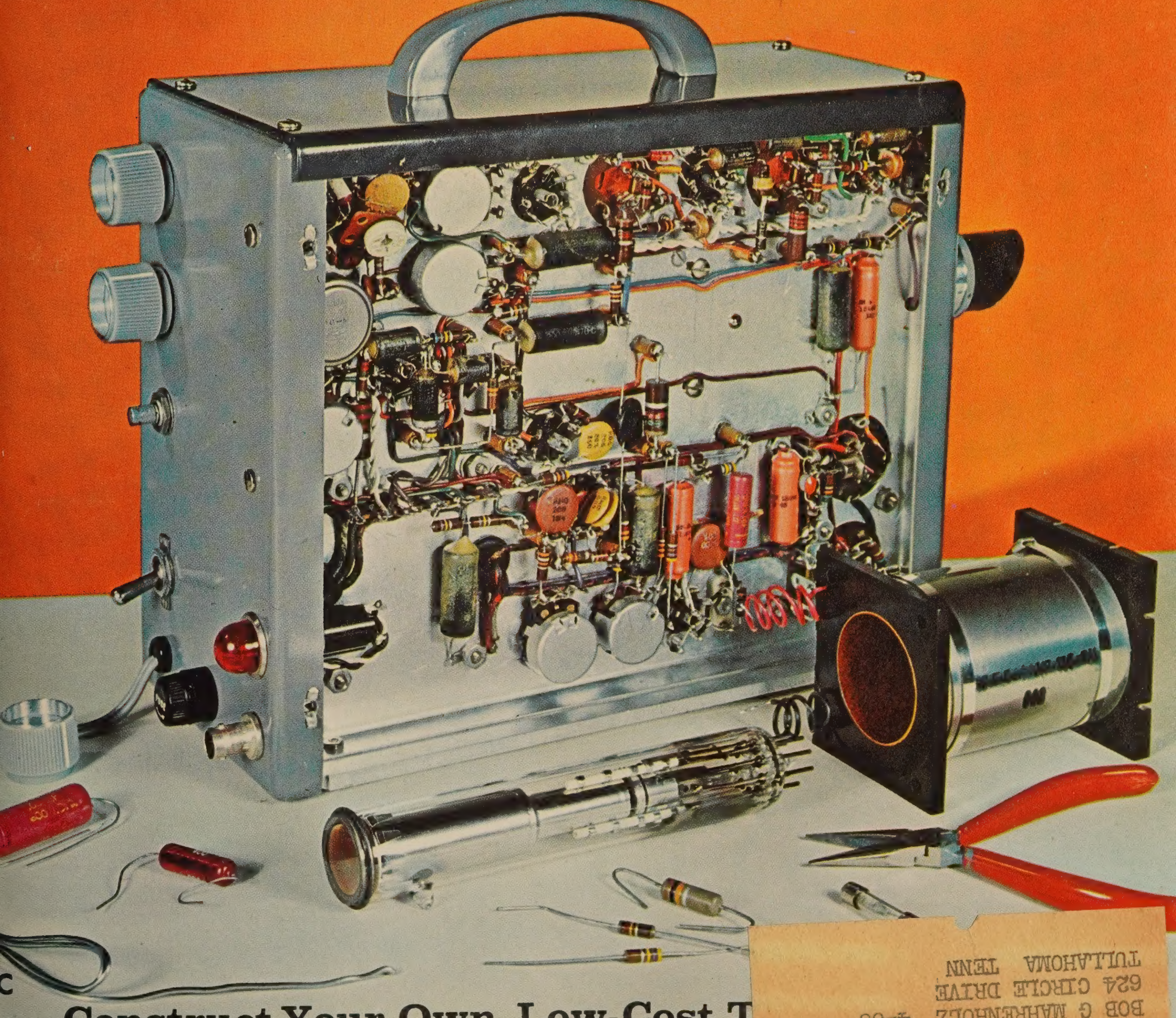
cket Service Kit

Useful Service Technique—
High-Voltage Substitution

Should I Build a Kit
Or Build from Scratch?



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Construct Your Own Low-Cost T

BOB G MAHRENHOLZ 4-66
624 CIRCLE DRIVE
TULLAHOMA TENN

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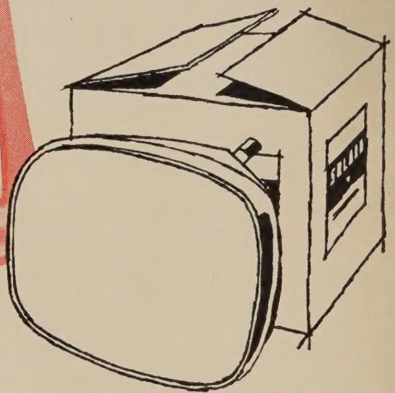

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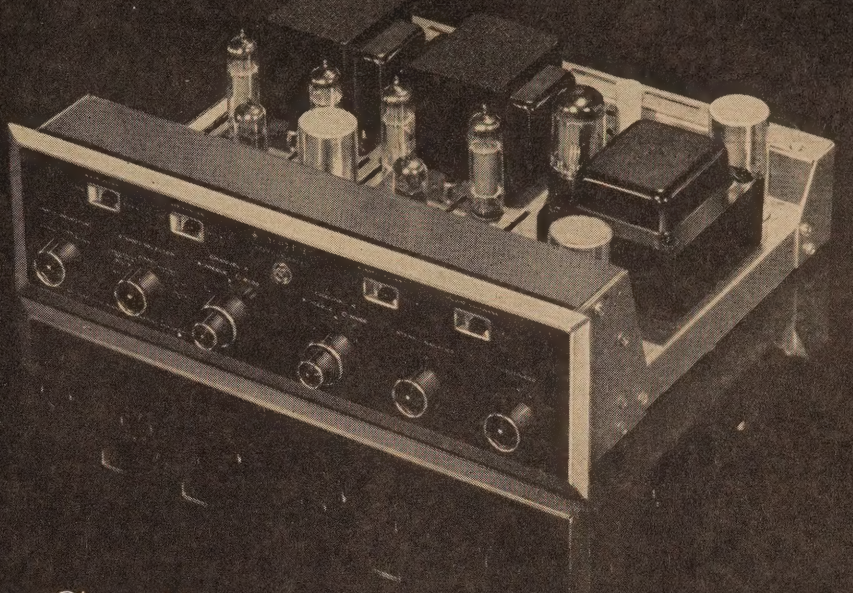

Hermon Scott could make this new kit for $30 less, If...

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The LK-48 is rated at 48 watts. By using a smaller power supply, ordinary output transformers, and pushing the output tubes to their limits, the amplifier might still produce 48 watts at 1000 cycles where many amplifier kits are rated. But measured at 20 cycles, where Scott engineers feel power is really important, output would be down considerably. No compromise was made. The LK-48 *actually* produces 28 watts per channel at 20 cycles, and delivers full power throughout the audio range.

Many kits use a one color instruction book. Hermon Scott decided to continue to use full color to insure factory-built performance, even at the hands of a novice.

Important Scott engineering extras like the all-aluminum chassis, DC operated preamp heaters and unique hum-null balancing could have been eliminated. Hum would have been audibly higher and distortion at levels normal to many kits, but Hermon Scott felt that the kit builder was entitled to the same performance he has come to expect from Scott factory-wired units.

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Radio-Electronics

MAY 1962
VOL. XXXIV No. 5

Formerly RADIO CRAFT — Incorporating SHORT WAVE CRAFT—TELEVISION NEWS—RADIO & TELEVISION*

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(Story on page 48)

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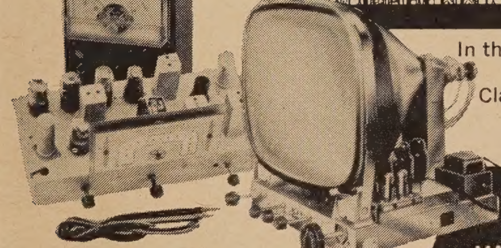

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News Briefs

FCC May Charge License Fees

The FCC proposes a charge for licenses and other regulatory functions. Suggested rate schedule calls for $150 for new commercial broadcast stations or major changes in existing AM and FM stations, and $250 for similar TV applications. For TV translators and other broadcast applications, the fee would be $30. Safety and special radio services would be charged $5 for amateur and disaster services, and $20 for all other special radio services. Charges for common-carrier applications would range from $10 to $150. A $20 fee is proposed for experimental-service applications.

The commission also suggests $2 to $5 fees for commercial radio operator exams and licenses.

Atomic-Powered Weather Station Installed in Arctic

The world's first atomic-powered automatic weather station is now operating at Sherwood Head on Axel Heiberg Island in the Arctic. The original site was to have been Graham Island, but ice and shoals prevented landing the apparatus there. The new location is some 60 miles farther north.

The station transmits temperature, barometric pressure and wind speed every 3 hours.

Power for the station comes from pellets of a strontium-90 compound that generates heat spontaneously by radioactive decay. A series of thermocouples turns the heat into electrical energy, which is stored in rechargeable batteries to operate the intermittently transmitting equipment. The data are transmitted on 3.4 and 5 mc simultaneously. The total transmission takes only 9 seconds every 3 hours. Output is 250 watts on each frequency. The picture shows the artist's concept of the station as installed, probably a much more detailed and satisfactory picture than could have been obtained by actual photography.

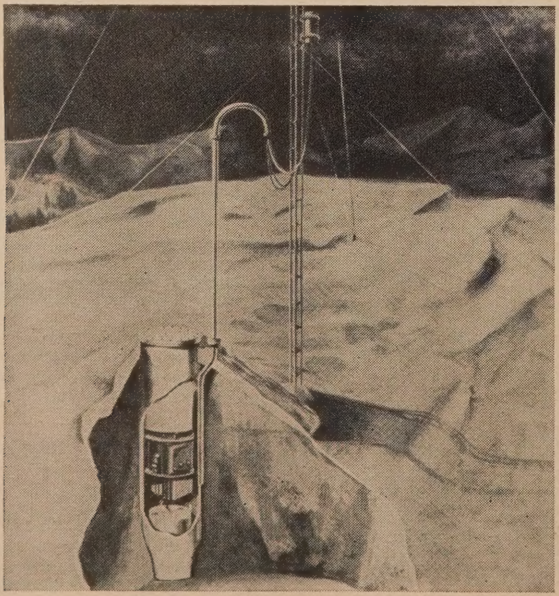
"Discrete" Is Discreet

For secret communications, the University of Michigan announces the "discrete frequency synthesizer" developed by its Cooley Electronics Laboratory under the leadership of Thomas W. Butler, Jr. Ph.D.

Through a process known as "pseudo-random generation," both receiver and transmitter jump from frequency to frequency, apparently at random, but actually following a computer-designed pattern. Eavesdropping is rendered impossible.

The tuning mechanism consists of a diode that varies capacitance, allowing frequency changes up to 500,000 times per second with a high degree of accuracy—1 part in 100,000,000. Only a single crystal is required, as the diode generates a large number of harmonics. The device is built of solid-state components and contains no moving parts.

The "discrete frequency synthesizer," says Dr. Butler, should be particularly useful in air navigation systems.



Translator Concern Proposes Cutting TV Audio

A change in the aural–visual power ratio in low-power transmitters has been recommended to the FCC as a means of fostering expanded use of uhf television channels. According to Adler Electronics Inc., who made the proposal, this would make a considerable saving in lower-powered transmitters, which can use a common amplifier for both visual and aural, and would also eliminate the costly diplexer. Experiments with a visual-to-aural power ratio of 4 to 1 and even higher have not brought forth a single reported instance of reduced coverage area, whereas, with the present 2-to-1 ratio, the aural signal coverage is greater than the visual at both vhf and uhf. Other suggestions for cutting costs in low-power stations such as those used for television translators were elimination or reduction of the requirements of vestigial sideband suppression, elimination of restrictions on antenna directivity, provision for remote control, and elimination of the current uhf channel assignments.

Radio Waves Measure Ice

The Army Signal Corps has measured the depth of a massive glacier with a new radio-sounding technique. Amory H. Waite, Jr., veteran engineer of the Research and Development Lab, reports that the soundings were made on Brae Glacier, 20 miles south of Ellsmere Island in the far-north region of Canada.

The method works this way: radio signals penetrate the depth of the glacier and return to a receiver, after reflecting off underlying soil, rock or water. Traveling time of the signal (about 93,000 miles per second—approximately half the free-

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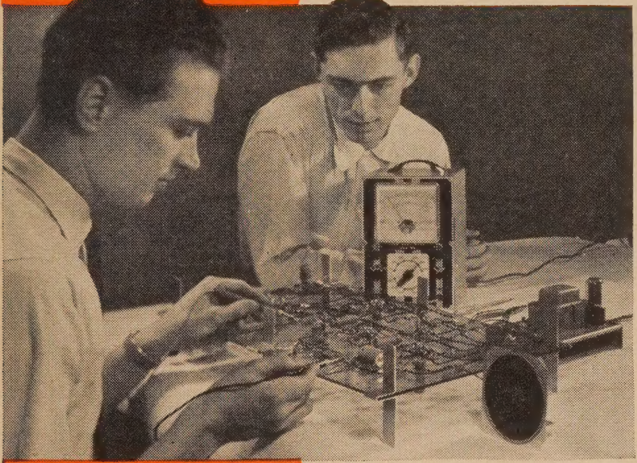

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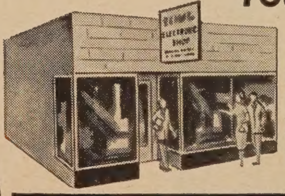

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space velocity) tells operators how deep the glacier is.

The Army Signal Corps technique has been used in measuring ice gaps, but it was thought that the greater movement of glaciers might deflect signals from their course and upset readings. No serious disruptions were observed, however.

Radio sounding is faster and less expensive than the older method of seismic sounding, which involves explosives and highly trained personnel. The work is also being carried on in the Antarctic, and will provide a clearer picture of geographical features hidden by ice in these areas.

FM Sets New Record

Purchases of FM radio receivers exceeded 2,500,000 in 1961, surpassing 1960's former record by 450,000 sets. FM stations have also increased, numbering 1,162 as of mid-February, 1962. A part of this increase represents a steady gain in FM which was beginning in late 1958 and has continued to increase up to the present. Accelerating factors are the entry into the field of FM stereo and the development of FM automobile and portable radios, first imported from abroad and now being made in the United States as well.

Writer Wins Edison Award

Amateur radio operator William G. Welsh, 34, of Cambridge, Mass., and Burbank, Calif., has received General Electric's 1961 Edison Radio Amateur Award for public service. In addition to the award trophy, he received a $500 cash prize.

Employed as an electronics engineering writer by Raytheon Corp., Waltham, Mass., and more recently by Librascope, Inc., Glendale, Calif., Welsh operates amateur radio station W1SAD/6 and uses his spare time to teach electronics. He is said to have devoted 20 to 30 hours a week to this endeavor over the past 10 years, giving free instruction to about 2,800 persons.

His courses include eight 1,800-foot code practice tapes, which he has run off free of charge and distributed to voluntary study groups throughout the nation and in at least 12 foreign countries.

Nominated by various persons in the Boston area, Welsh was chosen from 23 candidates as the tenth winner of this award.

Special citations also went to runners-up Robert T. Herndon, Port Lavaca, Texas; Eugene M. Link, Boulder, Colo.; and George L. Thurston, Tallahassee, Fla.

Lucien Chretien Passes

Lucien Chrétien, electronics editor of the magazine *Radio et TV* (formerly *La TSF pour Tous*) for more than 30 years, has died in Paris. In addition to his work as editor, he was the author of a number of texts on radio, television and electronics, an instructor (Ingénieur de l'Ecole Supérieure d'Electricité) an inventor, and a technical journalist since 1917.

Doppler Navigators To Take Over in Air?

Aerial navigators on TWA's overseas jetliners may soon be replaced by Doppler radar sets and analog computers.

The human navigator accomplished his task with radio aids, dead reckoning and a periscopic sextant for celestial observation. Limitations of this method demanded a longer and wider block of air space for each flight. The new system, far more accurate, permits sharp reduction in ocean air-space assignments.

The TWA cockpit now contains a side-by-side pair of ground speed and drift indicators (A and B), each preset to give guidance for the first two segments of the trip—about 500 miles each. The pilot then sets A for the third segment, and the units overtake each other in leapfrog fashion for the rest of the journey.

These computer-run units are adjusted by turning knobs to the preselected course and mileages supplied to the pilot before flight time.

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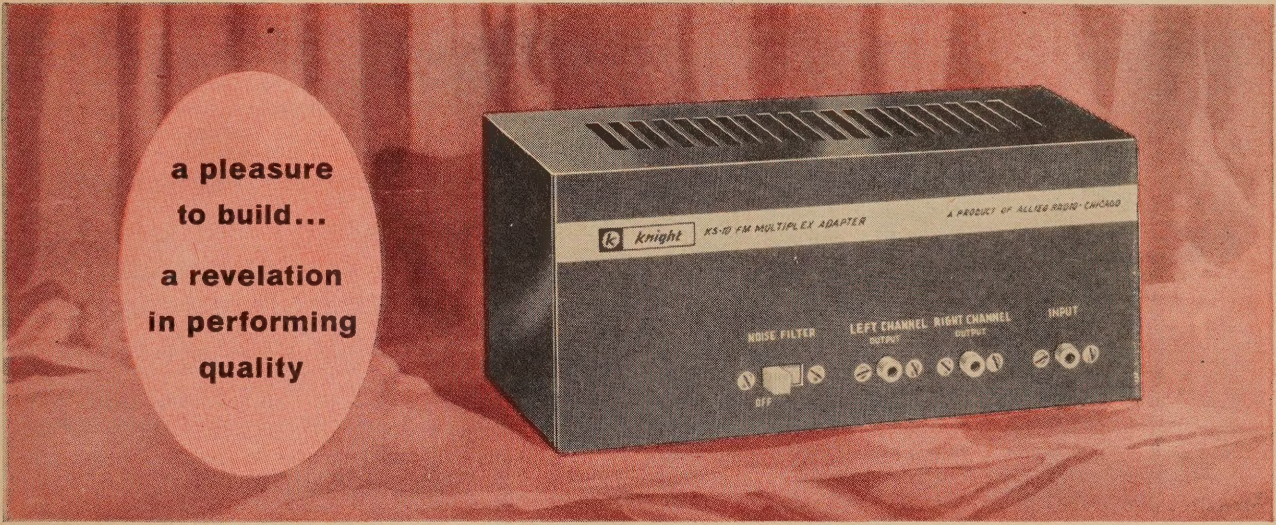
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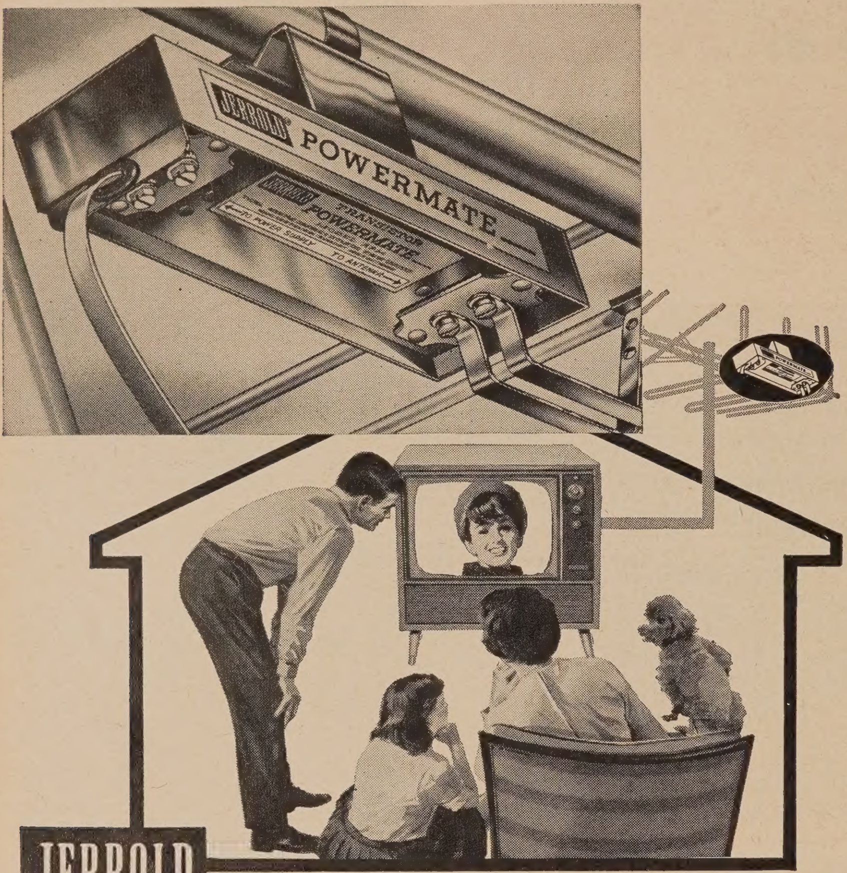

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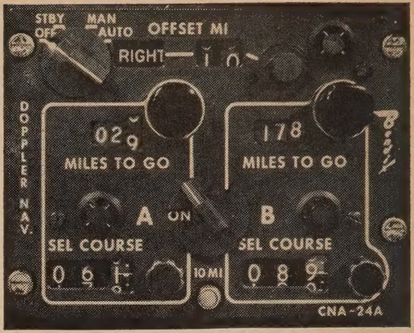

A vertical bar informs the pilot that he is on course or specifies the number of miles off course. A drift-angle pointer indicates the amount of heading correction necessary to compensate for crosswinds.

Barber-pole alarm flags in the indicator windows tell the pilot when the Doppler system is not working due to microwave signals glancing off the ocean's surface.

Although TWA officials say the system is "fantastically accurate," the FAA requires the use of ground-based radio aids to confirm positions, at least for the present.

Calendar of Events

IRE-AIEE Symposium on Mathematical Theory of Automata, April 24–26, United Engineering Center, New York, N. Y.

NATESA Directors Spring Conference, Apr. 28–29, Americana Hotel, Miami, Fla.

SMPTE 91st Convention, April 29–May 4, Ambassador Hotel, Los Angeles, Calif.

IRE, AIEE Spring Joint Computer Conference, May 1–3, Fairmont Hotel, San Francisco, Calif.

IRE International Congress on Human Factors in Electronics, May 3–4, Lafayette Hotel, Long Beach, Calif.

IRE, AIEE, EIA Electronic Components Conference, May 8–10, Marriott Twin Bridges Hotel, Washington, D. C.

IRE National Aerospace Electronics Conference, May 14–16, Biltmore Hotel, Dayton, Ohio.

Institute for Advancement of Medical Communication Council on Medical TV, May 15–16, National Institutes of Health, Bethesda, Md.

Navy Medical Dental TV Workshop, May 16–17, National Naval Medical Center, Bethesda, Md.

1962 Electronic Parts Distributors Show, May 21–24, Conrad Hilton Hotel, Chicago. Attendance limited to manufacturers, distributors, representatives and their advertising agencies. RADIO-ELECTRONICS will exhibit in Room 610.

ISA National Aero-space Instrumentation Symposium, May 21–23, Marriott Twin Bridges, Motor Hotel, Washington, D. C.

IRE, AIEE, ASME, ISA National Telemetering Conference, May 23–25, Sheraton Park Hotel, Washington, D. C.

EIA Annual Convention, May 23–25, Pick-Congress Hotel, Chicago, Ill.

IRE Seventh Region Space Communications Conference, May 24–26, Seattle, Wash.

IRE Spring Conference on Broadcast and TV Receivers, June 18–19, O'Hare Inn, Chicago.

Not All Recruiters Welcome Women Engineers

Despite the statement of Mildred Webber, placement official at the University of Michigan (Radio-Electronics, April, 1962, page 12), who said that "women have just as good a chance as men in any science field, and can earn comparable salaries," a survey of personnel recruiters from 30 of the nation's larg-

(*Continued on page* 16)

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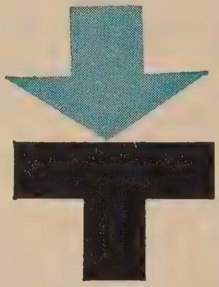


When you're putting together a DC power supply, these little Mallory packaged rectifier circuits can spark a lot of time-saving, space-squeezing ideas.

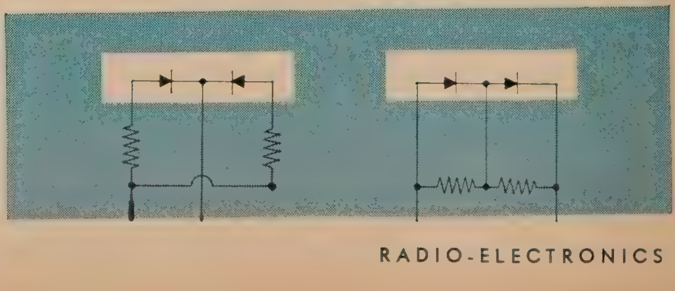
Each package is a complete rectifier circuit . . . bridge, doubler or center-tap . . . that does the job of two or four separate rectifiers. So you've only got *one* component to wire in place. The individual rectifier cells are factory-connected in the package.

You can get the exact rectifier you want in this compact form. And we mean compact. Less than ¾″ by ½″, and ¼″ thick. Cold case design, too; you can mount 'em anywhere without worrying about case-to-ground shorts.

PRV ratings on all three types go as high as 600 volts. And there's plenty of current capacity. The FW full wave bridge models are rated 1.5 amps. DC at 50°C. ambient, 1.0 amp. at 100°C. Doubler Type VB and center tap Type CT are rated 0.75 amp. at 50°C., 0.5 amp. at 100°C.

If you need more current rating, you can parallel the two sides of the type CT package, using 0.5-ohm equalizing resistors in series with each leg. And you can get a high PRV unit at low cost by using a type VB double package as a series-connected half-wave rectifier, connecting a one-megohm resistor across each cell for voltage equalization.

As if all this weren't enough, you save money, too, because our packaged circuits cost less than individual rectifiers. Get them from your Mallory Franchised Distributor. He's a good man to call on for Mallory capacitors, switches, controls, batteries, resistors and vibrators . . . and for any other components you need.



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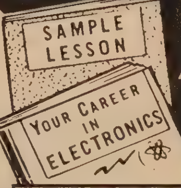

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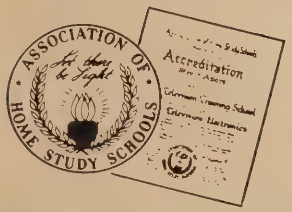
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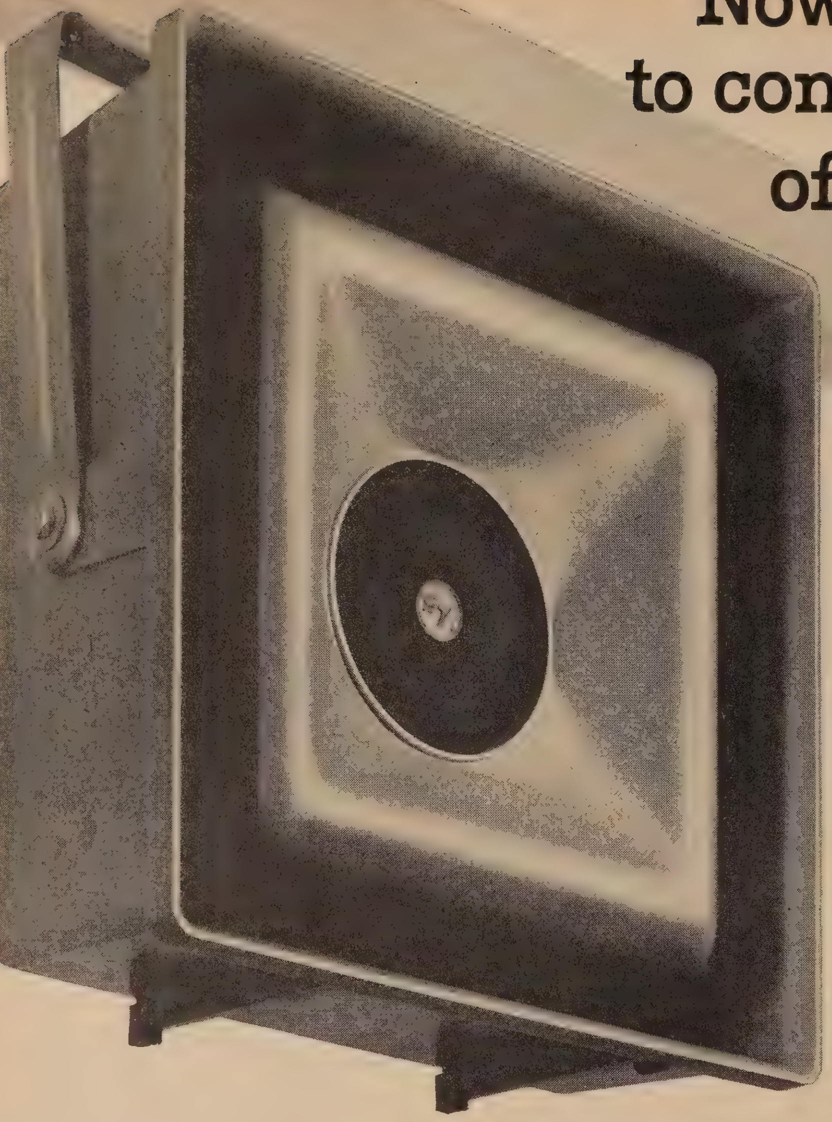

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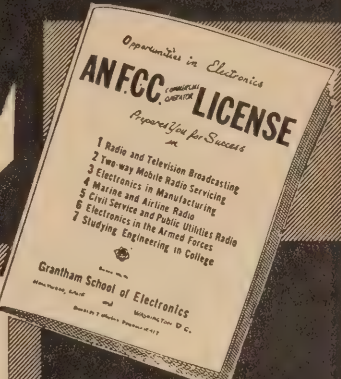

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M. A. Dill, Jr., 20 Cherry St., Gardiner, Maine	1st	12
Bernhard G. Fokken, Route 2, Canby, Minn.	1st	12
Kenneth F. Foltz, Broad St., Middletown, Md.	1st	12
James C. Greer, Mound City, Kansas	1st	12
Thomas J. Hoof, 216 S. Franklin St., Allentown, Pa.	1st	22
Clyde C. Morse, 7505 Sharronlee Dr., Mentor, Ohio	1st	12
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a quality trio of microphones for "loud & clear" communications

There's no secret to Sonotone's ability to combine performance with durability. Sonotone has pioneered research in hearing aids — where transducers must meet the unbelievably critical demands of frequency response and day-in, day-out use and still function dependably. This know-how is responsible for this smartly engineered line-up of microphones tailored to communications requirements.

SONOTONE CERAMIKES

perfect cb team

CM-30
CM-31
CM-17A

SONOTONE CERAMIKE CM-30 — Perfect for mobile use. Intelligibility unsurpassed. Sensitivity curve favors voice frequency range. High sensitivity from -49 db from 90 to 6000 cps. Ruggedly built to take the punishment of mobile use. Lightweight, shatterproof plastic case. Easy to handle—and control with convenient "Push-to-Talk" button. Has special dashboard mounting bracket. Supplied with spring-spiraled 4-conductor shielded cable. **List $14.00.**

SONOTONE CERAMIKE CM-17A — 13″ Flex-mike. Ideal base station microphone for CB-or other communications applications. Gooseneck mounting makes it easy to talk while keeping hands free. Sharp,clear communication with frequency response sensitivity of -56 db from 50 to 11,000 cps, ± 2 db. Equipped with 6′ shielded cable. **List $24.50.**

rugged mobile communications mike

SONOTONE CERAMIKE CM-31 — Budget-priced communications model in shatterproof plastic case features excellent intelligibility (90 to 6000 cps frequency range at -49 db sensitivity). 2-conductor coil cable — no switch. **List $13.50.**

Fixed communications or mobile, Sonotone Ceramikes provide top-flight, long-term, maintenance-free performance.

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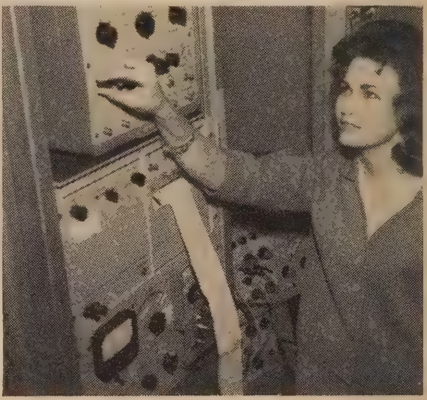
(*Continued from page* 10)

est defense contractors reveals that 20% are still reluctant to hire women engineers and scientists.

The survey was made by the Research Dept. of Careers Inc., national job information clearing house for scientists and engineers. Since it consisted of interviews with the actual recruiters of some of the nation's largest defense contractors, it may perhaps reflect the facts more accurately than the "official" statements of corporation spokesmen.



—Army Photo

Engineer Sylvia Welker, with the Signal Missile Support Agency at the White Sands Missile Range, N. M., is a graduate of Virginia Polytechnic Institute. Mrs. Welker, 24, is the youngest of several women engineers at the Range. She holds down a full-time work assignment in the Vulnerability Research and Development Branch of Missile Electronic Welfare Division. In her spare time, she cares for her 14-month-old daughter, works toward her Master's degree at New Mexico State University and studies Russian at a night class.

The question "Are you reluctant to hire women scientists or engineers?" was asked recruiters representing 30 corporations. The answers were "No, not reluctant"—23, "Yes, reluctant"—6.

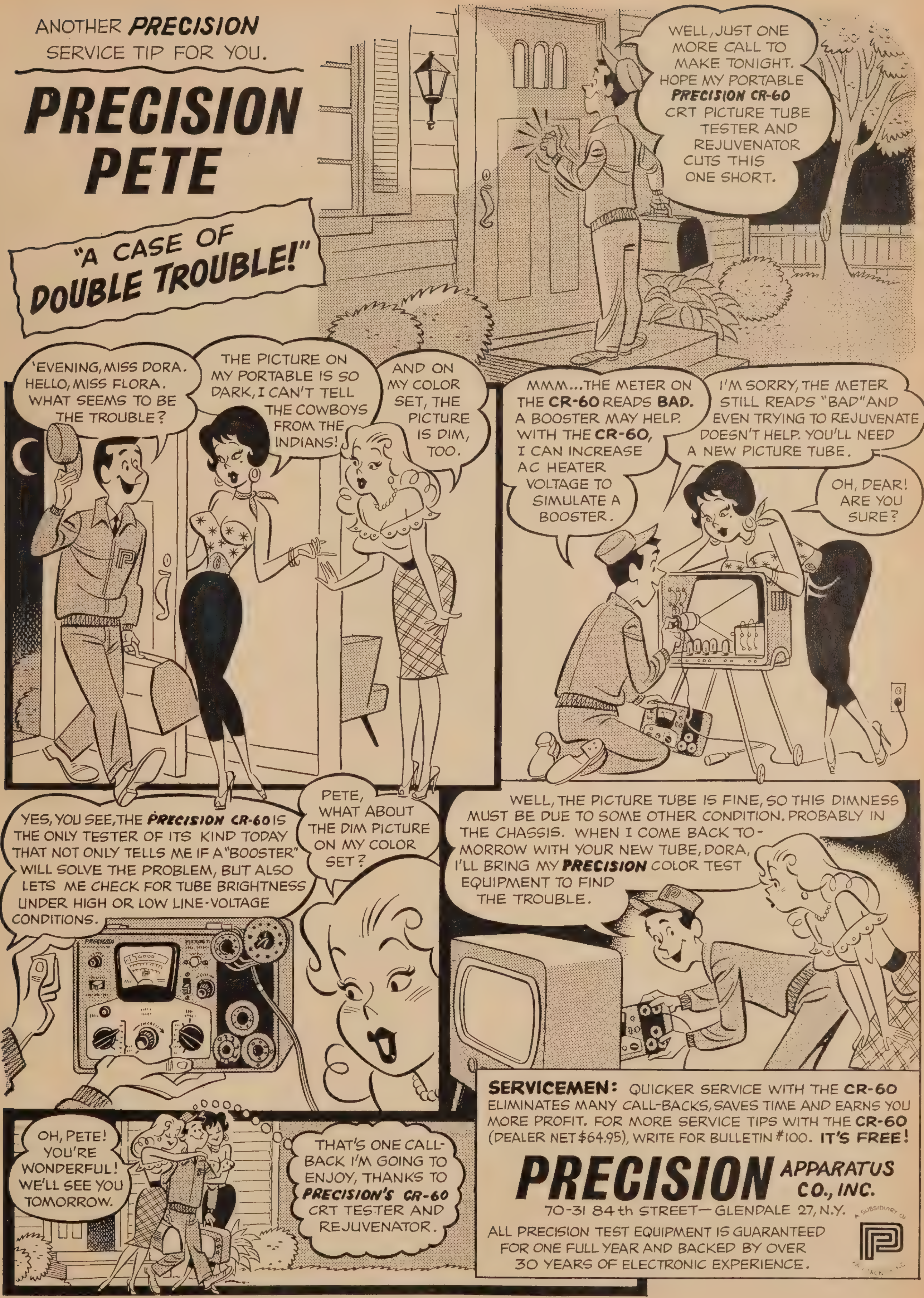
Electric Power Station Will Use Atomic Energy

The Atomic Energy Commission has issued a permit for a 40,000-kw high-temperature, gas-cooled nuclear power station at Peach Bottom in southeastern Pennsylvania.

The Peach Bottom plant will be built by Philadelphia Electric and 52 other electric utility companies, organized as High Temperature Reactor Development Associates Inc. The 53 companies generate 42% of all the electricity produced by the privately owned power companies of the United States.

The plant is expected to be in operation by mid-1964, and will be operated by Philadelphia Electric as a unit of its 3,500,000-kw power generating system. It will represent the first commercial application of an advanced technique of nuclear power generation known as the high-temperature, gas-cooled power reactor.

(*Continued on page* 20)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PRECISION PETE
"A CASE OF DOUBLE TROUBLE!"
WELL, JUST ONE MORE CALL TO MAKE TONIGHT. HOPE MY PORTABLE PRECISION CR-60 CRT PICTURE TUBE TESTER AND REJUVENATOR CUTS THIS ONE SHORT.
'EVENING, MISS DORA. HELLO, MISS FLORA. WHAT SEEMS TO BE THE TROUBLE?
THE PICTURE ON MY PORTABLE IS SO DARK, I CAN'T TELL THE COWBOYS FROM THE INDIANS!
AND ON MY COLOR SET, THE PICTURE IS DIM, TOO.
MMM...THE METER ON THE CR-60 READS BAD. A BOOSTER MAY HELP. WITH THE CR-60, I CAN INCREASE AC HEATER VOLTAGE TO SIMULATE A BOOSTER.
I'M SORRY, THE METER STILL READS "BAD" AND EVEN TRYING TO REJUVENATE DOESN'T HELP. YOU'LL NEED A NEW PICTURE TUBE.
OH, DEAR! ARE YOU SURE?
YES, YOU SEE, THE PRECISION CR-60 IS THE ONLY TESTER OF ITS KIND TODAY THAT NOT ONLY TELLS ME IF A "BOOSTER" WILL SOLVE THE PROBLEM, BUT ALSO LETS ME CHECK FOR TUBE BRIGHTNESS UNDER HIGH OR LOW LINE-VOLTAGE CONDITIONS.
PETE, WHAT ABOUT THE DIM PICTURE ON MY COLOR SET?
WELL, THE PICTURE TUBE IS FINE, SO THIS DIMNESS MUST BE DUE TO SOME OTHER CONDITION. PROBABLY IN THE CHASSIS. WHEN I COME BACK TOMORROW WITH YOUR NEW TUBE, DORA, I'LL BRING MY PRECISION COLOR TEST EQUIPMENT TO FIND THE TROUBLE.
PRECISION
OH, PETE! YOU'RE WONDERFUL! WE'LL SEE YOU TOMORROW.
THAT'S ONE CALL-BACK I'M GOING TO ENJOY, THANKS TO PRECISION'S CR-60 CRT TESTER AND REJUVENATOR.

SERVICEMEN: QUICKER SERVICE WITH THE **CR-60** ELIMINATES MANY CALL-BACKS, SAVES TIME AND EARNS YOU MORE PROFIT. FOR MORE SERVICE TIPS WITH THE **CR-60** (DEALER NET $64.95), WRITE FOR BULLETIN #100. **IT'S FREE!**

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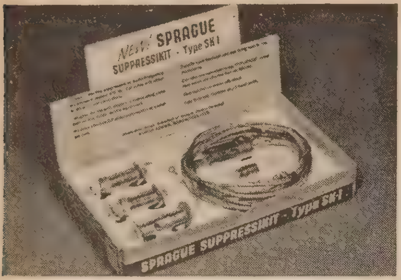

New! SPRAGUE SUPPRESSIKIT · Type SK-1
SPRAGUE SUPPRESSIKIT · Type SK-1

The Sprague Type SK-1 SUPPRESSIKIT—Easily installed on any truck, car, or boat engine using a 2-pole d-c generator.

RADIO HAMS, fleet owners, and CB operators can now enjoy clearer, more readable, less tiring mobile communications at longer effective ranges.

Sprague's new Type SK-1 SUPPRESSIKIT provides effective RF Interference suppression—at moderate cost—up through 400 megacycles. Designed for installation on automobiles, trucks or boats with either 6-volt or 12-volt generators, the Suppressikit makes possible high frequency interference control by means of Sprague's new, extended range, Thru-pass® capacitors.

The components in the SK-1 Suppressikit are neatly marked and packaged, complete with easy-to-follow installation instructions. All capacitors are especially designed for quick, simple installation. Unlike general-purpose capacitors, these heavy-duty units are rated at 60 amperes, and will operate at temperatures to 125°C (257°F). This means you'll have no trouble with an SK-1 installation in the terrific temperatures found "under the hood" on a hot summer's day. There's no chance of generator failures from capacitor "short outs", as with 85°C general purpose capacitors.

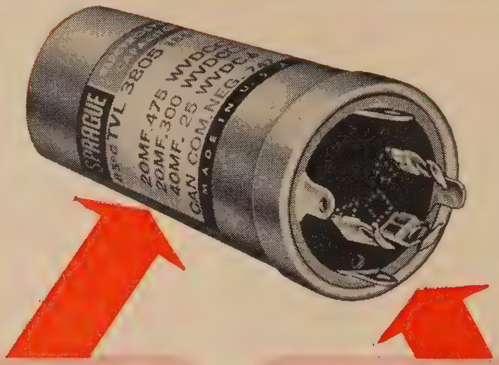
The Deluxe Suppressikit is furnished complete with an 8-foot shielded lead on the generator capacitor which can be trimmed to necessary length for any car or small truck, preventing RF radiation from armature and field leads.

Containing only 5 easy-to-install capacitors, the Deluxe Suppressikit is truly a "do-it-yourself" kit. The net price of $17.85 is a little higher than that of makeshift, thrown-together kits, but it saves you so much time and aggravation it's well worth the slight extra cost.

If the SK-1 Suppressikit is not available at your Sprague Electronic Parts Distributor, send your order to Sprague Products Company, 81 Marshall St., North Adams, Mass.

HPB 6S-341 3-13-62

Sprague TWIST-LOK® Capacitors give you 2 tremendous advantages over all other twist-prong electrolytics


SPRAGUE
TVL 3805
20MF 475 WVDC
20MF 300 WVDC
40MF 25 WVDC
CAN COM NEG.
MADE IN U.S.A.

1

The right size, the right rating, for EVERY replacement job

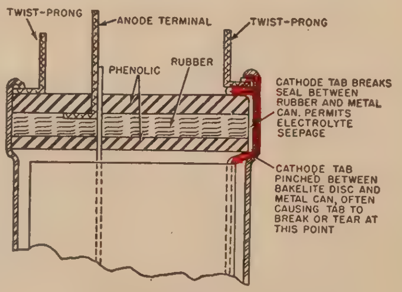
No need to compromise or improvise...the TWIST-LOK Line includes over 1690 different capacitors . . . It's the industry's most complete selection of twist-prong type capacitors, bar none!

2

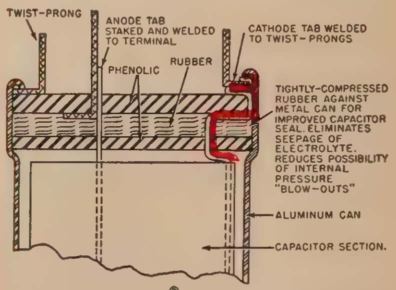
Exclusive, improved cover design for greater dependability

Type TVL Twist-Lok Capacitors are now more dependable than ever! Sprague's new cover design provides a truly leak-proof seal and permits capacitors to withstand higher ripple currents.

Compare internal construction of TWIST-LOK to ordinary 'Lytic!


TWIST-PRONG
ANODE TERMINAL
TWIST-PRONG
PHENOLIC
RUBBER
CATHODE TAB BREAKS SEAL BETWEEN RUBBER AND METAL CAN. PERMITS ELECTROLYTE SEEPAGE
CATHODE TAB PINCHED BETWEEN BAKELITE DISC AND METAL CAN, OFTEN CAUSING TAB TO BREAK OR TEAR AT THIS POINT

ORDINARY ELECTROLYTIC CAPACITOR


TWIST-PRONG
ANODE TAB STAKED AND WELDED TO TERMINAL
CATHODE TAB WELDED TO TWIST-PRONGS
PHENOLIC
RUBBER
TIGHTLY-COMPRESSED RUBBER AGAINST METAL CAN FOR IMPROVED CAPACITOR SEAL. ELIMINATES SEEPAGE OF ELECTROLYTE. REDUCES POSSIBILITY OF INTERNAL PRESSURE "BLOW-OUTS"
ALUMINUM CAN
CAPACITOR SECTION.

SPRAGUE TWIST-LOK® ELECTROLYTIC CAPACITOR

Complete listings are shown in handy Wall Catalog C-457. Get your copy from any Sprague Distributor, or write to Sprague Products Company, 81 Marshall St., North Adams, Mass.

WORLD'S LARGEST MANUFACTURER OF CAPACITORS

SPRAGUE®
THE MARK OF RELIABILITY

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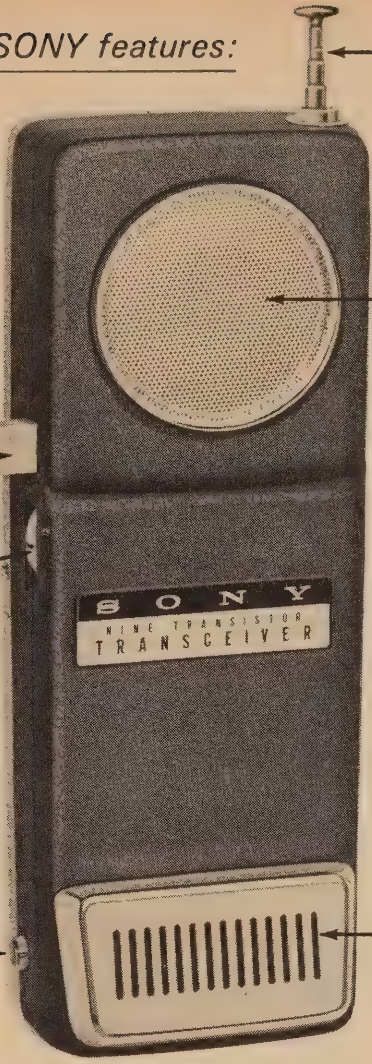
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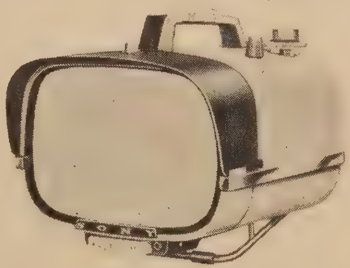
VARIABLE RELUCTANCE MICROPHONE
PUSH-TO-TALK BUTTON
VOLUME CONTROL
SONY
NINE TRANSISTOR
TRANSCEIVER
EARPHONE JACK
2¼" PERMANENT MAGNET SPEAKER

SONY® *quality Citizens Band Transceiver*

RESEARCH MAKES THE DIFFERENCE

The New Sony 9 Transistor Citizens Band Class D transceiver uses a SEPARATE MICROPHONE AND SPEAKER. A quality product of the world's foremost research and development team in transistor electronics, weighs only one pound and is powered by 8 penlite cells for up to 50 hours of operation. The crystal controlled CB-901 employs a sensitive variable reluctance microphone and 2¼" PM speaker. Note how the microphone and speaker are each placed in the most natural position for transmitting and receiving. With 5 foot telescoping whip, push-to-talk button and volume control, the SONY CB-901 lists at **$149.95** per pair, including batteries, earphones and leather case. Stop in at your dealer's and test it today.

Also see the amazing **SONY 8-301W TV,** the only truly portable, fully transistorized set that works on its own battery pack, 12v auto/boat battery and AC. Weighs a mere 13¼ lbs. List **$249.95.** BCP-2 alkaline battery power pack, **$39.95.**



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514 Broadway, New York 12, N. Y.
Regional Offices
Western: 627 South Towne Ave., Los Angeles 21, Calif.
Central: 4959 W. Belmont Ave., Chicago 41, Ill.

Please send me the Sony "FACTS" booklet covering the SONY 8-301W TV and information on the SONY CB-901 Transceiver.

NAME____________________

ADDRESS____________________

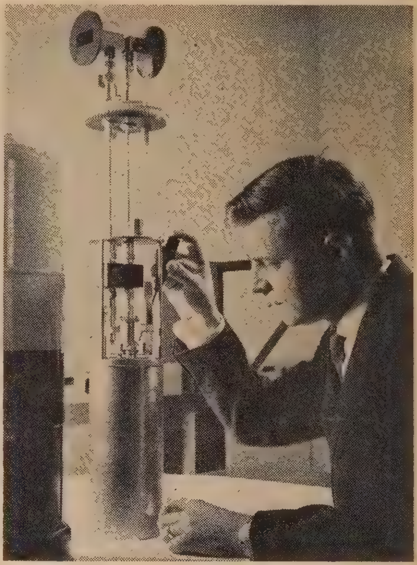
CITY__________ZONE_____STATE________

SONY CORP. OF AMERICA, 514 B'WAY, N.Y. 12, N.Y.

(Continued from page 16)

Parametric Amplifier Features New Noise Figure

A microwave amplifier with a noise figure of about 0.9 db, the lowest noise ever achieved by this type of amplifier, is reported by Bell Telephone Laboratories. A new, hermetically sealed gallium arsenide diode is one of the factors contributing to the improvement in this amplifier. Another contributor is a new cooling arrangement, in which the amplifier is contained in a metal cavity, sealed by indium wire and immersed in liquid nitrogen. This leads to more even cooling, and improves operating stability. The nitrogen cannot leak into the device.



K. M. Eisele of Bell Labs makes final adjustment to new low-noise parametric amplifier before it is sealed into it cavity and immersed in liquid nitrogen.

Brief Briefs

A tandem Van de Graaff 15,000,000-electron-volt accelerator is being installed by Rutgers University, New Jersey, in collaboration with the Bell Telephone Laboratories. It will be used in nuclear research by both organizations.

A semiconductor strain gage with an output powerful enough to drive panel meters direct has been introduced by International Resistance Co. The new strain-gage pressure transducer is rated for 5 volts dc output, and will not require amplifiers in most applications.

A video tape recorder weighing only 30 pounds, and able to record ½ hour of television pictures, was announced by the Goddard Space Flight Center. The little recorder, developed by Ampex, occupies less than 1 cubic foot of space, and will be used in satellites.

Paul B. Findley, editor of the Bell Laboratories Record for 27 years, until his retirement in 1952, died at the age of 73. END

WE GET BETTER TV RECEPTION THAN YOU DO
YOU DO NOT
YES WE DO
NO YOU DON'T
WE HAVE A WINEGARD ELECTRONIC POWERTRON ANTENNA
OH!
DON'T SEE HOW ANYONE GETS ALONG WITHOUT A POWERTRON

Winegard
ANTENNA SYSTEMS

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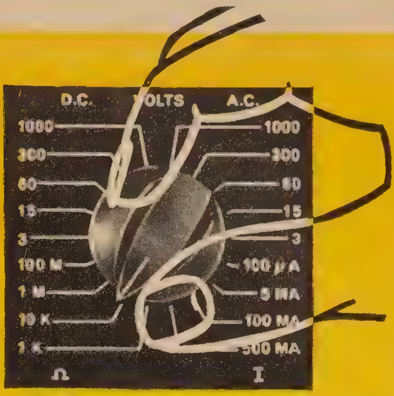
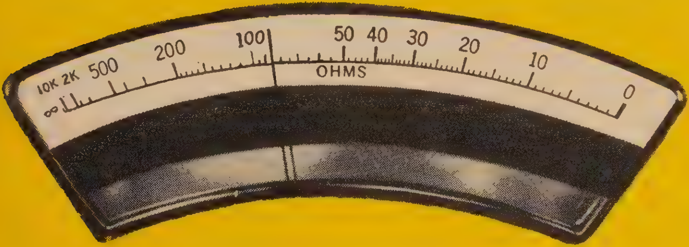
See Only the Scale You Want... in the Exact Range You Want



just set the range switch

and the correct scale appears AUTOMATICALLY



in the new B&K VOM and VTVM

V O MATIC 360

WITH BURN-OUT PROOF METER

AUTOMATIC VOLT-OHM MILLIAMMETER

Greatly simplifies your VOM use. Individual full-size scale for each range—and only one scale visible at any one time, automatically. Once you set the range switch, it is impossible to read the wrong scale. Reading in the range you want is amazingly easy—and direct. No reading difficulties, no multiplying, no errors.

Sensitivity 20,000 ohms per volt DC; 5000 ohms per volt AC. **Accuracy** ±3% DC; ±5% AC; (full scale). DC Volts in 6 ranges 0-6000. **AC Volts** in 6 ranges 0-6000. **AF** (Output) in 4 ranges 0-300 volts. **DC Current** in 5 ranges 0-10 amps. **Resistance** in 4 ranges 0-100 megohms. Supplemental ranges also provided on external overlay meter scales. Meter protected against extreme overload and burn-out. Polarity reversing switch. Automatic ohms-adjust control. Mirrored scale. Complete with 1½-volt and 9-volt batteries, test leads, and easy-viewing stand. Net, $59^{95}

V O matic 360

B&K
MODEL 375 AUTOMATIC VACUUM TUBE VOLTMETER

DYNAMATIC 375

AUTOMATIC VACUUM-TUBE VOLTMETER

Once you set the range switch, you automatically see only the scale you want and read the exact answer directly. Saves time, eliminates calculation, avoids errors. Individual full-size direct-reading scale for each range. Simplifies true reading of peak-to-peak voltages of complex wave forms in video, sync and deflection circuits, pulse circuits, radar systems, etc. Includes DC current ranges, too.

Accuracy ±3% full scale AC and DC. **Sensitive** 100 microampere meter movement. **DC Volts** in 7 ranges 0-1500. **AC Volts** (rms) in 7 ranges 0-1500. **AC Volts** (peak-to-peak) in 7 ranges 0-1500. **DC Current** in 3 ranges 0-500 ma. **Ohms** in 7 ranges 0-1000 megohms. Utilizes single DA-AC ohms probe and anti-parallax mirror. Swivel stand converts to carry-handle. Includes 1½ volt battery.
Operates on 117 volts 50-60 cycle AC. Net, $89^{95}

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for Demonstration, or
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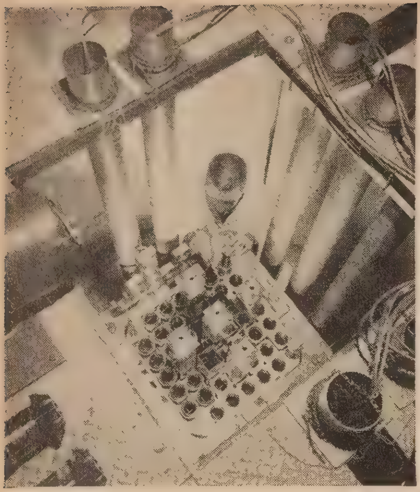

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30

Correspondence

LIKES TROUBLESHOOTING CHARTS

Dear Editor:

Your radio troubleshooting charts that appeared last November and December are just the thing for lazy guys like me. They sure are tops. When are you going to come out with a TV trouble chart?

R. J. CORRIGAN

Dayton, Ohio

[Whether or not he is lazy, the charts help a technician form good servicing habits—to develop a radio servicing technique that will save him time, effort and headaches. The TV trouble chart is a lot more complex. When we have one that really works you'll be sure to see it in RADIO-ELECTRONICS.—*Editor*]

INSTANT ON

Dear Editor:

After seeing the item on "Instant On" in the January 1962 issue, I decided to add such a circuit to a small radio for testing. After studying the diagram, I could not devise a way to replace the special switch–volume control now in the set. Instead, I installed a silicon rectifier across the switch and left the B-plus on. As I see it, with the two rectifiers back to back, it is almost an open circuit anyway. Maybe my theory is wrong on this, but it seems to be working fine.

DICK ROGERS

Rogers Electronics
Brighton, Mass.

[The author thought of that, too! He tried the same thing and it popped the silicons—repeatedly. Experiments are continuing—more will appear in a future issue.—*Editor*]

NO SUSPICION?

Dear Editor:

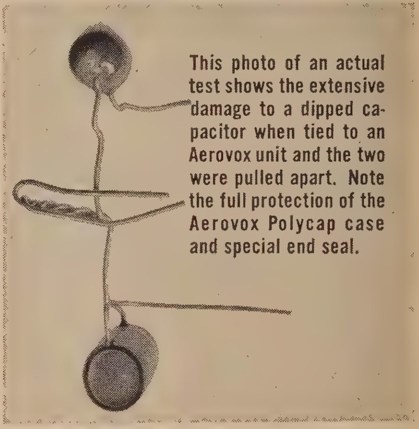
Looking through your October issue I rather belatedly came across this gem of modesty by Mr. Crowhurst: ". . . we suspect that we now know more . . . than anyone else in the industry." This is no mere suspicion with Mr. Crowhurst. It's been a conviction of his for years.

In fairness to your other advertisers, don't you think it's time you started charging Mr. Crowhurst your established rates, and taking his copy out of the editorial section?

Mr. Crowhurst is less interested in advancing the art of stereo—or in anything else — than gratifying his monumental vanity, indisputably the greatest in the industry. He has a

TESTS PROVE POLYCAP® CASE & SPECIAL END SEAL ON AEROVOX BI-ELECTRIC MYLAR PAPER BYPASS CAPACITORS ELIMINATE CRACKING & CHIPPING PROBLEMS

PRODUCT NEWS FROM AEROVOX



This photo of an actual test shows the extensive damage to a dipped capacitor when tied to an Aerovox unit and the two were pulled apart. Note the full protection of the Aerovox Polycap case and special end seal.

Why take chances with the cracking and chipping problems common with conventional dipped capacitors. After all, your profits and your reputation are at stake with every set you service—protect both by replacing with only genuine Aerovox Bi-Electric Mylar* Paper Bypass Capacitors! You see, actual tests prove that the uniform, protective Polycap case from end-to-end, and the special process-controlled end seals, eliminate your cracking and chipping troubles. No wasted time . . . no expensive call-backs, as service technicians everywhere know from experience.

*Registered DuPont trademark

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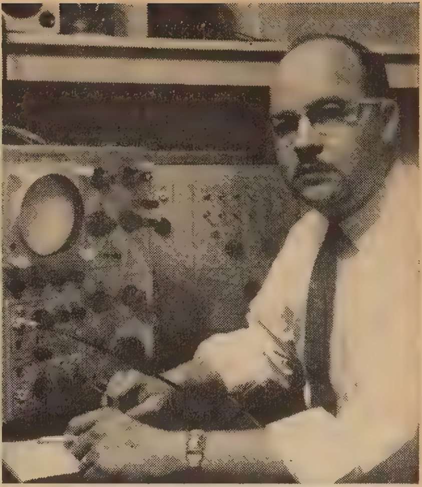
RICHARD S. CONWAY (CREI grad 1960) is Supervisor, Electronic Test Department Wilcox Electric Co., Kansas City, Mo.

ROBERT T. BLANKS (CREI grad 1960) is Engineer, Research & Study Div., Vitro Labs., Division of Vitro Corp. of America, Silver Spring, Md.



MEARL MARTIN, Jr. (CREI grad 1956) is a Senior Engineer and Field Support Manager, Tektronix, Inc., Portland, Oregon.

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SUCCESS IS NO ACCIDENT. There is a reason why some men move ahead in electronics while others stand still, year after year, in routine, low-paid jobs. Responsible, rewarding positions in electronics require advanced technical knowledge. Without such knowledge, you cannot hope for success no matter how bright and ambitious you are.

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Quam Quality Line speakers are enameled in gold—and while the color has no effect on performance characteristics, it symbolizes the quality and reliability that's built into every Quam speaker.

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FIRST LESSON IN
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(JUNE 1962)

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Servicing small transistor radios can be a real headache and a financial loss to service technicians—UNLESS you have the knack of quickly locating and repairing troubles caused by faulty miniature components or defective printed boards.

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Lesson 8. **Making Effective Use of Test Equipment.** Test equipment needs and applications.
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Lesson 10. **Analyzing Troubles by Symptoms.** Commonly-found problems, recognizing the symptoms, and locating defective components.
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mortal fear that his genius will not be fully appreciated, a tragedy he intends to avoid if he has to hit his readers on the head.

ROBERT G. VAUGHAN
Greensboro, N. C.

QUESTION OF RELIABILITY

Dear Editor:

In your February 1962 issue there was a very interesting letter in your correspondence column from Mr. W. F. Palmer, of Palmer Electronics Labs.

In it, he suggested that the reliability of the thyratron ignition system (September 1961) was questionable, and initial and maintenance costs were high. As a manufacturer of transistorized ignition I am inclined to believe this.

Our Magnition works on a similar basis to Mr. Palmer's Transfire but is different in many ways. The Magnition has two power transistors in the switching circuit, and two transistors in a multivibrator circuit controlled by the points.

As in Mr. Palmer's circuit, a special coil is used in our unit, as well as Zener diodes for transient voltage protection.

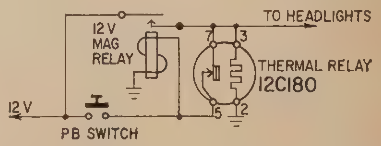
There have been many letters of controversy in the matter of transistor vs. conventional and other types of ignition but, should I be in a position to choose, I would take transistor ignition over all.

KARL M. WIESSMANN
Design Engineer
Hofmann Electronics Co.
Wayne, N.J.

ELECTRONIC PATHFINDER

Dear Editor:

In the September 1961 issue of RADIO-ELECTRONICS appeared an article on an electronic pathfinder. Don't you think this is going to a lot of trouble when something as easy as this could be built?



The pushbutton switch energizes the 12-volt relay, thermal delay relay and headlights. After 180 seconds have elapsed, the normally closed contacts of the thermal relay open, de-energizing the entire system.

WILLIAM CHAKERES
Newark, N. J.

DDT FOR GREMLINS

I note the sound and fury still running on the electronic ignition system. I finally put one together and my troubles began. But I found that, when I finally boiled it for one hour in 100% DDT, the gremlins disappeared and it was ready for the field test. I'll report when the field test is completed.

In the meantime I've been experi-

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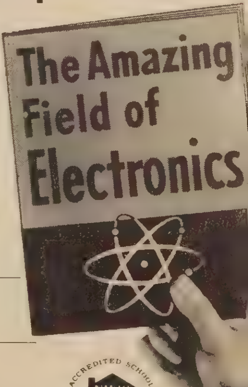

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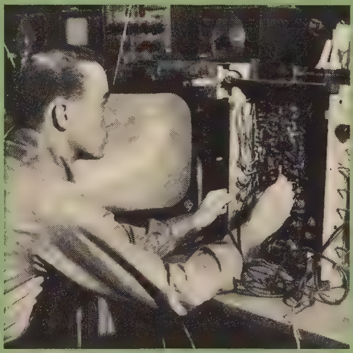

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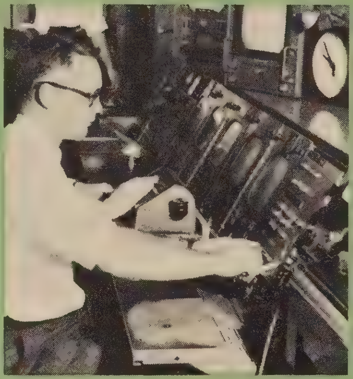

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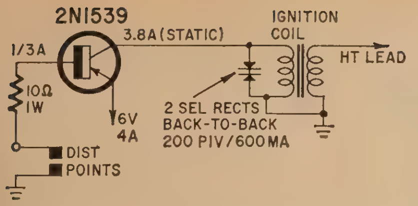


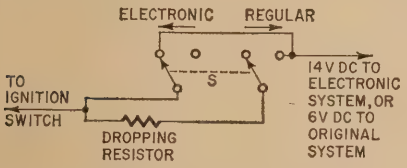
menting with a simple gadget for my Jeep. It gives me a spark many-fold hotter than the standard system, yet reduces current across the breaker points to a twelfth of its former value. Also the reverse surge is well damped. For interested parties the circuit is shown here.

William K. Guthrie, Jr.
Central City, Colo.

ELECTRONIC IGNITION AGAIN

Dear Editor:

After building the electronic ignition system described in the September 1961 issue, I had to make a change to get the unit to work in my 1960 V8 Lark. It was simply a matter of changing C5 from the indicated .001 μf to .003 to trigger the 2D21 with the distributor points. I use the original 12-volt ignition coil on the car.



I found my lead from the ignition switch included a series-dropping resistor which gave me only 6 volts on starting. To overcome this, I installed a separate lead from the ignition switch and, by adding a dpdt switch, I retained the original wiring for use with the regular system if it should ever be needed. See the diagram for the hookup.

Joseph Frei
Alamagordo, N.M.

[Readers will find the value for C5 varies slightly according to the particular thyratron used and the car in which the system is installed.—*Editor*]

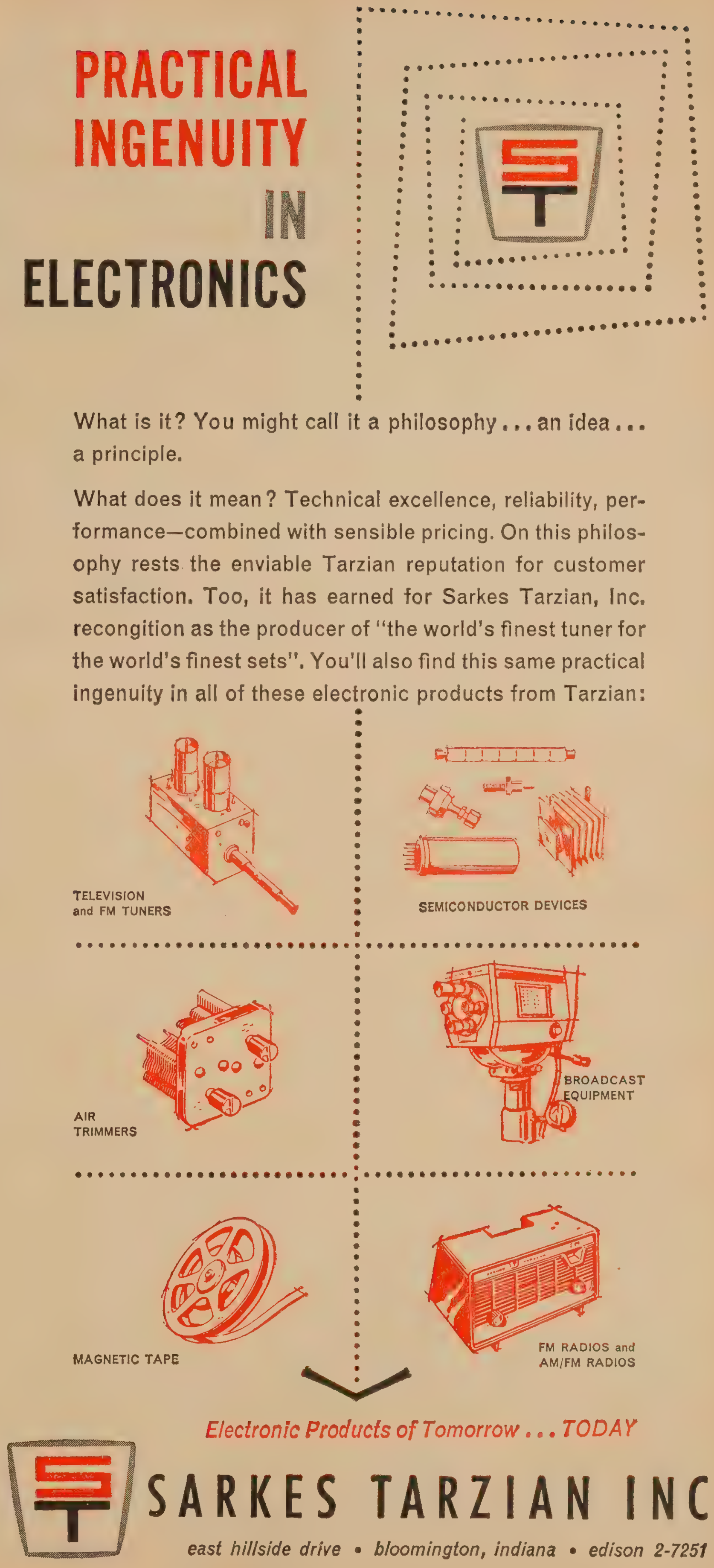
ABOUT THAT "X"

Dear Editor:

With all due respect, whoever wrote the caption "X = Trans" above Mr. Silverman's letter (September, 1961) is misleading Mr. Pearsall (January, 1962) and possibly many more of your readers. The use of "x" as a substitute for *part of a word* (not necessarily "trans") is as old as amateur radio telegraphy and perhaps as old as wire telegraphy. Typical examples include "px" (press), "wx" (weather) and "dx" (distance). See *The Radio Amateur's Handbook*, first edition, page 142.

Think hard. Back in December, how many times were you wished a "Merry Transmas"?

Byron Goodman, W1DX
West Hartford, Conn. END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What does it mean? Technical excellence, reliability, performance—combined with sensible pricing. On this philosophy rests the enviable Tarzian reputation for customer satisfaction. Too, it has earned for Sarkes Tarzian, Inc. recognition as the producer of "the world's finest tuner for the world's finest sets". You'll also find this same practical ingenuity in all of these electronic products from Tarzian:

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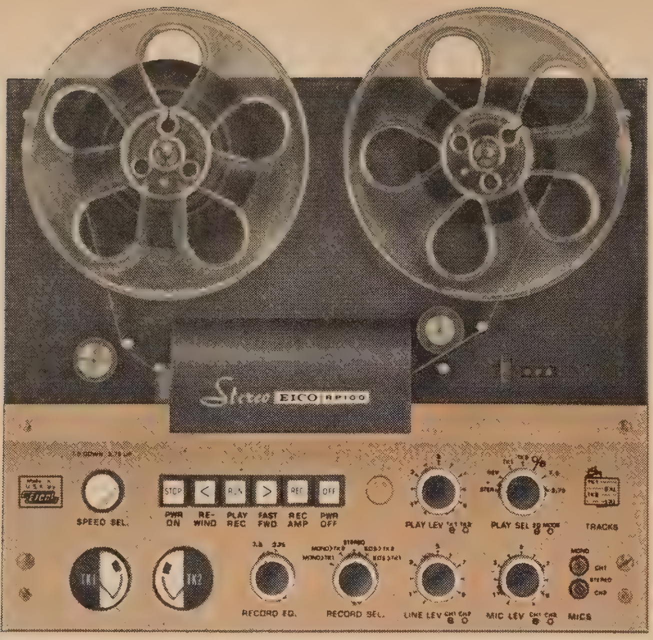

A great tape recorder made greater:

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2. Two **new** take-up and rewind reel motors, both extra-powered for effortless operation.
3. **New** cored-out steel capstan flywheel with all the mass concentrated at the rim for improved flutter filtering.
4. **New** optimally designed capstan drive belt brings wow down to negligibility.
5. **New** relay provides instantaneous extra power to the take-up reel motor at start to minimize tape bounce. Provides near-perfect stop-and-go operation and eliminates any risk of tape spillage when starting with a nearly full take-up reel.
6. **New** automatic end-of-tape stop switch cuts off take-up reel motor power. Also permits professional editing techniques, whereby tape being edited out runs off the machine while you are listening to it.
7. Playback preamps remain"on"during stop-standby mode to permit cueing.
8. Recording level adjustment during stop-standby.
9. Shock-absorbent helical spring tape lifters practically eliminate tape bounce at start of fast winding.

And All These Well-known RP-100 Features:

Separate stereo 1/4 track record and playback heads permitting off-the-tape monitor and true sound-on-sound recording; **separate** transistor stereo record and stereo playback amplifiers meeting true high fidelity standards; monaural recording on 4 tracks; digital turns counter; electrodynamic braking (no mechanical brakes to wear out or loosen); all-electric push-button transport control (separate solenoids actuate pinch-roller and tape lifters); unequalled electronic control facilities such as mixing mic and line controls, two recording level meters, sound-on-sound recording selected on panel, playback mode selector, etc. Modular plug-in construction.

Wow and flutter: under 0.15% RMS at 7½ IPS; under 0.2% RMS at 3¾ IPS. **Timing Accuracy:** ± 0.15% (±3 seconds in 30 minutes). **Frequency Response:** ± 2db 30-15,000 cps at 7½ IPS, 55db signal-to-noise ratio; ± 2db 30-10,000 cps at 3¾ IPS, 50db signal-to-noise ratio. **Line Inputs Sensitivity:** 100mv. **Mike Inputs Sensitivity:** 0.5mv.

Semikit: Tape transport assembled and tested; electronics in kit form $299.95

Factory-assembled: Handwired throughout by skilled American craftsmen $399.95

An original, exclusive EICO product designed and manufactured in the U.S.A. (Patents Pending)

Carrying Case $29.95
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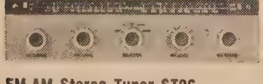

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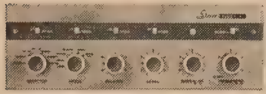
Includes Metal Cover and FET



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Kit $94.95 Wired $149.95
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Radio-Electronics
Hugo Gernsback, Editor-in-Chief

CLOSED-CIRCUIT TV ADVANCES

. . . Vast New Uses for Television Are in The Making . . .

MASS closed-circuit TV, neglected for nearly two decades, suddenly has come of age in 1962. Closed-circuit TV is by no means a novelty; it has been with us since the very beginning of the television art. Baby-watching via TV; police lineups to precinct stations; surveillance of inmates in prisons, or of factory workers; machine inspection; factory gate-watching by night watchmen; TV cameras in hotel and apartment house lobbies that watch the inside of self-service elevators; round-table meetings with officials in different cities; bank surveillance of tellers to verify check signatures and to alert police during holdups; TV in large railroad terminals to speed ticket service; giant TV screens installed in various theaters throughout the country, all interconnected to exhibit sporting events, etc. and other uses too numerous to mention now operate in many parts of the world.

None of these examples, however, are true *mass* closed-circuit TV applications, for *individual* use in the viewers' homes or rooms. The nearest approach today are the Community Antenna Television (CATV) Systems throughout the United States and the Virgin Islands, according to a recent report by the National Community Television Association. There are now roughly 1,000 of them. The "cable" systems average out at 800 subscribers each. Sixteen have more than 500 subscribers, and two serve more than 10,000 viewers each. It is estimated that about 2.5 million viewers use cable and are served by lines which, for the most part, carry five signals. A number carry only one, and others have as many as nine. Pennsylvania has the largest number of CATV systems, with 204 listed, while five states have only one.

Long before broadcast television, the present writer foresaw that one day we would have actual live theater in the home via closed-circuit TV. In his former magazine, *Television News*, in the January-February issue of 1932, he covered the subject under the title "The Tele-Theater." Instead of paying outrageous prices for theater tickets, viewers could see all important *live* Broadway shows *direct* from the theater via TV at 50 cents. If millions of people would view such Tele-theater shows at 50¢ a family, the theater entrepreneurs would soon grow rich. While this idea has still to be realized, a parallel series of enterprises has erupted quietly without much fanfare.

In Manhattan's Hotel Statler-Hilton, the Telad Corp. has installed a system whereby every one of the 2,200 hotel room guests can see a special program about sightseeing New York, shopping news from the big stores, gallery openings, all sorts of special New York events, weather and transportation information, theater news, special restaurant information—in short, everything that out-of-town visitors and tourists wish to know. This information is received on regular TV receivers, tuned to channel 6 (normally blank in New York City).

The program on channel 6 repeats every half hour. The company spots about 5 minutes of commercials for each half hour. Programs run 12 hours a day, seven days a week, starting at 8 AM daily.

Another company, Teleguide, will broadcast similar TV programs to 12 (or more) other hotels comprising some 12,000 rooms. This company will use channels 3, 6 and 10—all presently unused in New York City. Thus channel 3 will carry condensed programs in French, German, Italian, Japanese, Portuguese and Spanish—30 minutes for each language, for guests who do not understand English.

In Washington, D. C., similar programs will be disseminated by another company named Hotelevision in two large hotels, the Sheraton-Park and the Shoreham.

There seems little doubt that other installations will be made very soon in all the larger hotels in the US. It is anyone's guess how many million old and new TV sets will thus be connected and interconnected in the near future.

The companies mentioned above have their plants either in the hotels or at outside quarters. In either case, they run their ½-inch-diameter coaxial cable to the hotels' master antennas for the necessary connections.

Of importance to these new broadcasters is the fact that, inasmuch as they do not utilize a radio frequency, they are not affected by FCC regulations. Presumably this may not always be the case in the future. Conceivably, if closed-circuit television becomes a nationwide big business in years to come, some Federal regulations may inevitably come about.

When the new closed-circuit TV broadcasters tapped the hotels for their new service, the major facilities were already in existence—all that was required was to connect the coaxial cable. Yet there is waiting the infinitely larger market—*the public at large*. How can this *well paying* market be tapped in the future?

While the cost of conduits and installing coaxial cable would be astronomical if a separate cable were to run to every home and every apartment individually, yet to be an economic success, such a TV system should not cost much more than the present system of electric light, gas or water lines. A number of "pay-Television" companies have tried various technical schemes to bring programs to subscribers. None has succeeded so far.

How will the housewife of the future shop via television in her supermarket or department store—a dream publicized by many forecasters for the past 50 years? From a technical viewpoint, there is nothing impossible about this. It can be done right now; it is eminently feasible—except for the fantastic cost.

The same thing is true of the writer's early Tele-theater. It, too, will become possible in the future.

How? The physical facilities are already in existence—but the technical problems have yet to be solved. Almost every home has a telephone service supplied by two wires. The same is true of the electric wire supply. The telephone companies, well aware of the television-via-wire service, have been working over that problem for several decades. Many patents are in existence, but the final breakthrough of phonovision has as yet to be realized. The chief obstacle so far has been to channel the necessary high frequencies over a pair of not too highly insulated wires. In other words, to eliminate the coax. Perhaps some semiconductor device will prove to be the key to the difficult problem.

Once the technical difficulties are solved, the economics will be solved automatically, too—even the billing of the closed-circuit TV service will be done by the telephone companies.

Will phonovision adversely affect broadcast television? Probably not in the slightest. It will simply be a an adjunct—a supplementary service to broadcast TV—both decisively have their own spheres of utility. —*H.G.*

Sun-tracking robot furnace uses servo amplifier

A robot furnace or a light-seeking (or sound-seeking) robot can be built around this transistor servo amplifier

By TOM JASKI

A SERVO SYSTEM IS ONE IN WHICH A mechanical position or motion is controlled by a small input signal which often includes some negative feedback. Some form of amplification is an essential element in any servo system. Most servo systems today use electronic servo amplifiers which can control relatively large mechanical motions and forces with very small input signals, or by corrective (feedback) signals supplied by the controlled elements.

A great many kinds of servo amplifiers operate on different amplification principles. But all basically function on the basis of a signal at the input derived from the action at the output—the so-called closed-loop system. See Fig. 1.

Whether you wish to build a light-seeking robot or track satellites with an antenna, or perhaps wish to follow the sun with a mirror furnace (as was my plan), you will need some form of servo amplifier. The one shown is about the simplest I could devise, yet it is reliable, versatile and inexpensive.

Fig. 2 shows a block diagram of the amplifier and power supply. In my case, the input signals were derived from two small solar cells for each of two motions. One is called a polar motion (rotation about an axis approximately parallel to the earth's axis). The other is a declination motion, which here meant primarily angle above the horizon.

Whatever you call it, one amplifier is needed for each motion. With two such amplifiers you can point an object (light-sensitive cell, microphone or what have you) in any direction you wish, depending only on the mechanical limitations of your system.

Circuitry

Fig. 3-a shows the circuit diagram of one servo amplifier (my complete system uses two amplifiers and one power supply), and Fig. 3-b the power supply. As you can see, the amplifier could not be much simpler. Each amplifier consists of three transistors per section, one potentiometer to balance the two halves and one polarized or differential relay. If you cannot obtain either a polarized or differential relay, two sensitive relays will do in its place,

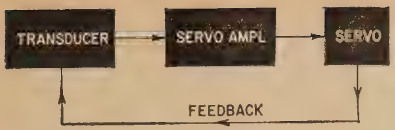

TRANSDUCER
SERVO AMPL
SERVO
FEEDBACK

Fig. 1—Basic closed-loop servo system.

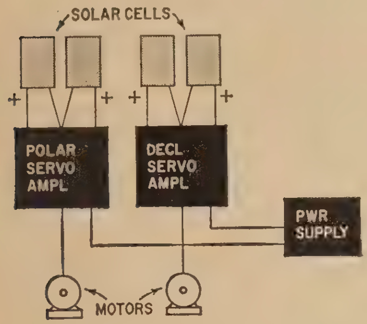

SOLAR CELLS
+
+
+
+
POLAR SERVO AMPL
DECL SERVO AMPL
PWR SUPPLY
MOTORS

Fig. 2—Block diagram of servo system used to track the sun.

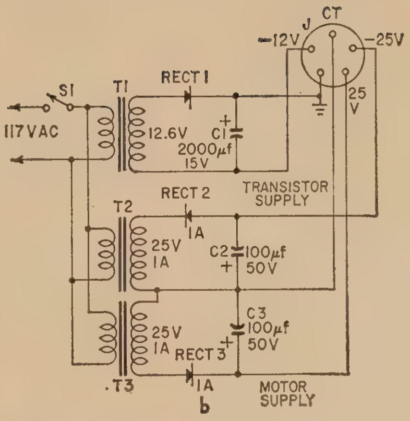
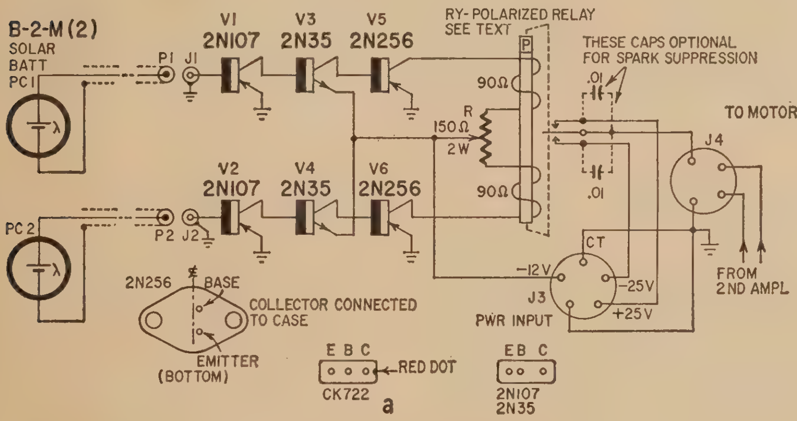

J
CT
−12V
−25V
25 V
S1
T1
RECT 1
117 VAC
12.6V
C1
2000µf
15V
RECT 2
TRANSISTOR SUPPLY
T2
1A
25V
1A
C2
100µf
50V
C3
100µf
50V
25V
1A
RECT 3
.T3
1A
MOTOR SUPPLY
b

Fig. 3-a (below)—Schematic of servo amplifier (two are required for author's system); b (above)—power supply schematic. Output voltage of T2 must suit the motors used.


B-2-M (2)
SOLAR BATT
PC1
V1
2N107
V3
2N35
V5
2N256
RY-POLARIZED RELAY SEE TEXT
P
THESE CAPS OPTIONAL FOR SPARK SUPPRESSION
P1
J1
90Ω
.01
R
150Ω
2W
TO MOTOR
J4
V2
2N107
V4
2N35
V6
2N256
90Ω
.01
PC2
P2
J2
CT
−12V
−25V
+25V
J3
PWR INPUT
FROM 2ND AMPL
2N256
BASE
COLLECTOR CONNECTED TO CASE
EMITTER (BOTTOM)
E B C
RED DOT
CK722
E B C
2N107
2N35
a

AMPLIFIER (Fig. 3-A)
R—pot, 150 ohms, 2 watts, linear taper
V1, 2—p-n-p transistors (2N107, CK722 or equivalent)
V3, 4—n-p-n transistors (2N35 or equivalent)
V5, 6—p-n-p power transistors (2N256 or equivalent)
PC1, 2—solar cells (International Rectifier B-2-M or equivalent)
RY—2-coil polarized relay, see text
P1, 2—phono plugs
J1, 2—phono jacks
J3—5 contacts (Amphenol 86-CP5 or equivalent, see text)
J4—motor jack, number of contacts depends on number of motors used
Above parts list is for one amplifier only.

POWER SUPPLY (Fig. 3-B)
C1—2,000 µf, 15 volts (Cornell-Dubilier A-0070 or equivalent)
C2, 3—100 µf, 50 volts
T1—primary, 117 volts; secondary, 12.6 volts at 0.6 ampere or more (Thordarson 26F67 or equivalent)
T2, 3—primary, 117 volts; secondary, 25 volts at 1 ampere (Stancor P6469 or equivalent)
S1—spst toggle
RECT 1—silicon rectifier, 100 ma or more
RECT 2, 3—2 500-ma silicon rectifiers in parallel (Sarkes Tarzian M500 or equivalent)
J—output jack, 5 contacts (Amphenol 78-S5 or equivalent
Cable to amplifier, 5 conductor with connectors on both ends (Amphenol 86-PM5 and 78-PF5 plugs or equivalents)
Chassis for amplifier(s) and power supply, line cord and miscellaneous hardware

as will be shown. Each amplifier chain is a direct-coupled p-n-p n-p-n p-n-p sequence, now familiar in transistor literature.

With each side of the amplifier receiving an identical signal, the output transistors pass the same amount of current (assuming both halves of the amplifier to be equal) and cause equal pull on both sides of the armature in the relay. As soon as one side receives more signal (as shown, or *less* signal with reversed input polarity), the output transistors pass different amounts of current through the relay coils. The armature is attracted to the side with the greatest current, closing a contact which causes a motor to turn in one direction. Closing the opposite contact would have turned the motor in the other direction.

If the input is a set of photocells or solar cells, and if your object is to have an equal amount of light on each cell, the correction to the system is applied at the input. (Rotating the cells will even the amount of light, causing the signals to become equal again and restoring balance.) Thus if the light moves away, as the sun does, and more light falls on one cell than the other, the system will follow the moving light.

If the input is some other system of voltage-producing elements, these must also be balanced by the motor to make the system come to rest.

The photos show the amplifiers and power supply and one of my input cells. The construction of this cell is shown in Fig. 4. Two solar cells are set side by side on one side of a dark box (painted flat black inside) with a narrow slot in the opposite side of the box. If the box is pointed directly at a light, the cells are lighted equally. As soon as the box is pointed directly at a light, one cell receives more light. This unbalances the system and causes servo action. If the cells had been mounted in a longer box, with greater distance from the slot, a smaller angle of rotation would have obtained the same result. Thus, by making the input enclosure larger, the system becomes much more sensitive. In my case the short boxes were good enough to make the system active in bright sunlight with only a fraction of a degree of rotation.

Adjustments

This servo amplifier contains one paradox. Its greatest advantage is also its greatest disadvantage. It is a very versatile system, with wide latitude for inequalities in transistors, components, relays and input signals. On the other hand, this makes the system a little troublesome to adjust. Setting it up will require some patience. Current through the output transistors will be greatest with no input signal.

To adjust, you can shunt each input with a 100,000-ohm resistor, for example. Then—assuming the relay is balanced—balance the amplifier by adjusting potentiometer R. If that fails, swap transistors in each stage progressively (turn off the power before

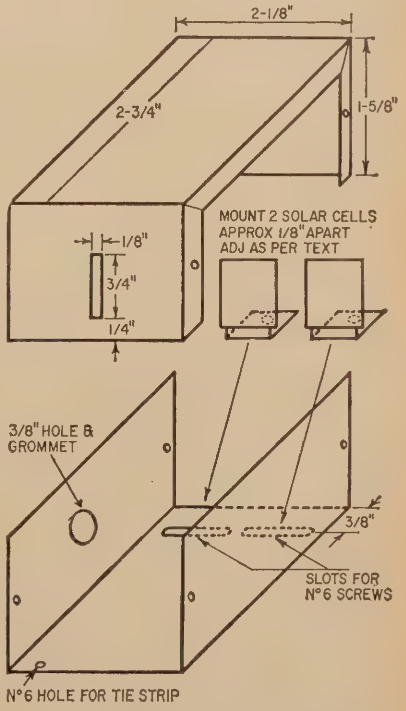

2-1/8"
2-3/4"
1-5/8"
1/8"
3/4"
1/4"
MOUNT 2 SOLAR CELLS APPROX 1/8" APART ADJ AS PER TEXT
3/8" HOLE & GROMMET
3/8"
SLOTS FOR N°6 SCREWS
N°6 HOLE FOR TIE STRIP

Fig. 4—Construction of solar-cell box.

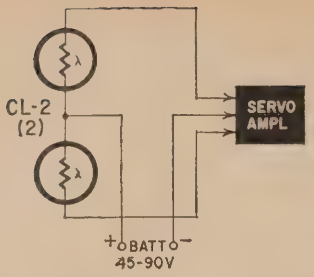


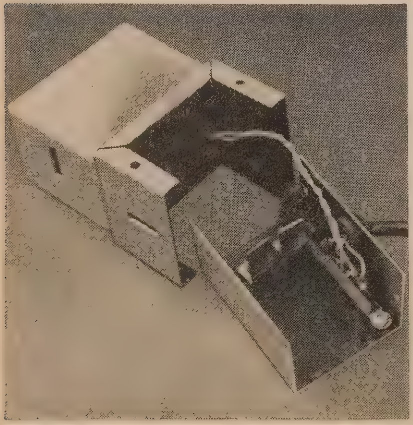
Fig. 5—Photocells and an external voltage source may be used.

withdrawing a transistor!), and try to balance the amplifier. If that also fails, there is always the relay adjustment. If you use the relays I indicate, there will be tremendous latitude in balancing, by adjusting the contact spacing or the holding magnets (or both) on each side. You can check initial relay balance by pushing the armature one way or the other. Even though the holding magnets may make the armature seem sticky on either side, it should return to center if the current is equal in the two coils. You can make sure of this condition by testing with the coils in series but opposing across a low-voltage source (3.5 volts will do).

[Western Electric 209 FJ relays were used by the author. These may be obtained as surplus from Red Johnson Electronics, 3311 Park, Palo Alto, Calif., or relay No. 255A at $16 per unit may be ordered from Metropolitan Telecommunciations, 9614 Dean St., Brooklyn 38, N. Y. These are two-coil polarized relays with a coil resistance of approximately 100 ohms.—*Editor*]

Each amplifier chain should give from 600 to 1,000 gain, depending on the condition of the transistors used. This means that with the relay shown, which requires a *difference* current of only 3 ma, a few microamps of difference at the input will activate the servo motor. Such a small current can be obtained from a set of photocells. Fig. 5 shows the diagram for a set of Clairex CL-2 photocells in place of the solar cells. The input could equally well be a pair of thermistors with a voltage source, but in that case the time required to heat or cool the thermistors might slow the system down considerably.

This brings up the point of *hunting*. If the system is made very sensitive, and, as a result, quick-acting, it might overshoot the balance point, backtrack to correct and overshoot in that direction, and then again go forward, and so on, oscillating back and forth. This is called hunting. Eventually the system would come to rest because of the mechanical friction represented by the motor if for no other reason. But *any* hunting is undesirable. It can be corrected by making the system less sensitive, or less rapid, by introducing electronic "friction." This is most easily done by shunting the relay coils with large capacitors.



Boxes housing solar cells.

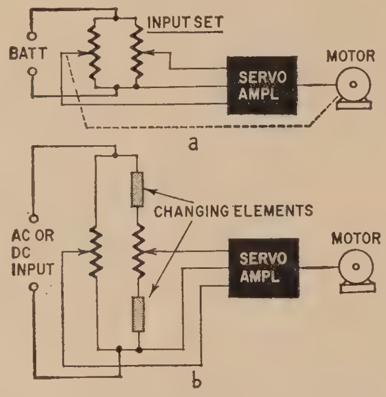


Fig. 6—Either mechanically unbalanced (a) or electronically (b) bridge may be used to supply input signals.

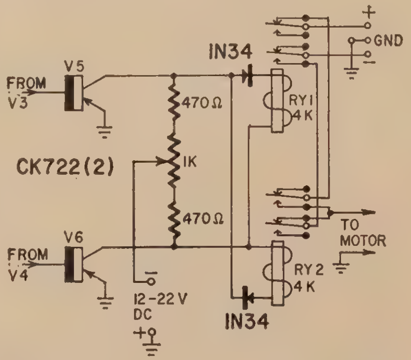


Fig. 7—Sensitive relays may be used in place of differential relay. Extra set of normally closed contacts is used to protect power supply in event both relays are energized.

The collector of the 2N256 is connected to the transistor case, so it must be insulated from the chassis.

Various inputs

Fig. 6 shows how the servo amplifier could be responsive to a voltage difference in a bridge circuit. If one of the bridge potentiometers is mechanically linked to the motor, the system will come to rest once the bridge is again balanced. The elements of the bridge can be any kind (other than the resistors shown) so long as they produce a dc imbalance, or an ac imbalance that can be rectified and filtered. If there is not enough filtering, the relay will chatter with the ac frequency. (I tried it!)

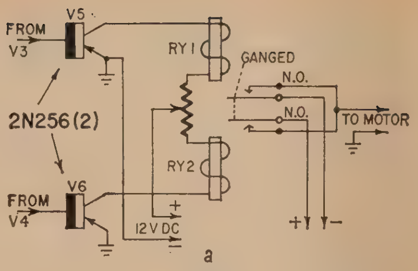
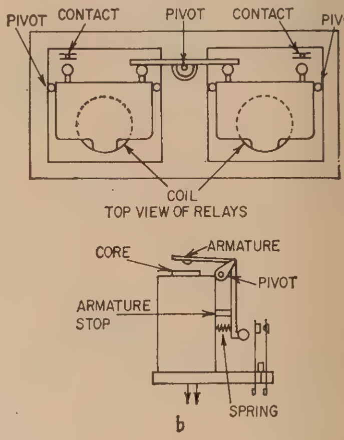


Fig. 8-a—Two relays may be used if armatures are linked (see text); b (below) — simplified sketch showing method of linking relay armatures.



To operate the motor with other than a polarized or differential relay, use the circuit shown in Fig. 7. Here two sensitive relays take the place of one polarized one, and the signal directivity is controlled by the diode rectifiers. An alternate is to use less sensitive relays, and simply circuit them as in Fig. 8-a, but the armatures then must be mechanically linked so that only one at a time can be attracted (Fig. 8-b).

To avoid overlap without the mechanical linkage in Fig. 7, each relay can energize a motor only if the other one is not energized. This can result in a "dead" spot if the relays have a great deal less holding than attracting current. Although differential relays and polarized relays also suffer from a "dead" spot, they are generally designed to have as little of this as possible. A single-coil polarized relay would be connected as shown in Fig. 9.

For more sensitive relays, the output transistors need not be power transistors. These were used because the

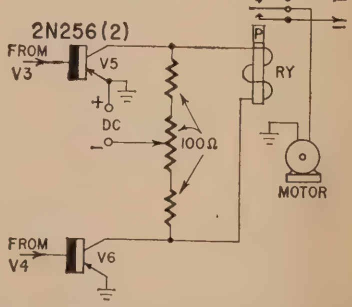
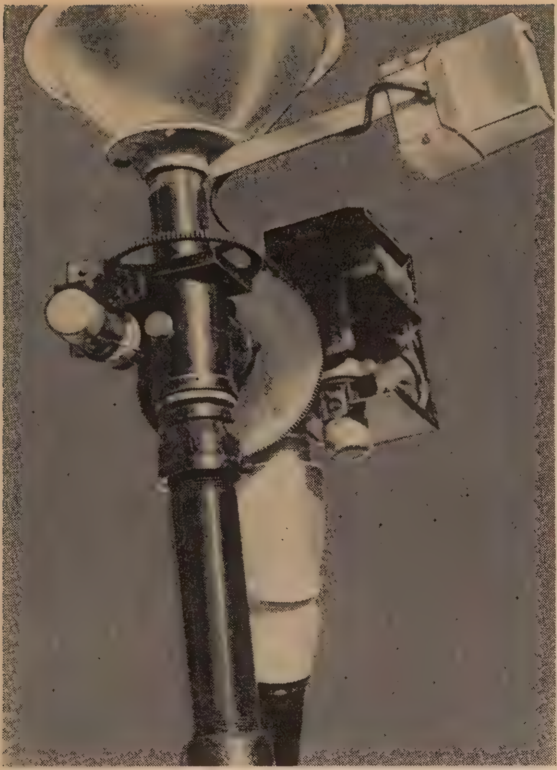
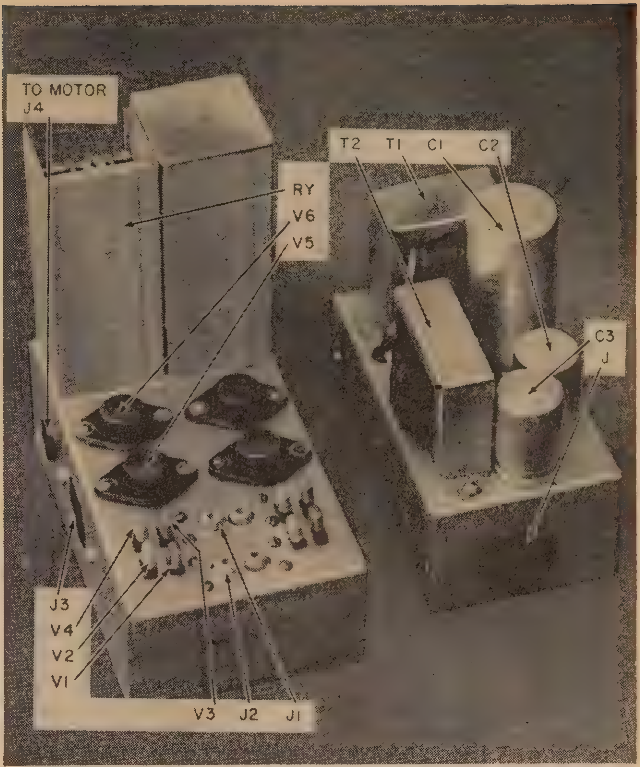


Fig. 9—A single-coil polarized relay may be used.



Motor and gear arrangement and solar cells mounted on rear of furnace.



Servo amplifiers (two) and power supply. Author eliminated transformer T3 by adding a second 25-volt winding to T2.

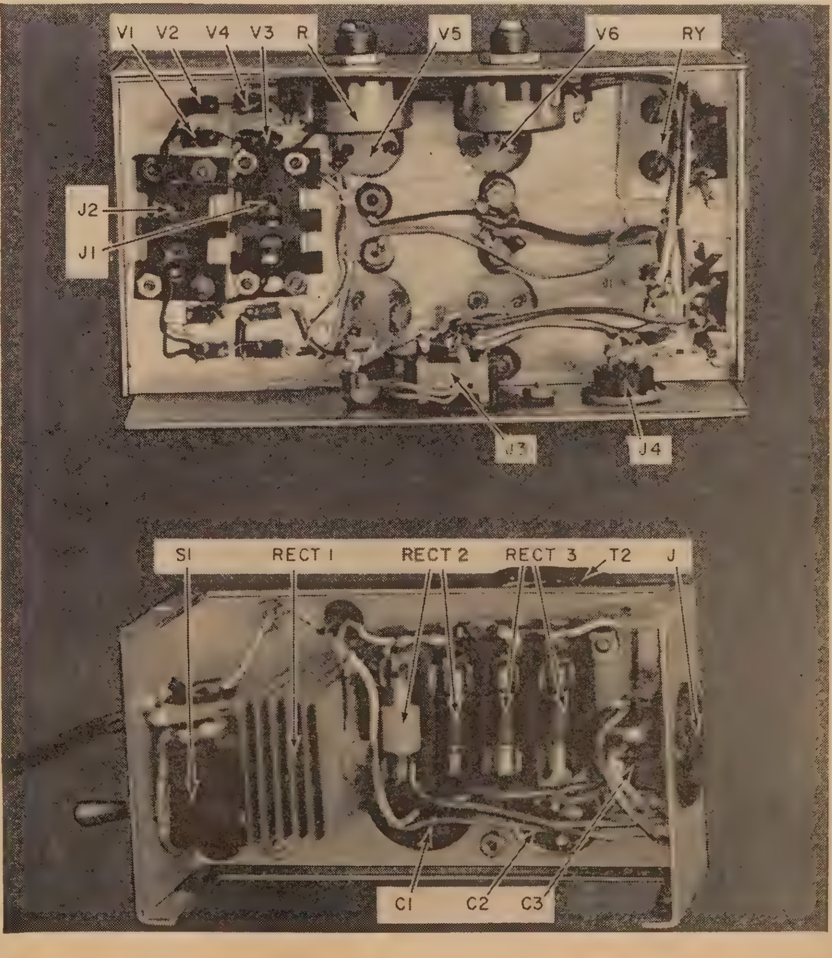
coil resistance is around 100 ohms. With sensitive high-resistance relays, the output transistors could be the same as the input transistors (2N107's, CK722's or equivalent).

Mechanical construction is of course totally uncritical, with one exception. The two sets of transistors should be exposed equally to any temperature change, in which case the system is almost entirely balanced for this factor. With the sun falling on only one part of the amplifier, you might find the system working without any input signal.

To protect the power supply, a male chassis connector should be used on the amplifier rather than the female one (J3) used in the original model.

Whatever your plans—robots, sun follower, heliograph, bridge balance or followup system, wherever you need a servo amplifier, this one will very likely fill the bill. With all the ways of compensating for differences in transistor characteristics, it can be built with inexpensive transistors. Very economically, in other words. If in the last analysis you still have difficulties solving the balance problem, resistors in the base connections of the transistors help a great deal. Their values will depend on the inequality of your transistors. The larger the resistors, the more sensitivity you sacrifice. This does not matter too much. Unless you hope to track stars (requiring much more sensitivity than this unit can provide), there is enough to spare for most purposes. END

Underside of power supply and amplifiers. Selenium rectifier was used in author's unit because it was readily available. Parts and layout of second amplifier are same as amplifier No. 1.



circuits for FM stereo

By **NORMAN CROWHURST**

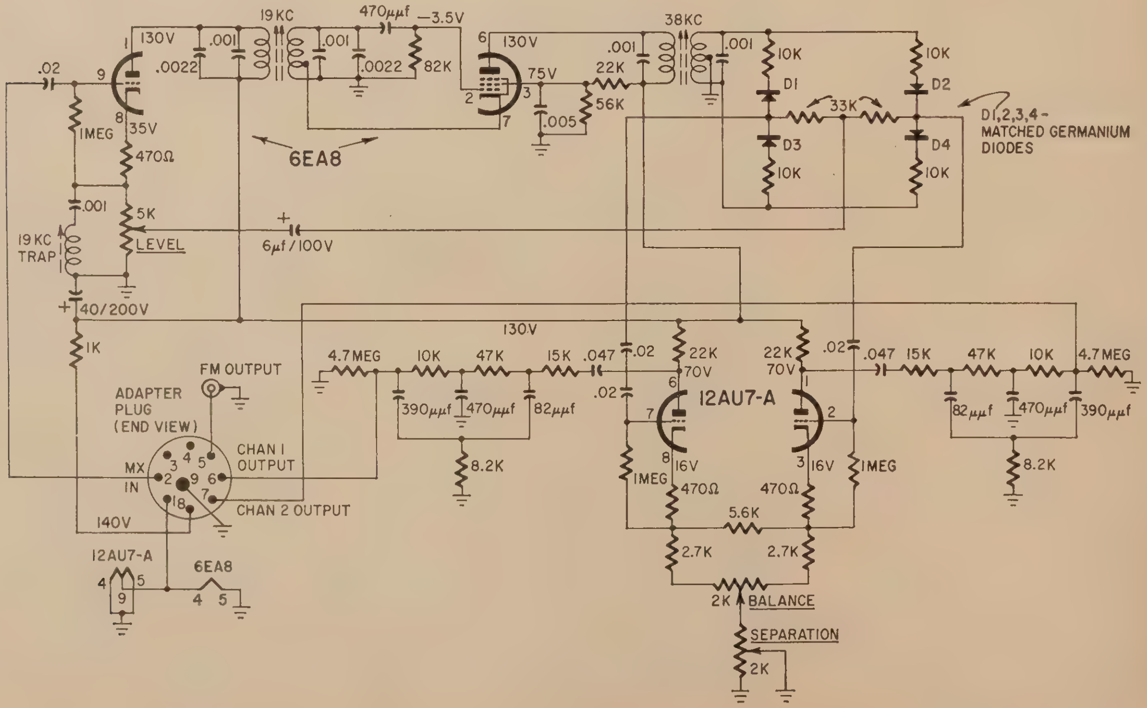
What makes that FM stereo equipment work?

In the coming months RADIO-ELECTRONICS will cover every important or unusual circuit used for FM stereo. We will tell exactly how they are arranged and exactly how they operate. Detailed descriptions will accompany each schematic.

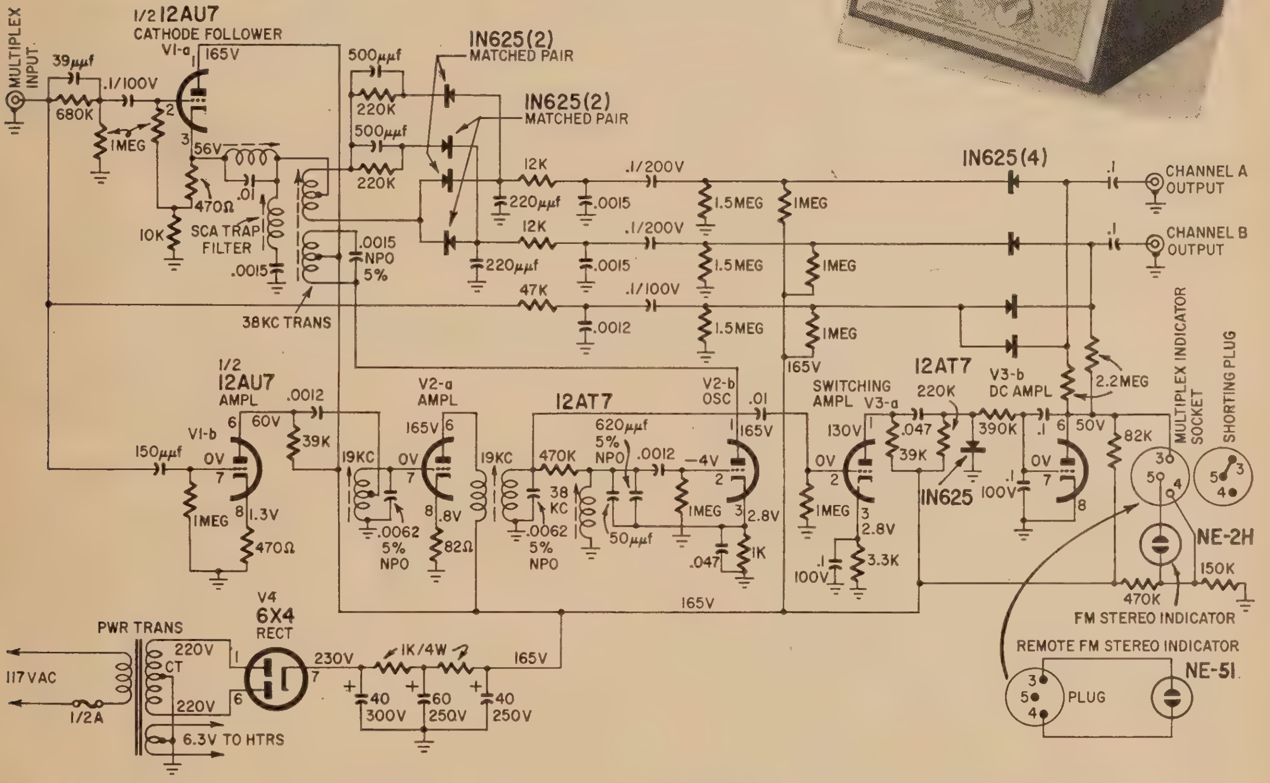
Our primary purpose is to show the many different forms taken to make FM stereo possible. This month circuits used by Sherwood, Pilot, Knight and Lafayette are presented. Others will appear in succeeding issues.

THE SHERWOOD CIRCUIT USES A REFINED FORM of switching. Like the others, the diodes attenuate the channel momentarily "unwanted", by about 18 db. This eliminates the diode characteristics from the performance figures. The cathode-follower triode with 19 kc tuned in its plate is a conventional input. A 19-kc oscillator uses cathode, grid and screen of the pentode section, while the plate doubles to produce 38 kc, which is transformer-coupled to the switching bridge. A 19-kc trap across the cathode resistor of the follower eliminates any residual 19 kc from the composite, which is then fed to the center of the switching bridge.

The attenuation of the channel in which the diodes are momentarily conducting (by the instantaneous phase of 38 kc) is set very precisely by the 33,000- and the two 10,000-ohm resistors. The separation and balance adjustment in the cathode circuit of the two output tubes then produces virtually a perfect null at the plates, for left in right channel and vice versa. These plates feed through twin-T filters to remove 38-kc switching components and provide correct de-emphasis.


19KC
470μμf
-3.5V
38KC
130V
.001
.0022
82K
.001
22K
75V
56K
.005
10K
D1
D2
D3
D4
33K
D1,2,3,4 - MATCHED GERMANIUM DIODES
.02
1MEG
35V
470Ω
6EA8
.001
5K
LEVEL
19KC TRAP
6μf/100V
40/200V
1K
4.7MEG
47K
15K
.047
22K
70V
390μμf
470μμf
82μμf
8.2K
12AU7-A
16V
5.6K
2.7K
2K
BALANCE
SEPARATION
FM OUTPUT
ADAPTER PLUG (END VIEW)
MX IN
CHAN 1 OUTPUT
CHAN 2 OUTPUT
140V

BOGEN
THE FISHER
PILOT
MULTIPLEX ADAPTER
Stereo EICO


MULTIPLEX INPUT
1/2 12AU7
CATHODE FOLLOWER
V1-a
165V
39μμf
.1/100V
680K
1MEG
56V
470Ω
10K
.01
SCA TRAP FILTER
.0015
38KC TRANS
500μμf
220K
500μμf
220K
.0015
NPO
5%
IN625(2)
MATCHED PAIR
IN625(2)
MATCHED PAIR
12K
.1/200V
220μμf
.0015
1.5MEG
1MEG
12K
.1/200V
220μμf
.0015
1.5MEG
1MEG
47K
.1/100V
.0012
1.5MEG
1MEG
IN625(4)
.1
CHANNEL A OUTPUT
.1
CHANNEL B OUTPUT
1/2
12AU7
AMPL
V1-b
.0012
60V
39K
150μμf
0V
1MEG
1.3V
470Ω
V2-a
AMPL
165V
19KC
0V
19KC
.8V
82Ω
.0062
5%
NPO
12AT7
470K
38 KC
.0062
5%
NPO
620μμf
5%
NPO
.0012
-4V
50μμf
1MEG
V2-b
OSC
.01
165V
2.8V
.047
1K
165V
165V
SWITCHING AMPL V3-a
12AT7
130V
0V
1MEG
.047
39K
2.8V
3.3K
.1
100V
220K
IN625
390K
.1
100V
V3-b
DC AMPL
50V
0V
2.2MEG
82K
MULTIPLEX INDICATOR SOCKET
SHORTING PLUG
NE-2H
470K
150K
FM STEREO INDICATOR
REMOTE FM STEREO INDICATOR
PLUG
NE-51
V4
6X4
RECT
PWR TRANS
117VAC
1/2A
220V
CT
220V
6.3V TO HTRS
230V
1K/4W
165V
40
300V
60
250V
40
250V

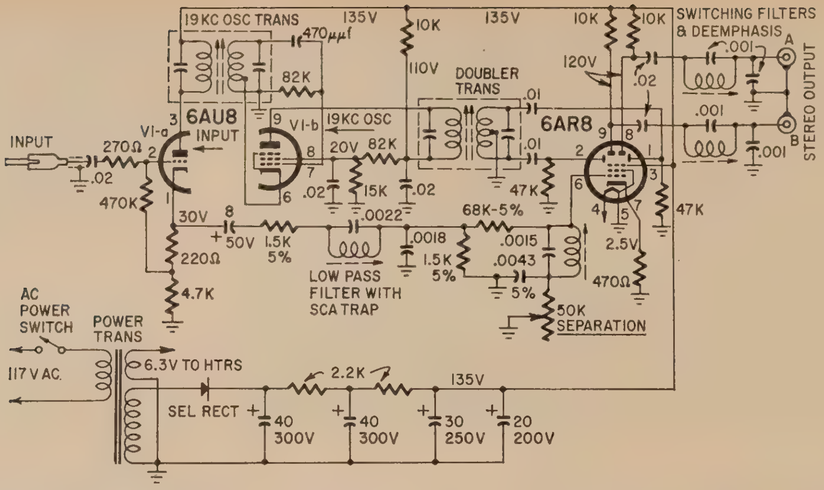
PILOT'S MODEL 200 USES SWITCHING WITH AN important difference. The cathode follower is fed with a high-frequency compensated divider. At the same time an amplifier stage feeds the 19-kc tuned amplifier that synchronizes the 38-kc oscillator. The 19-kc also feeds the switching amplifier which rectifies it for the dc amplifier controlling the relay.

In the earlier version of this circuit, the relay in the plate circuit of V3-b was mechanical. This has been changed to the solid-state circuit shown. A bias of three-fifths of B-plus is placed on the three lines isolated by 0.1-μf blocking capacitors by 1- and 1.5-megohm resistors. In monophonic (no 19 kc) the plate of V3-b is less positive than the lines, so the top two diodes are nonconducting, isolating the stereo channels from the output, while the bottom two are conducting, making a connection (for audio purposes) directly through the 47,000-ohm resistor.

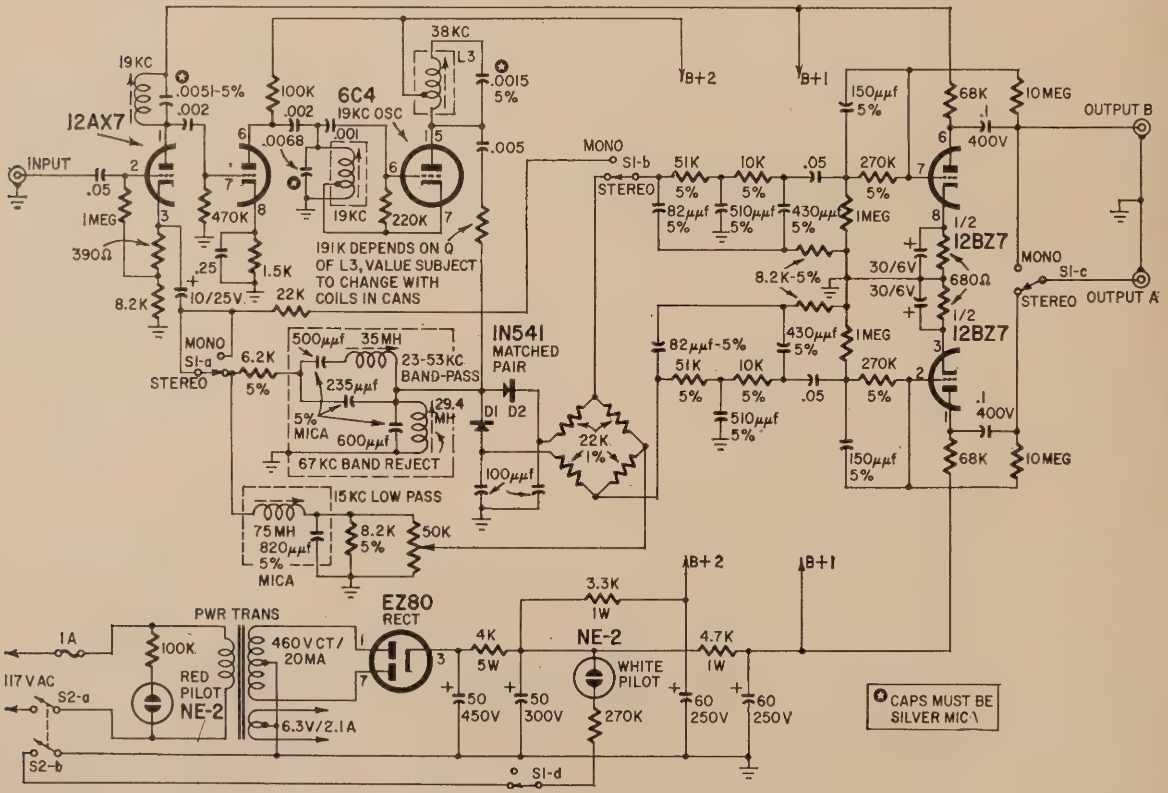
In stereo, the 19 kc makes the plate of V3-b more positive, so the top two diodes conduct and the bottom two don't. Now stereo channel connections are made, and the monophonic connection is open. This change in voltage also operates the neon indicator. The regenerated 38-kc is fed to the double-wound transformer whose secondary (and primary) has a center tap.

The composite from the input cathode follower feeds through the SCA rejection filter to the secondary center tap of the 38-kc transformer. The two 220,000-ohm resistors, each shunted by 500 μμf, maintain a charge close to the instantaneous peak value of 38 kc. Thus the matched pairs of diodes each conduct for only a short period near the peak of the 38 kc in one direction. When each conducts, it lets a sample of the composite fed in at the center tap through to the channel connected to that diode junction.

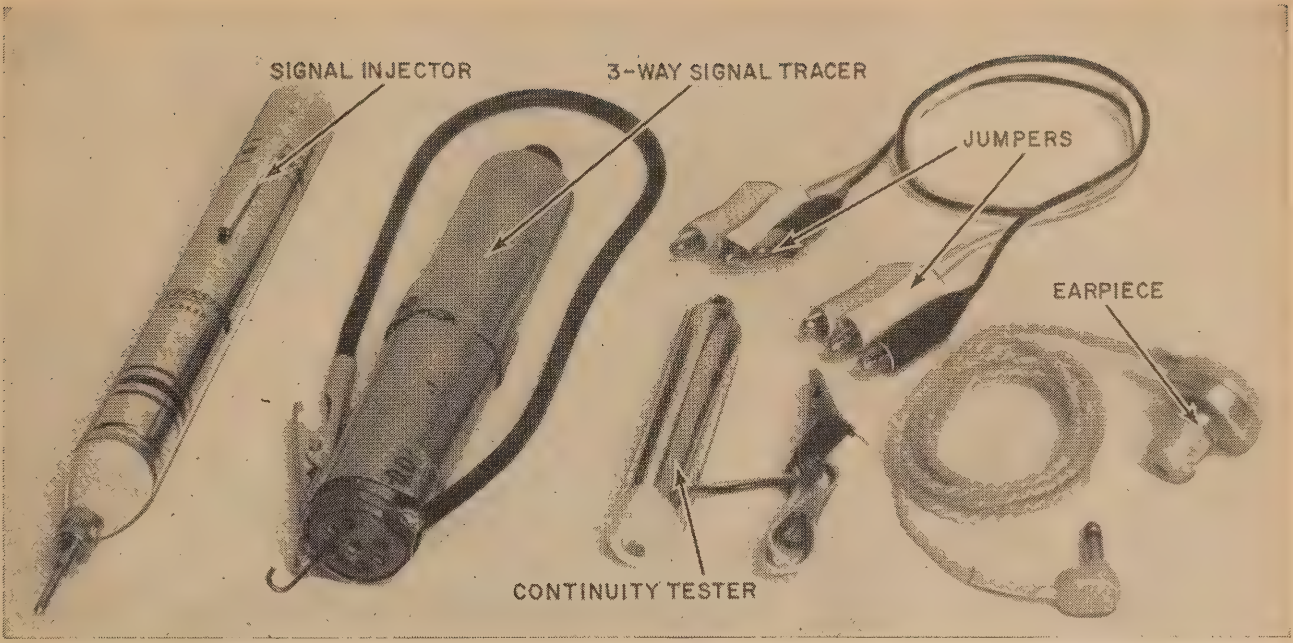
Where other switching circuits deliver half the composite waveform, on a time-division basis, to left and the other half to right, this circuit delivers just a short-time peak of each, when the 38-kc *modulation* (coming in from the transmitter, as distinct from the regenerated subcarrier) is *at* the point on left or right waveform, as the case may be. This avoids the reduction in L — R as compared with L + R inherent with normal switching circuits, and so does not need a separation adjustment to compensate for it.


19KC OSC TRANS
135V
470μμf
10K
135V
10K
10K
SWITCHING FILTERS & DEEMPHASIS
.001
A
STEREO OUTPUT
82K
110V
DOUBLER TRANS
120V
.02
.01
6AU8
V1-a
INPUT
9
V1-b
19KC OSC
INPUT
270Ω
.02
20V
82K
6AR8
.001
.01
B
.001
15K
.02
.02
47K
470K
30V
.0022
68K-5%
47K
+50V
1.5K 5%
.0018
.0015
2.5V
220Ω
1.5K 5%
.0043
470Ω
LOW PASS FILTER WITH SCA TRAP
5%
4.7K
50K SEPARATION
AC POWER SWITCH
POWER TRANS
117 V AC.
6.3V TO HTRS
2.2K
135V
SEL RECT
40 300V
40 300V
30 250V
20 200V

THE KNIGHT SELF-POWERED KN-MX ADAPTER uses an input stage that is cathode follower for all but the 19-kc pilot, which is tuned in the plate and coupled to a 19-kc oscillator, using screen, grid and cathode. This gives an input impedance of more than 5 megohms. Composite stereo from V1-a's cathode is fed through a filter to remove SCA subcarrier and a further filter that partially shapes sidebands to the grid of a beam-switching 6AR8. The plate circuit of the tube used as a 19-kc oscillator doubles frequency and feeds the beam switching electrodes with push-pull 38-kc. The plate circuits of the 6AR8 include filters to remove switching frequency and deemphasis.


38KC
L3
.0015 5%
19KC
.0051-5%
.002
100K
.002
6C4
19KC OSC
B+2
B+1
150μμf 5%
68K
10MEG
OUTPUT B
12AX7
.0068
.001
.005
.1 400V
INPUT
.05
1MEG
MONO
S1-b
51K
10K
.05
270K
STEREO
5%
5%
5%
470K
19KC
220K
82μμf 5%
510μμf 5%
430μμf 5%
1MEG
1/2 12BZ7
390Ω
191K DEPENDS ON Q OF L3, VALUE SUBJECT TO CHANGE WITH COILS IN CANS
30/6V
MONO
S1-c
.25
1.5K
8.2K-5%
680Ω
8.2K
10/25V
22K
30/6V
STEREO
OUTPUT A
MONO
S1-a
500μμf
35MH
1N541 MATCHED PAIR
430μμf 5%
1MEG
1/2 12BZ7
STEREO
6.2K 5%
23-53KC BAND-PASS
82μμf-5%
235μμf
51K
10K
270K
29.4 MH
D1 D2
5%
5%
.05
5%
5% MICA
600μμf
22K 1%
510μμf 5%
.1 400V
67KC BAND REJECT
150μμf 5%
68K
10MEG
100μμf
15KC LOW PASS
75MH
820μμf 5% MICA
8.2K 5%
50K
B+2
B+1
3.3K 1W
PWR TRANS
EZ80 RECT
1A
100K
460V CT/ 20MA
4K 5W
NE-2
4.7K 1W
117V AC
RED PILOT NE-2
S2-a
50 450V
50 300V
WHITE PILOT
60 250V
60 250V
6.3V/2.1A
270K
CAPS MUST BE SILVER MICA
S2-b
S1-d

THE LAFAYETTE LT-200 ADAPTER RETURNS TO the matrixing concept. It uses half a 12AX7 as cathode follower, with the 19 kc tuned at the plate. Input impedance is about 10 megohms. The follower divides to feed the 15-kc low-pass filter (for L + R) and a 23- to 53-kc band-pass filter, with 67-kc rejection. Output of the latter is rectified by diodes D1 and D2 in opposite phase, to produce L — R and R — L. These outputs are combined in a matrixing bridge with L + R (after a separation adjustment in the L + R channel) to give L and R. The subcarrier is regenerated by a 19-kc oscillator (6C4) with 38-kc tuned plate circuit to pick off the doubled frequency. This 38 kc is fed into the output from the bandpass filter. Each channel feeds through a twin-T circuit to an amplifier stage with voltage feedback. Mono–stereo switching bypasses filters and uses the left-channel output amplifier on mono, paralleling the output jacks so both are the same.



industrial technician's Pocket Kit

7-piece service kit includes signal tracer, signal injector, continuity tester, jumpers and an earpiece

By LEO LAZARUS

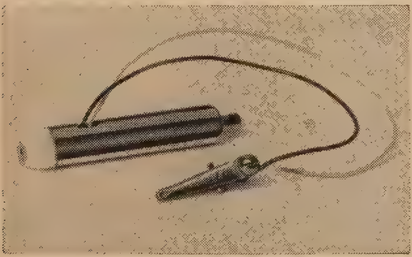
EVERY FACTORY ELECTRONIC TECHNICIAN can use a basic kit suited to his needs to avoid frustration in his work and to gain recognition as being competent in his field.

Contrast the usual way the electronic technician equips himself for his job as compared with skilled craftsmen in other fields. They have to provide an extensive range of tools at considerable expense to themselves. Compared with them, "our" man arrives at his job empty-handed. Yet by the very nature of his own skill he can provide himself, at minimal cost, with aids that are just as useful to him as the chisel to the carpenter or the calipers to the machinist.

Despite the small amount of money involved, very few technicians use these devices on their jobs though many of them have similar gadgets for home experiments. There seems to be an axiom in the electronic field—what the firm does not provide, do without.

How will this tool kit be useful? Very rare is the company which has an abundance of test equipment. Having worked in different plants on the production of equipment for home entertainment, industry and government, I have yet to find anything but shortages. This condition becomes especially acute when one works in the home consumer section of the industry. The pattern goes somewhat like this:

The firm plans a new production run. The pilot models have been made, tested, modified, tested again, and pronounced satisfactory. The unit goes into mass production, and the call goes out for more technicians. Now there is a sudden increase in the number of people who want to use the scopes and meters which were already in short supply. But this is not all.



This little flashlight doubles as a continuity checker.

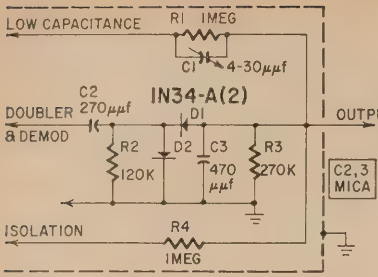
What you need

When there is multiple hiring usually some inept or inexperienced personnel are acquired. Thus, after waiting in line for the multimeter, you get it with a blown fuse. And all you wanted it for was to test for a short! Why not have a simple continuity checker of your own? It will save your time and sanity. And most important, it will be there when you need it!

There are the numerous times when you want to jump, ground out or temporarily hook up a component. I always see these jobs done with solder and iron. In a busy shop, jumper leads are never to be found. If there ever were any, they long since found their way to the lab. Carry your own jumpers; in fact, carry three! They are as useful as a third hand.

You get a dead set from the production line. All tubes are lit, B-plus is

The completed signal injector.



R1, R4—1 megohm
R2—120,000 ohms
R3—270,000 ohms
All resistors ½ watt, 10%
C1—4 - 30 µµf trimmer
C2—270 µµf, mica
C3—470 µµf, mica
D1, D2—1N34-A
Case—See text

Fig. 1—Signal-tracing probe has low-capacitance, doubler and demodulator, and isolation probe functions.

there, and the obvious possible shorts check out. Find the dead stage by injecting a signal and tracing it through. My signal injector is a transistorized multivibrator probe built into the body of a Winchester Traveller penlight. The 3,000-cycle audio square wave provides rich harmonics high into the rf range at the flick of a switch. When I want to hear the signal, I just clip on to an appropriate point with a hearing-aid type phone. My earphone is so sensitive that the multivibrator output can be heard directly at the probe tip. Because of this, I recommend a sensitive phone just so you'll know when the multivibrator has stopped oscillating. Some time in the future the battery will run down, even if the unit stops for no other reason, and a scope may not be handy. For most signal-tracing purposes, the cheapest phone will do.

To round out our tool kit, signal-tracing probes to suit the individual needs are a must. I made three probes in one body, with provision to add more if needed.

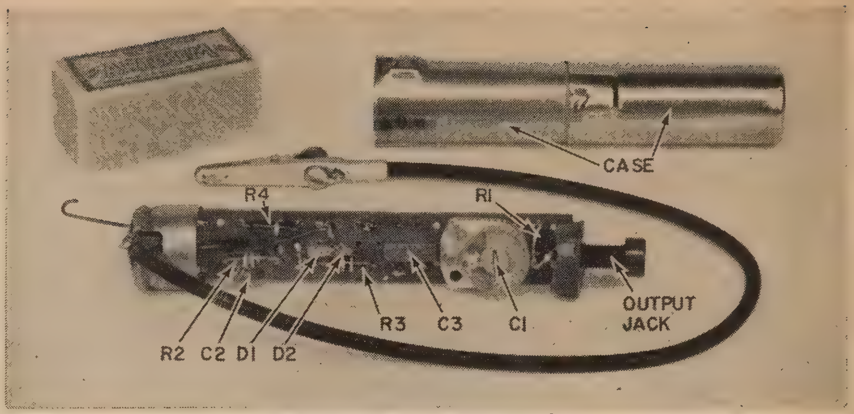
The signal tracer

All items can be made from easily obtainable commercial components, and a small drill is the only metal-working tool needed.

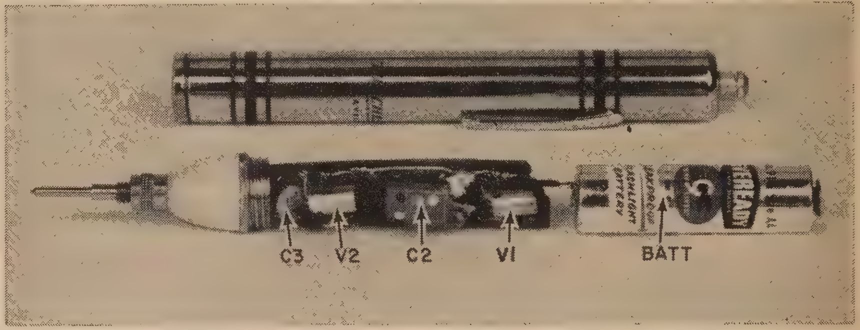
The signal-tracing probe (Fig. 1) is wired on a piece of perforated circuit board cut to fit snugly into a JAN type TS 102U03 tube shield. The probe housing is made from two of these shields placed end to end. Modify one shield by cutting the bent flange at the top in several places, and straighten it almost in line with the sides. Then push the second shield down over the straightened flange portions so it fits firmly. Finally, solder in two places.

Next take a JAN type 7-pin miniature tube socket with a shield base. Reverse the shield base (this is easy to do) so the socket pins are inside. Connect each probe input on the circuit board to a separate socket pin, and note which is connected to which.

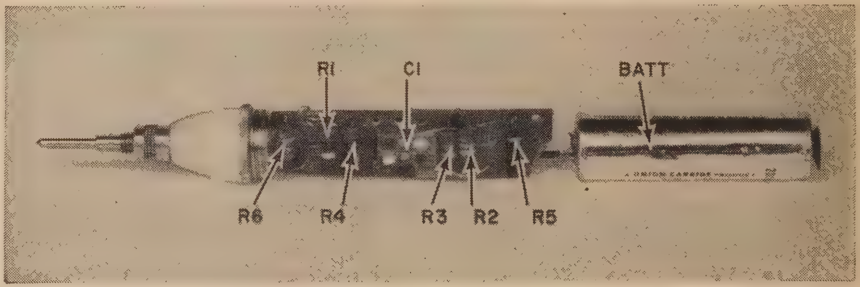
For the other end, cut from a piece of 1/16-inch plastic a disc a little smaller than the inside diameter of the probe housing. I used the top of the plastic cylinder that Ungar soldering tips are packaged in. Burn or drill a hole in the center of the disc to take a Johnson nylon tip jack. If the hole is slightly small, the jack will cut its own thread. Otherwise, use the nut to hold it in position. Now solder the common probe output to the jack terminal, and the probe is ready for assembly.



Inside the signal-tracing probe.



One side of the chassis inside the signal-injection probe.



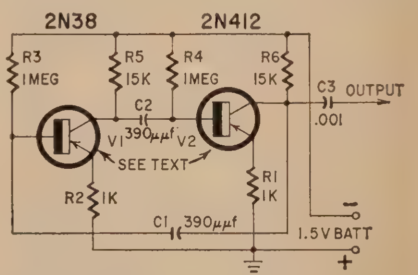
Most of the resistors and capacitors are on this side of chassis board.

Use one of the springs that are normally inserted in these tube shields in its normal position against its retaining flange, then place the circuit board with the disc against the spring. Now push on the housing over the shield base with the usual twist fit and everything will fit very firmly. The output jack will fit a meter or scope probe tip nicely.

For the multiprobe tip, cut about 1½ inches of a paper clip so that you take in the bend portion. The bend will give a ready-made hook to hook on to component leads, and also something to grip with the fingers when changing tip positions. The probe you want is selected by inserting the tip in the appropriate tube-pin socket. If the tip is a loose fit, tin it with solder until it fits firmly. Connect a ground lead to the mounting hole of the tube base, which in turn is connected to the probe circuit ground. Drill a hole opposite the variable capacitor in the low-capacitance probe so it can be adjusted.

Signal injector

The circuit of the signal injector is in Fig. 2. Any audio-frequency transistors should work in this circuit. I used the only two transistors I had on hand. The waveform is unbalanced, but that is not important here. If you have



R1, R2—1,000 ohms
R3, R4—1 megohm
R5, R6—15,000 ohms
All resistors ½ watt, 10%
C1, C2—390 µµf, mica
C3—.001 µf, ceramic
BATT—1.5 volts, AA penlight cell
V1—2N38 (see text)
V2—2N412 (see text)
Case—See text

Fig. 2—Circuit of the two-transistor signal injector.

to buy the transistors, get two of the same type. If the 2N38 is not available, use a 2N34, 2N109 or similar type.

As with the signal-tracing probe, I used easily obtainable commercial components for the probe housing and all other sections. I got a Winchester penlight and disassembled it. The bezel type nose takes a standard insulated phone-tip plug, which is the probe tip. Only ⅛ inch of the bakelite screw-on insulator acts as a retaining nut.

The circuit is wired on the same type of perforated board used for the signal tracer. The width is cut to fit the penlight case, and the length so the circuit board and one penlight cell fill the space normally occupied by two. Keep the circuitry in a little from each end of the board to allow for trimming. To use, clip one of your jumper leads to the pocket clip for a ground connection to the circuit under test.

I found that when the battery weakened to about 1.2 volts, the multivibrator would not start on closing the switch. I also found that momentarily grounding the junction of C1 and R3 never failed to start oscillations. To provide for this, I drilled a small hole in the penlight case opposite the junction of C1, R3. When the occasion arises, I just poke at the lead with any piece of wire I have on hand and the multivibrator never fails to start.

Those who do not want to go to the trouble of a perfect fit in the housing can solder a thin lead to the positive terminal of the battery from a ground point of the circuit. The multivibrator is always on, but so little current is drawn that battery life is long.

An alternative is to do what I did and use the penlight on–off switch to switch on the multivibrator. This entails soldering the round portion of a ground lug to the positive terminal of the battery to give a wider contact area and make sure the housing is in firm contact with the circuit ground when slipped over the circuit board.

Build the circuit breadboard style first to make sure your components work. With some transistors, 1.5 volts may not be enough to start the multivibrator oscillating. Check this by temporarily hooking in 3 volts. If it still does not work, recheck the wiring.

The earphone (Lafayette MS-260) has a .001-μf blocking capacitor (small disc type for compactness) in series with the hot lead, and alligator clips to clip on with.

The continuity checker is another penlight or a single-cell novelty light serving a dual purpose. As a flashlight it will always be valuable. For use as a continuity checker, drill a small hole in the case so you can insert two thin, insulated leads that can be fed through and soldered to the respective positive and negative points. Now when the other ends of the leads are stripped and touched together, they bypass the switch and the bulb lights. Some novelty lights are of odd shapes and provide plenty of room to run leads in.

This is my suggested service kit, and it is just a handful. END

LICENSE-FREE radio control

Check the FCC regulations; you'll find you can operate without a license

By DONALD L. STONER

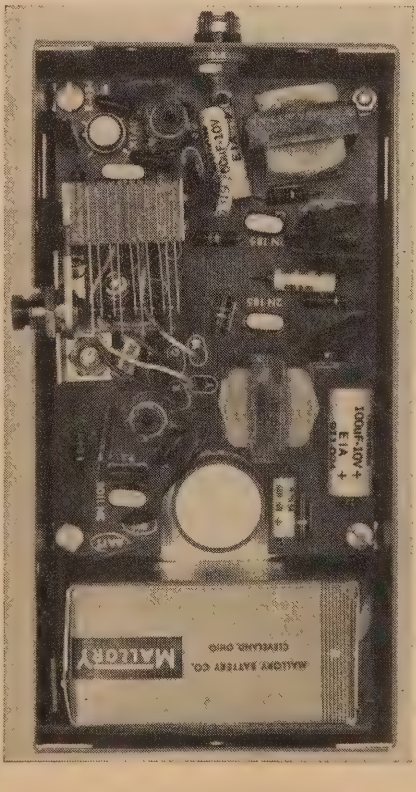
ALTHOUGH IT IS NOT GENERALLY KNOWN, you can operate a radio-controlled model *without a license*. Anyone who has taken the time to read paragraph 15.205 of "Part 15—Incidental and Restricted Radiation Devices" of the Federal Communications Commission Rules and Regulations will discover that a low-power *communications device* may operate between 26.97 and 27.27 mc (27.12 mc ±150 kc) provided it complies with the following requirements:

- The carrier of the device shall be maintained within the band 26.97 to 27.27 mc.
- All emissions, including modulation products below 26.97 or above 27.27 mc, shall be suppressed 20 db or more below the unmodulated carrier output.
- The power input to the final radio stage (exclusive of filament or heater power) shall not exceed 100 milliwatts.
- The antenna shall consist of a single element that does not exceed 5 feet in length.

The intended use is not specified and thus Part 15 radio-control equipment may be considered permissible. Note also that no specific channel assignments are made (subpart a) and that any frequency between the limits specified can be used. The carrier frequency could be "wedged" between two Citizens band channels where interference is at a minimum.

There is one other point which should be mentioned in connection with the rules and regulations: Part 15.208 (d) states, "The certificate may be executed by a technician skilled in making and interpreting the measurements that are required to assure compliance with the requirements of this part." Thus, if you are technically qualified to make the required measurements (second harmonic, modulation bandwidth, power input, etc.), you can build a transmitter or modify a commercial unit. No second-class radiotelephone license is required. However, if equipment is found to be operating improperly or in violation of regulations, then the certifying person may be called for a hearing before FCC examiners. If he is found to be *un*skilled in making and interpreting measurements required for certification, then he may be prosecuted.

Although the power input of equipment used under Part 15 is limited to 100 milliwatts (0.1 watt), this is adequate for up to 1-mile range. Radio-control transmitters are usually operated with a continuous carrier. Only the tone is pulsed to actuate a receiver escapement or relay. This system is more reliable since the carrier tends to override interfering stations. Experience has shown that battery-consuming high-power transmitters are not required since the model seldom goes



Inside the GW-30. This unit is about to be modified for license-free R/C use.

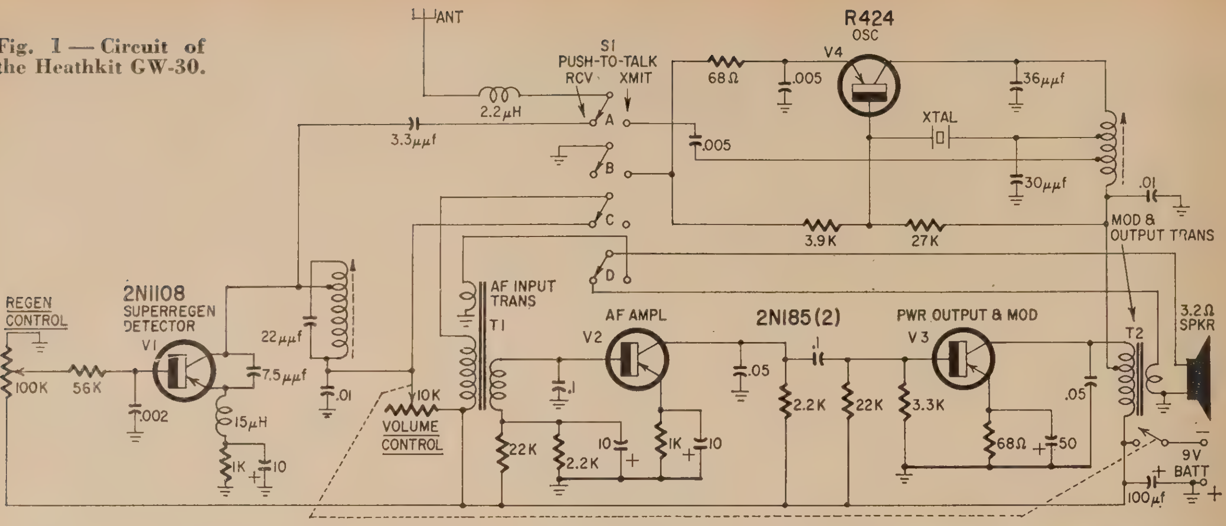


Fig. 1 — Circuit of the Heathkit GW-30.

more than ½ mile away. Modern transistor receivers are more selective and sensitive than their vacuum-tube predecessors. Completely transistorized receiver and transmitter systems are not only practical but are commercially available (Wen-Mac, etc.).

A Part 15 R/C transmitter

To prove that a low-power transmitter could be used for radio control, a Heathkit GW-30 Citizens-band transceiver was modified to work in conjunction with a transistor radio-control receiver, an F & M Electronics Pioneer model. The circuit of the GW-30 is shown in Fig. 1.

The modifications involve disabling the GW-30 receiver and inserting feedback in the modulator section to generate a tone. The transmitting frequency of the GW-30 need not be changed.

Here's how to modify the GW-30. Take the unit out of its leather case and remove the back panel. Lift the printed-circuit board from the case after removing the three screws that secure the chassis. Familiarize yourself with the location of the pushbutton switch contacts (Fig. 2 and the photograph). This switch is modified so the transmitter carrier comes on when the volume control–switch is turned on. Depressing the button, in the modified GW-30, then produces a tone rather than turning on the carrier.

It is easier to bend the switch contacts than to rewire the switch to do this. They may be straightened later if a return to the original operation is desired. Note the dotted lines in Fig. 2. Bend the fixed contact on section B up so it touches the moving contact. This completes the emitter circuit of transmitter transistor V4. Next bend the fixed contact on section C up. This breaks the primary circuit of T1 and disables the receiver. Do not modify section D. Finally, on section A, bend the upper fixed contact up to clear it from the moving contact. Bend the lower fixed contact of section A so that it touches the moving contact at all times. This connects the antenna to the transmitter section. Finally, the modulator is made to oscillate by introducing feedback.

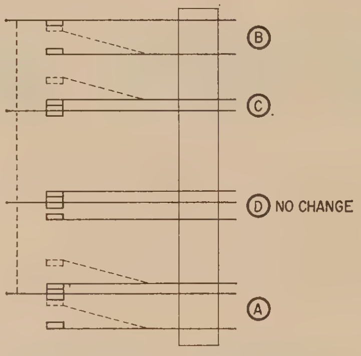


Fig. 2—Detailed view of the modified switch.

This can be done by reconnecting section D of the switch to tie the modulator output to the input. Locate the wires which connect section D to the speaker and T2. Reverse these two wires by "swapping" the connections from section D of the switch on the circuit board. Thus you can see that when they are connected in this manner, depressing the pushbutton connects the speaker winding on T1 to the speaker winding on T2. When this is done, the audio stages break into oscillation and tone-modulate the transmitter. This completes the changes to the unit and it can now be reassembled.

Although the modifications sound complicated, it actually takes more time to tell how to make them than to do the job.

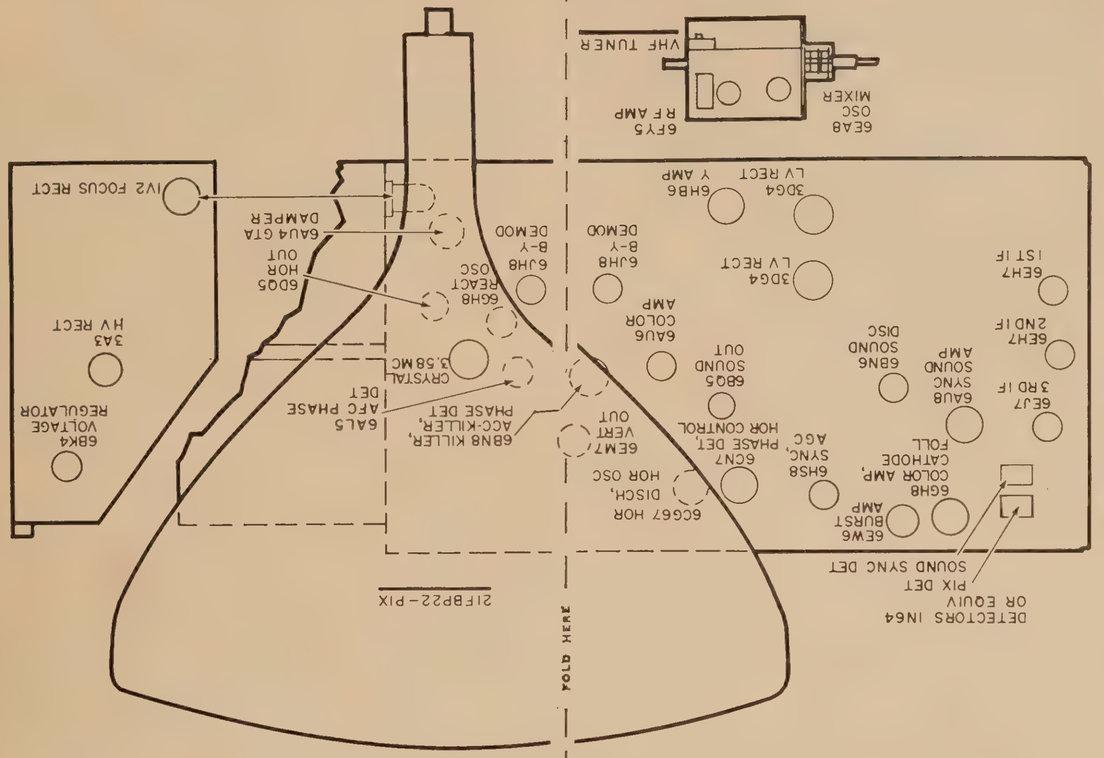
OFF
VOL
HEATHKIT

The GW-30 handheld CB transceiver.

To test the conversion, check the transmitter by energizing a radio-control receiver in a model on the ground. It should actuate the control surface reliably over a distance of 1,000 feet and more when the model is held aloft. In operation, the transmitter is energized, before launching the model, by turning on the volume control. As soon as the model is 50 to 100 feet from the transmitter and has enough elevation, the control button can be depressed. The exact sequence of operation will depend on the escapement used. END

"CENSORED"

may be a horrible word. But when applied to mail order tube advertising in Radio-Electronics, it protects readers from receiving seconds or rejects, when they believe they are buying new tubes. All mail order tube ads must specifically state the condition of the tubes offered for sale . . . new or used, seconds or rejects.


VHF TUNER
6FY5 RF AMP
6EA8 OSC MIXER
1V2 FOCUS RECT
6AU4 GTA DAMPER
6DQ5 HOR OUT
3A3 HV RECT
6BK4 VOLTAGE REGULATOR
6AL5 AFC PHASE DET
3.58MC CRYSTAL
6GH8 REACT OSC
6JH8 B-Y DEMOD
6BN8 KILLER, ACC-KILLER, PHASE DET
21FBP22-PIX
6JH8 B-Y DEMOD
6HB6 Y AMP
3DG4 LV RECT
3DG4 LV RECT
6EH7 1ST IF
6EH7 2ND IF
6EJ7 3RD IF
6AU6 COLOR AMP
6BQ5 SOUND OUT
6BN6 SOUND DISC
6AU8 SYNC SOUND AMP
6EM7 VERT OUT
6CN7 HOR CONTROL PHASE DET, AGC
6HS8 SYNC, AGC
6GH8 COLOR AMP, CATHODE FOLL
6CG7 HOR DISCH, HOR OSC
6EW6 BURST AMP
SOUND SYNC DET
PIX DET
DETECTORS IN64 OR EQUIV

FOLD HERE

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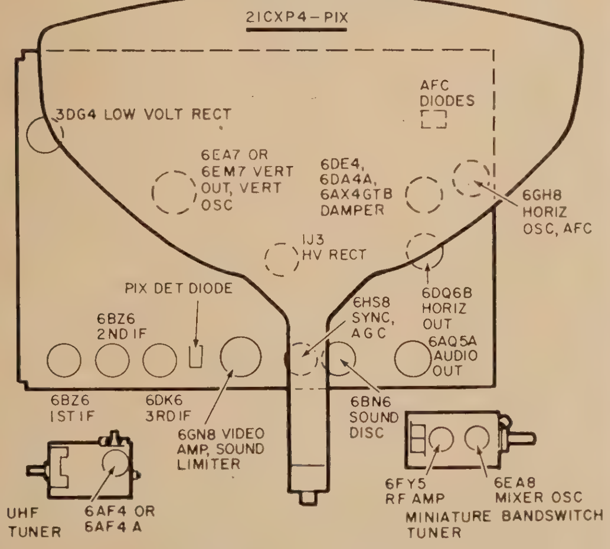
CUT HERE

COLOR CHASSIS 29JC20, 29JC20Q

TRIM HERE AFTER FOLDING

CHASSIS 16G21, 16G21Q


21CXP4-PIX
3DG4 LOW VOLT RECT
AFC DIODES
6EA7 OR 6EM7 VERT OUT, VERT OSC
6DE4, 6DA4A, 6AX4GTB DAMPER
6GH8 HORIZ OSC, AFC
1J3 HV RECT
PIX DET DIODE
6BZ6 2ND IF
6HS8 SYNC, AGC
6DQ6B HORIZ OUT
6AQ5A AUDIO OUT
6BZ6 1ST IF
6DK6 3RD IF
6GN8 VIDEO AMP, SOUND LIMITER
6BN6 SOUND DISC
UHF TUNER
6AF4 OR 6AF4 A
6FY5 RF AMP
6EA8 MIXER OSC
MINIATURE BANDSWITCH TUNER

HOW TO FOLD Fold the top down and back, keeping the cover facing you. Then trim the right and left edges. Now staple the booklet along the vertical center fold, about ¾ inch from the top and bottom. Now fold from left to right, keeping the cover facing you. Trim a fraction of an inch off the top and trim the bottom to size and you're finished. You now have another useful piece of service data, exclusive with RADIO-ELECTRONICS.

Radio-Electronics

TUBE LAYOUTS IN TV SETS

Compiled by Larry Steckler, Associate Editor

ZENITH
1961-1962

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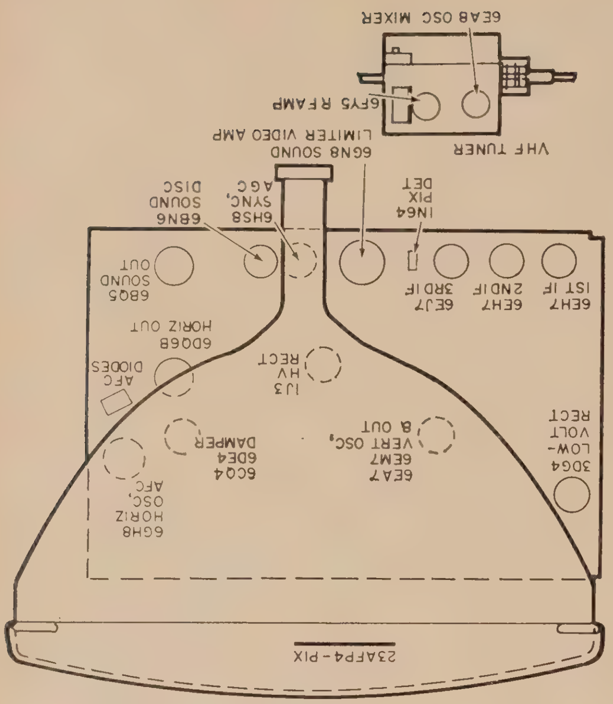
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1N64 PIX DET
6HS8 SYNC, AGC
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6BQ5 SOUND OUT
6EH7 1ST IF
6EH7 2ND IF
6EJ7 3RD IF
6DQ6B HORIZ OUT
AFC DIODES
1J3 HV RECT
3DG4 LOW-VOLT RECT
6EA7 6EM7 VERT OSC, & OUT
6CQ4 6DE4 DAMPER
6GH8 HORIZ OSC, AFC
23AFP4-PIX

CHASSIS 16H28, 16H28Q

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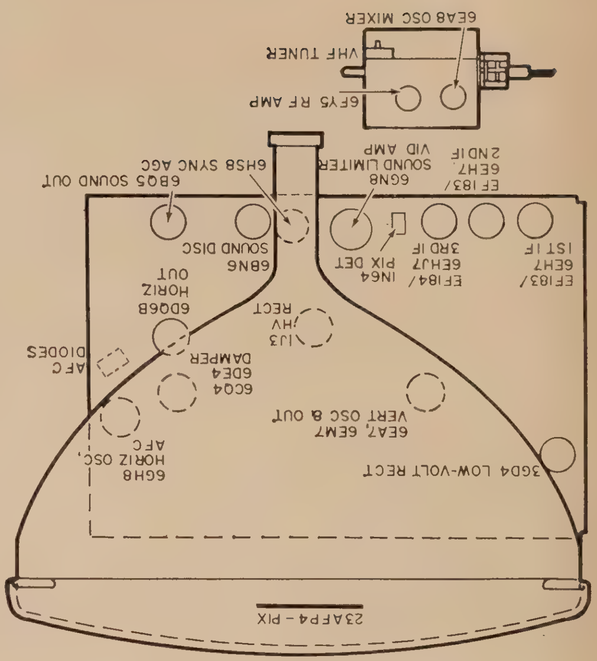
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EF183/ 6EH7 1ST IF
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1J3 HV RECT
AFC DIODES
6CQ4 6DE4 DAMPER
6EA7, 6EM7 VERT OSC & OUT
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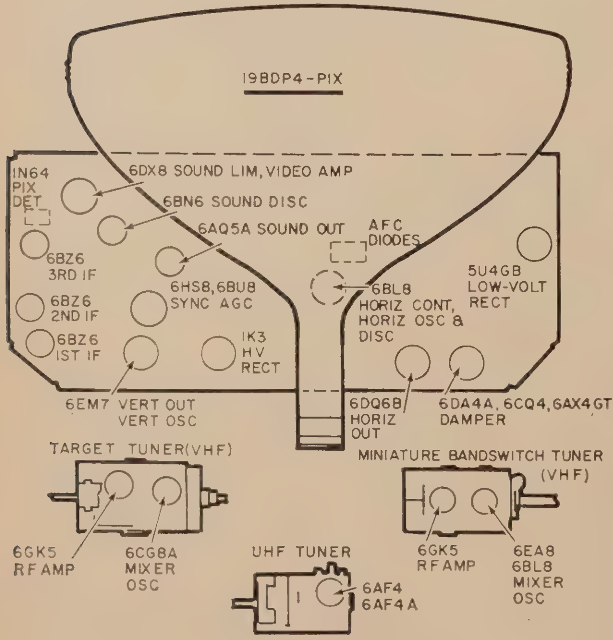
CHASSIS 16J28QS

CHASSIS 16J20, 16J20Q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6DX8 SOUND LIM, VIDEO AMP
6BN6 SOUND DISC
6AQ5A SOUND OUT
AFC DIODES
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6BZ6 2ND IF
6BZ6 IST IF
6HS8, 6BU8 SYNC AGC
6BL8 HORIZ CONT, HORIZ OSC & DISC
5U4GB LOW-VOLT RECT
1K3 HV RECT
6EM7 VERT OUT VERT OSC
6DQ6B HORIZ OUT
6DA4A, 6CQ4, 6AX4GT DAMPER
TARGET TUNER (VHF)
6GK5 RF AMP
6CG8A MIXER OSC
UHF TUNER
6AF4 6AF4A
MINIATURE BANDSWITCH TUNER (VHF)
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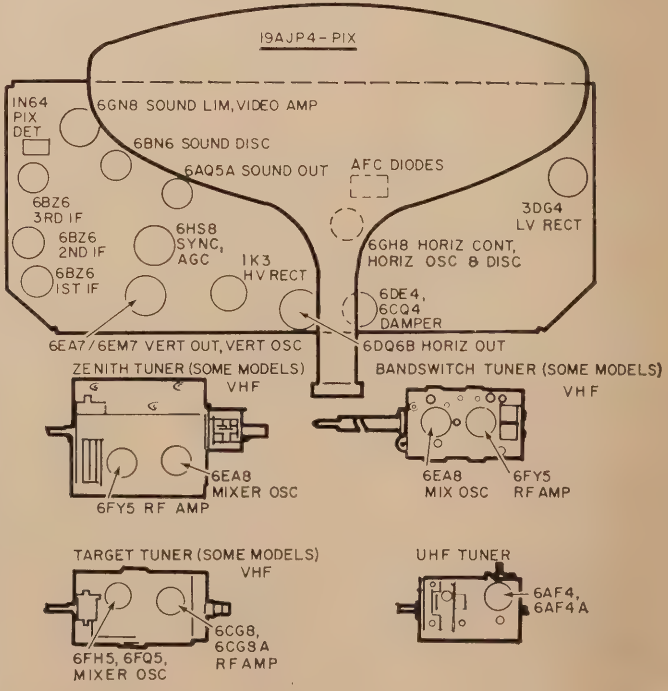
6EA8 6BL8 MIXER OSC

CHASSIS 16G27, T, Q, QT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6BZ6 IST IF
6HS8 SYNC, AGC
1K3 HV RECT
3DG4 LV RECT
6GH8 HORIZ CONT, HORIZ OSC & DISC
6DE4, 6CQ4 DAMPER
6EA7/6EM7 VERT OUT, VERT OSC
6DQ6B HORIZ OUT
ZENITH TUNER (SOME MODELS)
VHF
6EA8 MIXER OSC
6FY5 RF AMP
BANDSWITCH TUNER (SOME MODELS)
VHF
6EA8 MIX OSC
6FY5 RF AMP
TARGET TUNER (SOME MODELS)
VHF
6FH5, 6FQ5, MIXER OSC
6CG8, 6CG8A RF AMP
UHF TUNER
6AF4, 6AF4A

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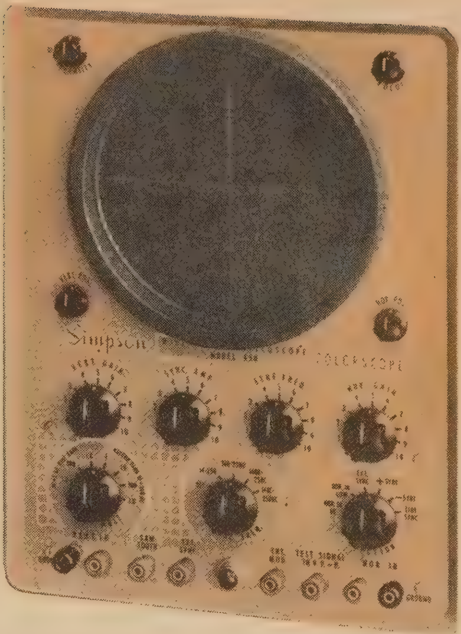
7

By ROBERT G. MIDDLETON

Power Measurements with your Scope

A scope will show you many things a wattmeter doesn't and will work where a wattmeter can't be used at all



HUNDREDS of important scope applications in electronics work are unknown in many shops. This is not surprising, simply because the field of electronics has become so large. Let us start with a few more basic applications.

A scope can be connected to show either the voltage waveform or the current waveform in a circuit. For example, Fig. 1 shows the appearance of the voltage and the current in a simple neon-lamp circuit.

What do these waveforms show? The current waveform (Fig. 1-b) shows that the neon lamp conducts over a part of the complete cycle. The horizontal line through the pattern is the zero-current level. While the spot is moving along this level, the neon lamp is not conducting.

We see that the lamp jumps suddenly into conduction from the zero-current level. There is a sudden tall spike of current when the lamp ionizes. Thereafter, a sine wave of current flows until the lamp extinguishes. The current is zero for a time; then the sequence is repeated through the negative half-cycle.

The voltage waveform (Fig. 1-c) shows that a clipped sine-wave voltage is dropped across the neon lamp. The resistance of the lamp is practically infinite until the moment of firing. At the instant the tube ionizes, its internal resistance falls suddenly to a low value. Although the current flow through the tube is changing, the voltage drop across the tube remains practically constant. This is an interesting property of gaseous conduction.

Note that a voltage spike precedes the clipped portion of the voltage waveform. In other words, the striking voltage is greater than the conduction voltage drop across the tube. We see from this why a current spike appears in the current waveform, preceding conduction.

Voltage vs current

Thus, we know that there are voltage waveforms, and that there are current waveforms. Another important type of waveform is the power waveform—a voltage vs current pattern. Let us see what this means.

If we have a load such as a motor connected to an ac line, it draws more or less real power from the line. An induction motor draws a lagging current. A synchronous motor draws a leading current. An ideal motor draws an in-phase current. A suitable combination of motors on a line is practically the same as an ideal motor. In-phase current is drawn from the line, and the power company is happy.

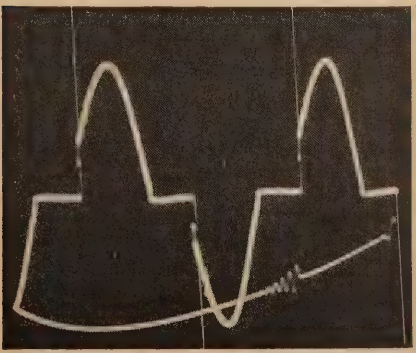
Let us look at Fig. 2. Here, the scope's vertical input terminals are connected across the line—line voltage is applied to the vertical amplifier. A small resistor, R, is connected in series with the line. The scope's horizontal input terminals are connected across the resistor—line current is applied to the horizontal amplifier.

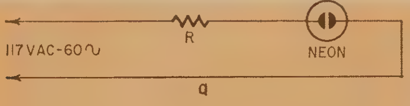
The load is a capacitor. A nearly circular pattern is displayed on the scope screen. In this arrangement, the pattern means that the current is 90° out of phase with the voltage. To put it another way, the current does no work. It merely surges in and out of the capacitor, back and forth in the line. All the power in the circuit is reactive power. The rule is: *If the power pattern is a circle, no real work is being done by the circuit.*

Next, let us look at Fig. 3-a. Here we have a resistive load R_L. It might be a bank of lamps, for example, or some device that "looks like" a resistor. The scope is connected as before—vertical deflection corresponds to line voltage, and horizontal deflection to line current.

We see a straight diagonal line on the scope screen in Fig. 3-b. This pattern tells us that there is 100% real power in the load. There is zero reactive power. All the current is doing work. It is converted completely into heat by the resistor. No reactive power is surging back into the line.

In many practical electronic configurations, both real power and reactive





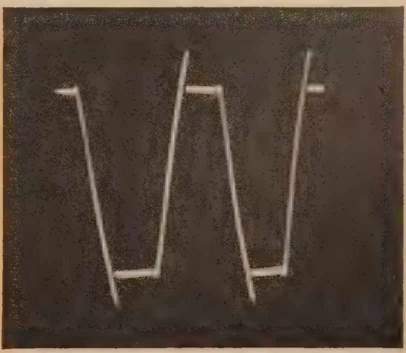


Fig. 1—A simple neon-lamp circuit (a) and its current waveform (left) which is seen when the scope is connected across resistor R. The voltage waveform (right) is seen when the scope is connected across the neon lamp.

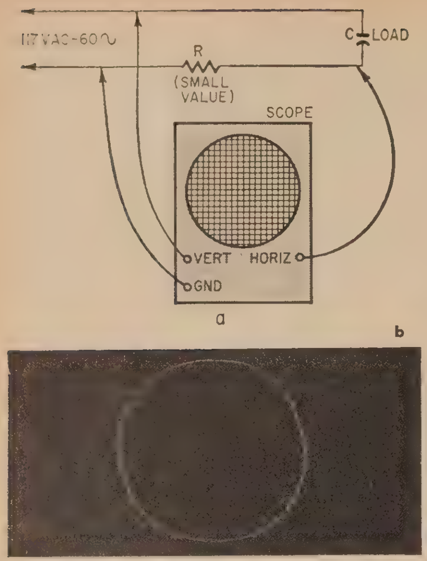


Fig. 2-a—Load across line is capacitor. Scope connected to show voltage vs current (power) waveform. b—Nearly circular pattern shows practically no real power is drawn from line by capacitor.

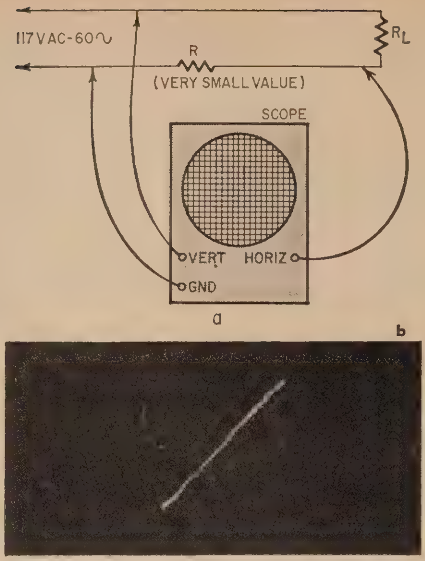


Fig. 3—Scope connected to check power in resistive load R_L (a) produces the straightline pattern (b) that shows 100% real power in the load.

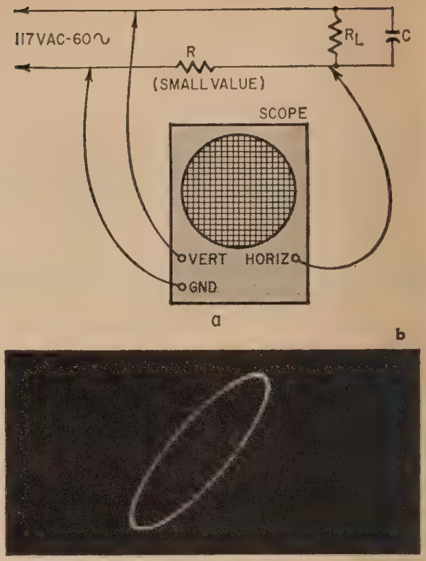


Fig. 4—This basic circuit (a) takes both real and reactive power from the line and produces an elliptical pattern (b).

power are present. In other words, the real power is doing work. The reactive power is merely taking current and returning the same current to the line. This situation is shown in Fig. 4. The current drawn by resistor R_L does work in heating the resistor. On the other hand, the current drawn by capacitor C is merely stored for a short time and then returned to the line. This surging current corresponds to reactive power.

This time the scope pattern is an ellipse. In other words, the pattern is between a line and a circle. *The amount of area in the ellipse, compared with the area in a circle, indicates the amount of real power compared with the reactive power.* If we choose, we can measure the vertical and horizontal deflections, to determine the power factor, and find the exact amounts of real and reactive power.

Non-sine-wave current

In many electronic circuits, a current sine wave does not flow when a voltage sine wave is applied. A rectifier tube, for example, changes a sine wave into a half sine wave. Thus, many scope patterns are not as simple as those discussed above.

Let us consider the simple power supply shown in Fig. 5. A scope is connected to show current flow into the circuit in terms of vertical deflection, and to show output voltage in terms of horizontal deflection.

Fig. 6 shows how the scope pattern indicates various circuit conditions. First of all, the patterns are not straight lines, and neither are they circles. We do not expect to see a circle because we know that the current is not a sine wave. Also, we do not expect to see a straight line because the filter capacitors would have to be tremendously large to have practically no reactance in the circuit.

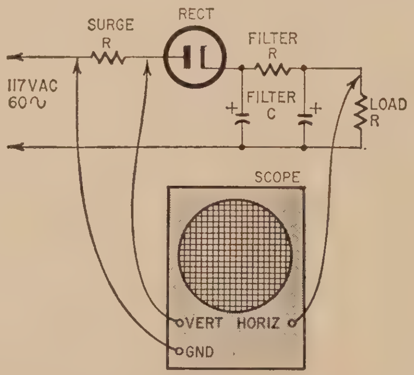


Fig. 5—Scope connected to check operation of a simple power supply.

Fig. 6-a is the normal waveform. It has a significant height, width and area. If the output filter capacitor has lost capacitance, its reactance increases and the ac voltage drop becomes greater. The pattern increases in width, and it encloses a larger area (Fig. 6-b). The line current is not changed appreciably, as shown by the pattern height.

Note the pattern in Fig. 6-c. The input filter capacitor is low in value. The voltage drop across the capacitor is increased. Or, we say that the ripple voltage is greater at the input of the filter—and this means that there will be a greater ripple voltage at the output of the filter. The scope shows more vertical and horizontal deflection, and a greater pattern area.

Wattmeter is no help

Here is an extremely important fact that the electronic technician must keep in mind: *A wattmeter test in this circuit is completely misleading.* In other words, a wattmeter does not read correctly unless the voltage and current are both sine waves. We know that the current is not a sine wave. Hence, we should never try to check such electronic circuits with wattmeters. A false read-

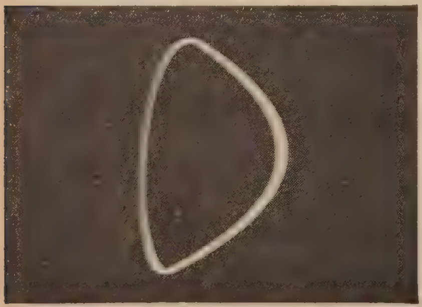
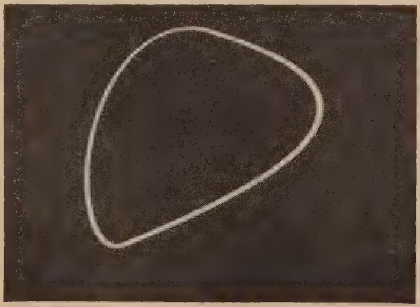
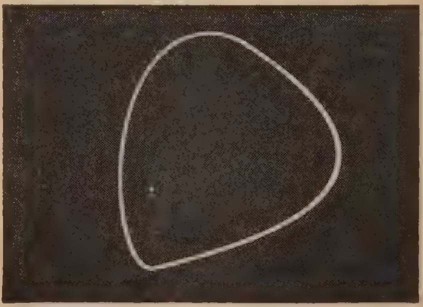


Fig 6-a—Pattern for normally operating circuit.



b—Pattern when output filter capacitor is low in value.



c—Pattern when input filter capacitor is low in value.

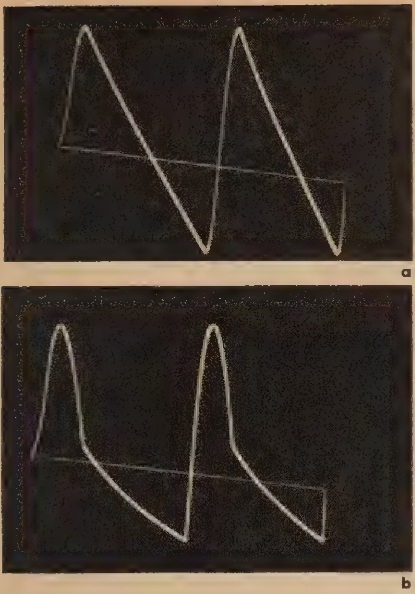


Fig. 7-a—Normal waveform across input filter capacitor. b—Distorted waveform is displayed when the input filter capacitor has low capacitance and a poor power factor.

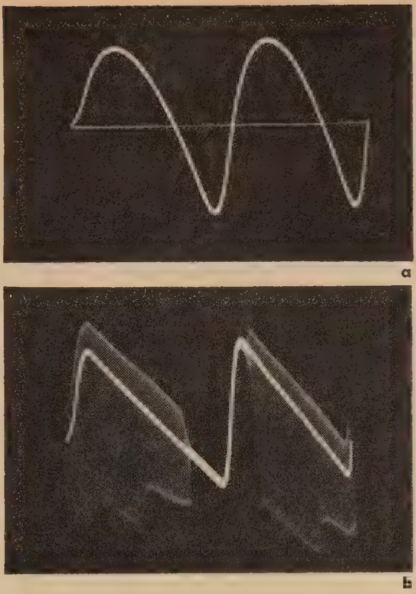


Fig. 8-a—Normal waveform across output filter capacitor in a radio receiver. b—Highly distorted waveform is displayed when the output filter capacitor has lost much of its capacitance and has a poor power factor.

ing is unavoidable.*

On the other hand, if we check a motor circuit or a lamp bank with a wattmeter, we read the real power in the circuit. The reading is correct because the load operates from a sine wave voltage and a sine wave current. Note that the wattmeter indicates only the real power in the circuit. An induction motor might be drawing considerable reactive as well as resistive current. The wattmeter shows only the resistive power. The wattmeter does not see the reactive power.

However, we can easily find the reactive power in such a motor circuit by supplementing the wattmeter reading with voltage and current measurements. Many service wattmeters also have current and voltage scales. Here is the basic principle: We measure the voltage and current in the circuit. For example, we might measure 100 volts and 1 ampere. Then, there are 100 volt-amperes in the circuit. Now, if the wattmeter reads 75 watts, 75 watts of real power are present. The 25 watts difference is reactive power (VARS—volt-amperes reactive), which merely surges in and out of the load, doing no real work.

Wattmeters must be used with great caution in electronic circuits. Whenever the voltage or current, or both has a nonsinusoidal waveshape, we cannot use wattmeters.* By the same token, we cannot use rms reading voltmeters and ammeters. This is why the scope is such a valuable tool in electronics work.

More waveforms

Now let us look at some other interesting waveforms found in a simple power supply. A simple test is made by connecting the scope's vertical input terminals across the input filter capacitor. We display the waveform in the ordinary manner using sawtooth sweep. Fig. 7-a shows the normal pattern compared with the distorted pattern (Fig. 7-b) displayed when the input filter capacitor is faulty (when it loses capacitance and develops internal resistance).

When a filter capacitor develops high internal resistance, it has a poor power factor. We can measure the power factor with a capacitance bridge, which will also show any capacitance loss which may have taken place. In other words, we confirm the scope test by disconnecting the capacitor and checking it on a bridge.

Next, let us connect the vertical input terminals of the scope across the output filter capacitor. Fig. 8-a illustrates the normal waveform compared with the highly distorted waveform (Fig. 8-b) displayed when the output filter capacitor is very low in capacitance and has a very poor power factor (high internal resistance). In addition to the distorted waveform, we see a periodic high-frequency oscillation riding on the pattern.

Where does the spurious high-frequency oscillation come from? In this example, we do not have a simple resistive load connected to the filter output. Instead, the filter feeds supply voltage to an ac–dc radio. With a faulty filter capacitor, normal bypassing (decoupling) is not accomplished. Instead, the receiver circuits break into spurious oscillation.

The beginner may judge the scope a mysterious and complicated instrument. However, it is really quite simple. It is only necessary to become familiar with reading distorted waveforms, so that we know what they mean. The best way to do this is to start with simple breadboard circuits or ordinary radio receivers which are operating unsatisfactorily. A little practice with the scope will open new fields of electronic savvy. END

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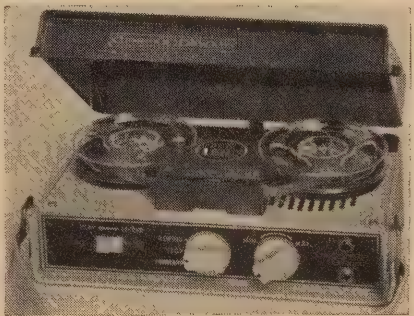
* A good electrodynamometer instrument will read correctly on such waveforms. However, this type of wattmeter is seldom found in service shops.

New Idea in Tape Recorders



THE REMARKABLE THING ABOUT THIS miniature tape recorder–playback machine is that no tape speed is specified. The reason is simple—there is no fixed tape speed! The unit operates without a capstan, the tape is pulled by the takeup reel. When that reel is nearly empty, the speed may be down to about 2 ips. As it fills up, the speed increases to about 5 ips.

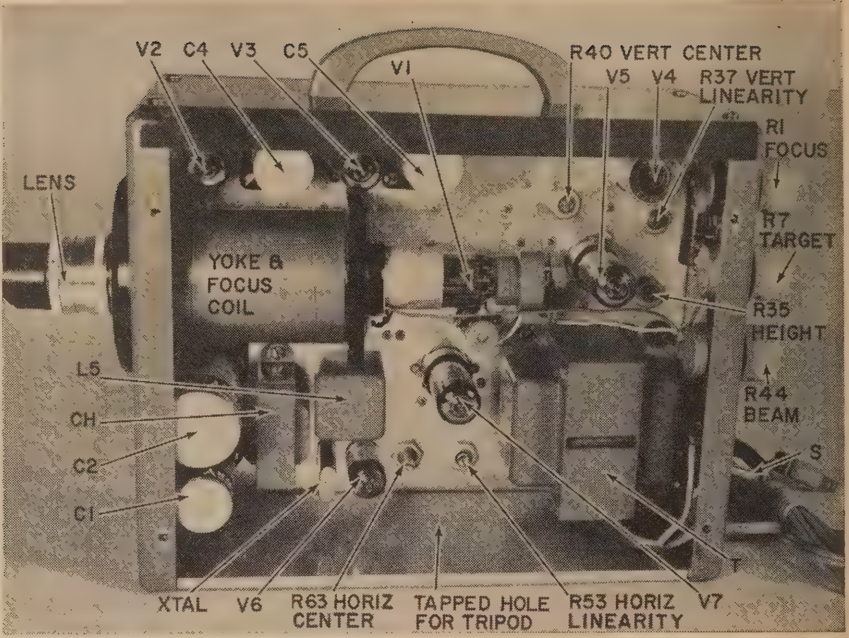
Since corresponding portions of the tape are played at the same speed (approximately) in recording and playback, this speed variation is not noticeable when tape is played back on the same machine. Although two machines were not available for testing, it would seem that tapes could be played back almost equally well by a similar machine; any individual variations would probably be too small to be easily detectable.

Used for voice, the little unit performs very satisfactory. No attempt was made to check it on music—it does not look to be designed as a hi-fi device.

The amplifier has four transistors (the last two in a push-pull output stage). The equipment operates off two size-C flashlight cells, one for the motor and one for the amplifier.

Several recorders of this type are being sold in the U. S. The one shown here carries the brand name Continental.

COVER STORY



TV Camera You Can Build

Six-tube instrument at far lower cost than commercial units

By W. E. PARKER

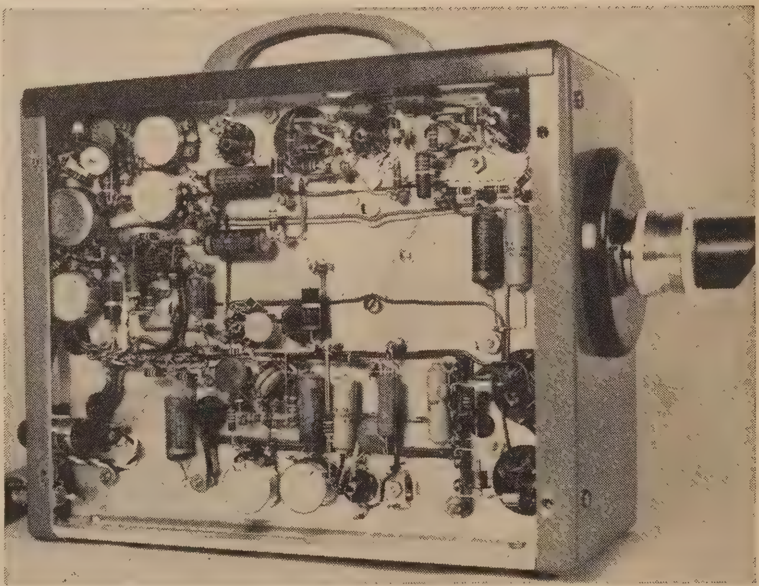
SIMPLIFIED CIRCUITRY AND COMMERCIALLY available vidicon camera deflection components now make it possible to build your own closed-circuit TV camera.

The single-unit self-contained TV camera has the essentials of a miniature television station. To form a complete closed-circuit (wired) television system, only the addition of a modern TV receiver is required.

The output signal of the camera is tuned in on a TV set the same way as a standard TV broadcast station is tuned. A single cable connects the camera output to the receiver antenna terminals. No other connections to the TV set are required. The modulated rf signal may be received on channels 2 through 6, depending on how the camera is adjusted. **NO ATTEMPT at broadcasting or other uses of the radio-frequency waves for radiated transmissions may be made without express permission being obtained from the FCC.**

Applications

There are many uses for the TV camera presented in this article. They are limited mostly by the user's imagination and the available light necessary for a satisfactory picture. From observing junior in his crib to the salesman knocking at your front door, there are limitless possibilities for your own private television system.



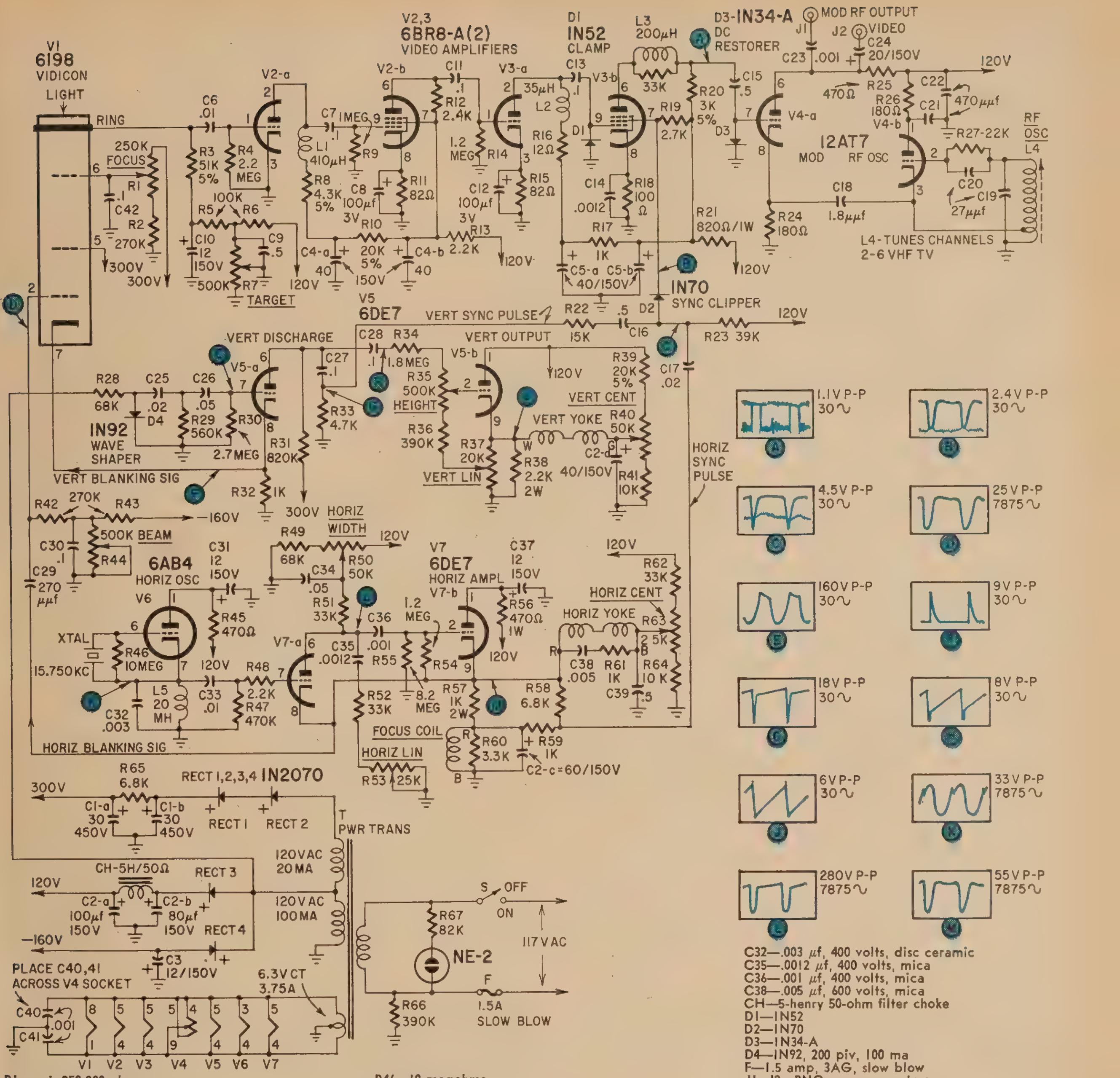
Careful wiring keeps the underchassis from getting confusing. Top photo shows the inside of the camera case as guide to the location of the larger components.

For the licensed amateur radio operator who contemplates the thrill of amateur TV transmissions on the currently authorized 420- to 450-mc band, this TV camera is ideal.

Now build it

The camera (Fig. 1) is housed in an 8 x 10 x 4½-inch aluminum case that is built around the chassis. The two end sections are the same size and shape. The bottom is a piece of 3/16-inch aluminum plate with a ¼-20 hole tapped near the point of balance for tripod mounting. The top section requires only two right-angle folds. One of the side panels has ventilation holes. The side panel without openings covers the wiring side of the chassis. No attempt was made to miniaturize the camera. Simplicity and accessibility are the keynotes of its design.

While not critical, parts placement must be considered. Weight distribution and ventilation were also considered in the parts layout. Locate the power


V1 6198 VIDICON
LIGHT
RING
FOCUS
TARGET
V2,3 6BR8-A(2) VIDEO AMPLIFIERS
D1 IN52 CLAMP
D3-IN34-A DC RESTORER
MOD RF OUTPUT
VIDEO
12AT7
MOD
RF OSC
L4-TUNES CHANNELS 2-6 VHF TV
V5 6DE7
VERT SYNC PULSE
IN70 SYNC CLIPPER
VERT DISCHARGE
VERT OUTPUT
HEIGHT
VERT CENT
VERT YOKE
VERT LIN
IN92 WAVE SHAPER
VERT BLANKING SIG
HORIZ SYNC PULSE
BEAM
6AB4 HORIZ OSC
XTAL
15.750KC
HORIZ WIDTH
V7 6DE7 HORIZ AMPL
HORIZ CENT
HORIZ YOKE
FOCUS COIL
HORIZ LIN
HORIZ BLANKING SIG
RECT 1,2,3,4 IN2070
PWR TRANS
120VAC 20MA
120V AC 100MA
6.3V CT 3.75A
NE-2
117VAC
1.5A SLOW BLOW
PLACE C40,41 ACROSS V4 SOCKET
1.1V P-P 30∿
2.4V P-P 30∿
4.5V P-P 30∿
25V P-P 7875∿
160V P-P 30∿
9V P-P 30∿
18V P-P 30∿
8V P-P 30∿
6V P-P 30∿
33V P-P 7875∿
280V P-P 7875∿
55V P-P 7875∿

R1—pot, 250,000 ohms
R2, R42, R43—270,000 ohms
R3—51,000 ohms, 5%
R4—2.2 megohms
R5, R6—100,000 ohms
R7, R35, R44—pots, 500,000 ohms
R8—4,300 ohms, 5%
R9—1 megohm
R10, R39—20,000 ohms, 5%
R11, R15—82 ohms
R12—2,400 ohms, 5%
R13—2,200 ohms, 1 watt
R14—1.2 megohms
R16—12 ohms
R17, R32, R59, R61—1,000 ohms
R18—100 ohms
R19—2,700 ohms
R20—3,000 ohms, 5%
R21—820 ohms, 1 watt
R22—15,000 ohms
R23—39,000 ohms
R24, R26—180 ohms
R25, R45—470 ohms
R27—22 000 ohms
R28, R49—68,000 ohms
R29—560,000 ohms
R30—2.7 megohms
R31—820,000 ohms
R33—4,700 ohms
R34—1.8 megohms
R36, R66—390,000 ohms
R37—pot, 20,000 ohms
R38—2,200 ohms, 2 watts
R40, R50—pots, 50,000 ohms
R41, R64—10,000 ohms
R46—10 megohms
R47—470,000 ohms
R48—2,200 ohms
R51, R52, R62—33,000 ohms
R53, R63—pots, 25,000 ohms
R54—1.2 megohms
R55—8.2 megohms
R56—470 ohms, 1 watt
R57—1,000 ohms, 2 watts
R58, R65—6,800 ohms
R60—3,300 ohms
R67—82,000 ohms
All resistors ½ watt, 10% unless noted
C1—30 - 30 μf, 450 volts, electrolytic
C2—100 - 80 - 60 - 40 μf, 150 volts, electrolytic (Mallory FP-412 or equivalent)
C3, C10, C31, C37—12 μf, 150 volts, electrolytics (Mallory TC-43 or equivalent)
C4, C5—40 - 40 μf, 150 volts, electrolytics (Mallory FP-212 or equivalent)
C6, C33—.01 μf, 200 volts, molded paper
C7, C11, C13, C27, C28, C30, C42—0.1 μf, 200 volts, molded paper
C8, C12—100 μf, 3 volt, electrolytics
C9, C15, C16, C39—0.5 μf, 200 volts, molded paper
C14—.0012 μf, 200 volts, molded paper
C17, C25—.02 μf, 400 volts, disc ceramic
C18—1.8 μμf, 200 volts, mica
C19, C20—27 μμf, 200 volts, mica
C21, C22—470 μμf, 400 volts, disc ceramic
C23, C40, C41—.001 μf, 400 volts, disc ceramic
C24—20 μf, 150 volts, electrolytic
C26, C34—.05 μf, 200 volts, paper
C29—270 μμf, 200 volts, disc ceramic
C32—.003 μf, 400 volts, disc ceramic
C35—.0012 μf, 400 volts, mica
C36—.001 μf, 400 volts, mica
C38—.005 μf, 600 volts, mica
CH—5-henry 50-ohm filter choke
D1—1N52
D2—1N70
D3—1N34-A
D4—1N92, 200 piv, 100 ma
F—1.5 amp, 3AG, slow blow
J1, J2—BNC coax connectors
L1—410 μh, peaking coil
L2—35 μh, peaking coil
L3—200 μh, wound on 33,000-ohm ½-watt resistor
L4—7 turns No. 20 enameled wire spaced ½ inch on ¼-inch slug-tuned form. Tapped at 1 turn from ground end.
L5—20 mh, 110-ohm, pi-wound inductor
RECT 1, RECT 2, RECT 3, RECT 4—1N2070, 400 piv, 500 ma
S—spst toggle switch
T—power transformer; primary, 117 volts; secondary, 120 volts, 20 ma; 120 volts, 20 ma; 6.3V CT, 3.75 amps. (Dage B400-256 available from Dage Div., 455 Sheridan Ave., Michigan City, Ind.)
V1—6198 vidicon (see text)
V2, V3—6BR8-A
V4—12AT7
V5, V7—6DE7
V6—6AB4
XTAL—15.750 kc (Bulova type 73H, Bulova Watch Co., Electronics Div., 61-10 Woodside Ave., Woodside 77, N.Y., or Bliley type BH9A. Bliley Electric Co., Union Station Bldg., Erie, Pa.)
Deflection yoke—VK-200 available from Cleveland Electronics or wind your own (see text next month)
Focus coil—VK-200 available from Cleveland Electronics or wind your own (see text next month)
Socket for vidicon (Cinch No. 54A18088 or equivalent)
Sockets for tubes
Pilot-light assembly with NE-2 lamp
Chassis and case to suit
Miscellaneous hardware

Fig. 1—Complete circuit of the home-built camera.

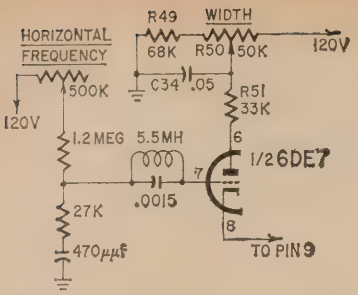


Fig. 2—L-C stabilized multivibrator eliminates crystal oscillator and reduces number of tubes to six.

transformer away from the deflection components. Arrange the first video amplifier as near as convenient to the signal ring of the vidicon. Keep the rf oscillator away from the first video amplifier or provide adequate shielding.

The BEAM, TARGET and FOCUS controls are adjusted frequently, and must be readily accessible. The remaining controls require less adjustment after initial setup. The horizontal sweep generator consists of V7-a and V7-b connected as a cathode-coupled multivibrator synchronized by V6, a 15, 750-cycle crystal oscillator. An alternate circuit with L–C stabilization is shown in Fig. 2. If the L–C stabilized horizontal oscillator is used, it may be wise to provide external adjustment for the HORIZONTAL FREQUENCY control.

Small insulated standoffs were used in place of terminal strips. The peaking coils are inexpensive standard replacement units.

Early adjustments

The vidicon is relatively delicate and must be handled with care. Be especially careful of the area around the exhaust tip (Fig. 3).

Many initial checks and adjustments can be made without the vidicon tube installed. This is a good idea as its photosensitive surface can be damaged by improper deflection or loss of deflection.

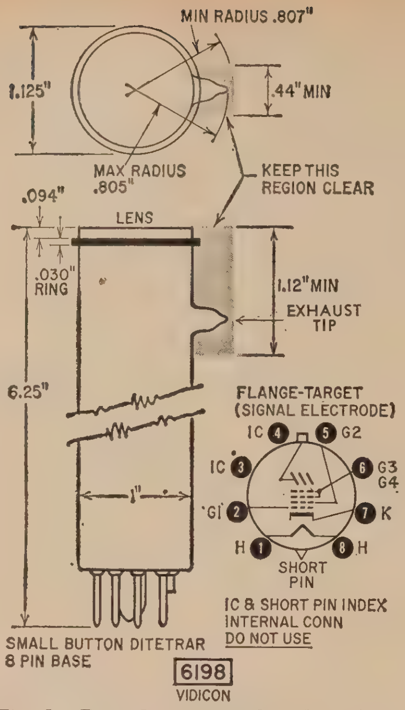


Fig. 3—Base diagram and outline drawing of the 6198.

With all tubes except the vidicon installed, measure the three power supply voltages. Even if the camera is not adjusted properly, this will not affect the readings appreciably.

Adjusting L4 while watching a nearby TV receiver should produce some bars on the screen if the receiver is tuned on one of the lower-frequency unassigned channels. This shows that the rf oscillator is working and the modulator is modulating the rf carrier. The bars are caused by the vertical and horizontal sync information. If an attempt to lock in the picture fails, the next step requires a general-purpose oscilloscope.

Waveforms

With the vidicon tube still removed, examine the vertical waveform on your scope screen. Do not proceed until waveforms almost identical to those shown in Fig. 1 are obtained. It is not absolutely necessary that the amplitude of the waveforms be exact at this point.

Check the horizontal waveforms next. They will differ from camera to camera to some extent. Do not install the vidicon until both the horizontal and vertical waveforms are reasonably correct.

When you have reasonably correct waveforms, a locked-in raster without video modulation should be obtainable. To check the video amplifiers place the tip of a screwdriver near the grid of V1-a and look at the locked-in raster on the TV set. Wavy lines or bars will be seen, indicating that the video amplifier is capable of amplifying.

Before installing the vidicon, check each socket pin for proper voltage and whether it can be varied by the associated control. Upon completion, install the vidicon tube, making certain that the signal electrode is connected and does not touch ground. Place the lens system in position.

Do not expect to see a picture right away! Expect to see blurred light and dark areas that move as the camera is positioned.

However, by adjusting the lens and the beam, target and focus controls an image should form. Adjust the linearity, height and width controls to improve the picture further. The positioning controls will aid in picture alignment. It may be necessary to rotate the yoke.

Lens systems

A lens with a focal length of approximately 1 inch (25 mm) will do nicely for general coverage. A lens with a speed of F:2.8 or better that has an adjustable iris will prove satisfactory. Movie camera 16-mm lenses are recommended, although some 8-mm lenses will do.

Miscellaneous

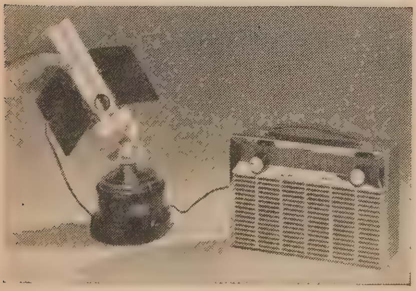
The deflection components are available from Cleveland Electronics Inc., 1974 E. 61 St., Cleveland 3, Ohio. The VK-200 coil kit is of the highest quality. The alignment coil was not used and need not be ordered. The scanning beam is aligned by passing a small amount of dc through each of the deflection coils (see R40 and R63). If you wish to wind your own coils, you will find all needed data next month.

Grade B and C vidicon tubes are available from Al Denson, P.O. Box 122, Rockville, Conn. (A grade-B tube has minor imperfections that are of little consequence to hobbyist, ham or home experimenter.) Vidicons other than the 6198 may be used.

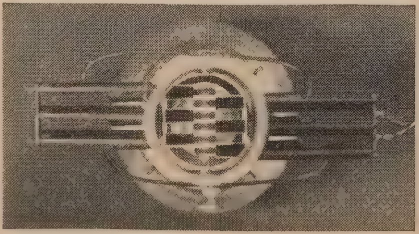
Next month we'll also see just how each of the many camera circuits operate.

TO BE CONTINUED

Kerosene Generator Powers Radio



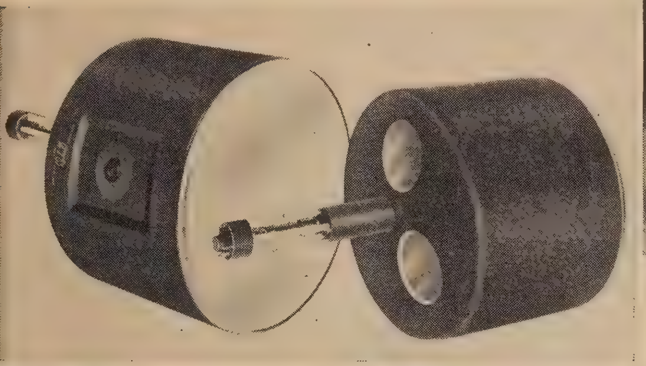
This Aztec thermoelectric generator will power a transistor radio for 24 hours on one pint of kerosene. It delivers ½ watt at ⅜ volt to a transistorized voltage converter built into the base of the lamp. This unit steps up the output to 6 volts dc at 175 mw. The lower photo is a view looking straight down on the generator when it is in place over the lamp. Made by Minnesota Mining and Manufacturing Co., the Aztec generator is designed as an emergency power source for use in fallout shelters, farms, sportsmen's camps and other remote locations away from power lines.



What's New

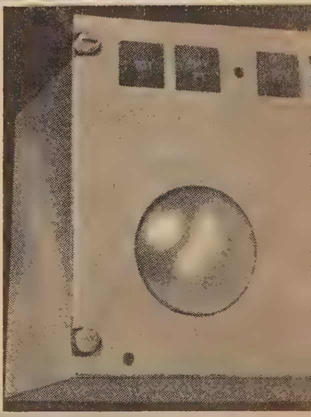
TUNNEL DIODE–TRANSISTOR MODULES operate at bit rates as high as 500 mc. They go together to form a computer system that can add four times as fast as conventional computers with only one-tenth of the circuit components. The G-E-built system is officially called a pumped tunnel diode–transistor logic system.

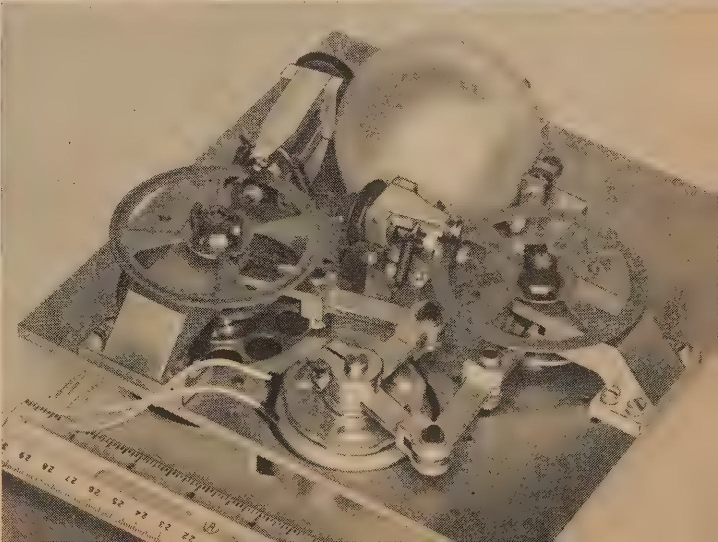
REAR WINDOWS IN RADAR CRT allow auxiliary displays to be projected onto the tube screen along with the actual radar image. For example, you might project a map or grid onto the face of the tube. Then the radar display would indicate exactly where the pip was located in relation to the area shown on the map. The tube was developed by General Atronics Corp.

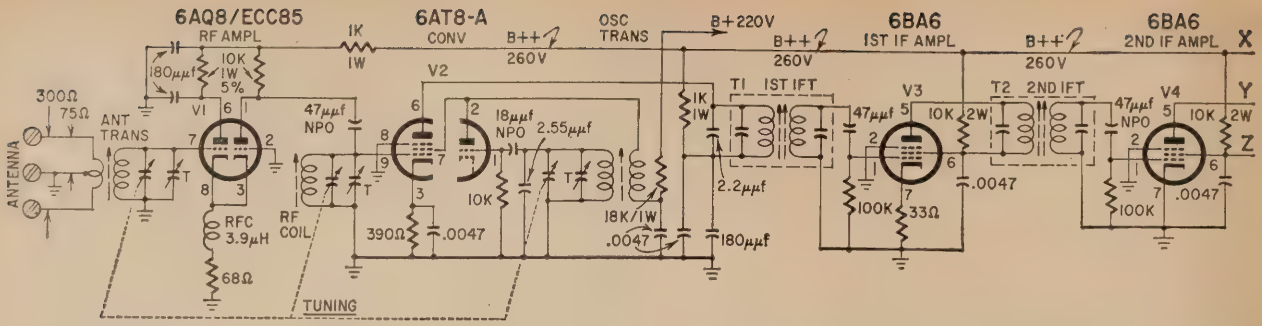


ULTRASONIC TRANSLATOR turns 35,000 - to 45,000-cycle sound into audible frequencies. It's used to detect early stage friction in bearings, bushings and other machine parts. Here an engineer is checking for lubrication requirements on the tail rotor drive shaft of a helicopter with The Delcon Leak and Friction Detector.

BALL TRACKER centers the pip on radar screen. The single control adjusts two potentiometers simultaneously, speeding the process considerably. Turning the ball moves the pip both horizontally and vertically at the same time and the operator has only the one control to fuss with, rather than two interdependent controls. The device is made by Hughes Aircraft.






6AQ8/ECC85
RF AMPL
1K
1W
6AT8-A
CONV
B++?
260V
OSC TRANS
B+220V
6BA6
1ST IF AMPL
B++?
260V
B++?
260V
6BA6
2ND IF AMPL
X
Y
Z
180μμf
10K 1W 5%
300Ω
75Ω
ANT TRANS
ANTENNA
V1
T
RFC 3.9μH
68Ω
RF COIL
47μμf NPO
V2
18μμf NPO
2.55μμf
10K
390Ω
.0047
18K/1W
.0047
180μμf
1K 1W
2.2μμf
T1 1ST IFT
47μμf
V3
10K 2W
100K
33Ω
.0047
T2 2ND IFT
47μμf NPO
V4
10K 2W
100K
.0047
TUNING

FM TUNER

By JOSEPH MARSHALL

The purchaser of an FM tuner kit looks for two things—the highest possible performance and the greatest immunity to trouble in assembling and adjusting it. Since these two ends conflict, the kit tuner designer is faced with no easy problem. The Dynatuner presents a most interesting and unconventional solution from a circuit standpoint.

The FM-1 Dynatuner bucks the current trend in front ends by using a cathode-coupled rf stage instead of the almost universal cascode or the new nuvistor neutrode. The noise figure of the cathode-coupled stage is inferior to a cascode arrangement with the same tube or an equivalent triode in the neutrode circuit. But it has some very significant advantages over the other two—particularly in a kit. It is much simpler and less critical than either the cascode or neutrode, requires no neutralization and fewer parts. Also it is less susceptible to cross-modulation and thus more nearly immune to spurious signals in local areas and easier to construct and align.

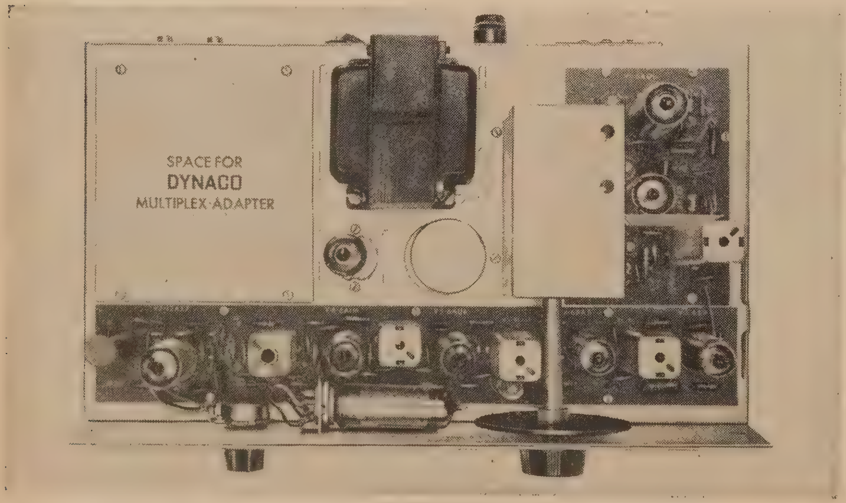
Despite its higher noise figure, the Dynatuner has a very respectable effective sensitivity. The manufacturer specifies 4-μv IHFM sensitivity, and individual tuners have measured sensitivities as good as 2.5 to 3 μv. Very few run higher than the specified 4 μv.

Circuit features

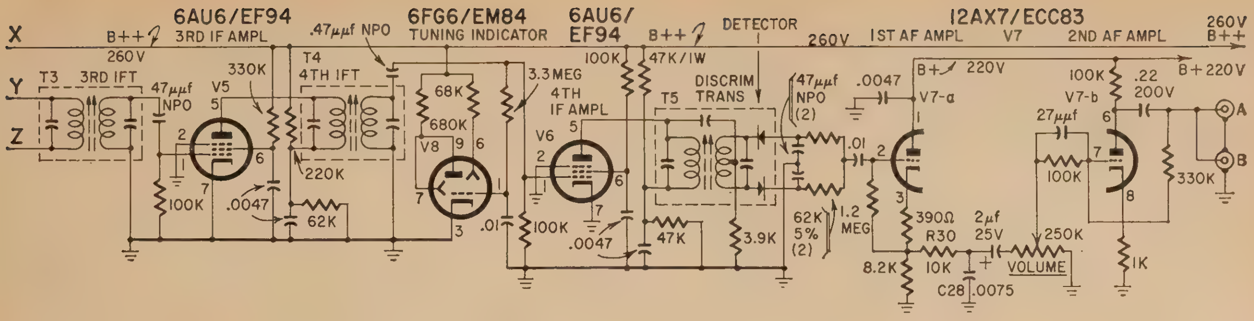
The converter is also unconventional, though not new. Oscillator voltage is injected into the screen of a pentode through a direct connection to the plate coil of the tuned-plate–tuned-grid oscillator. This gives a high degree of injection, which results in exceptionally uniform gain over the entire FM band. Moreover, it isolates the local oscillator from the tuned circuit in the converter grid, resulting in almost complete freedom from "pulling." As a result, the tracking adjustment for the front end is uncritical, since converter-coil peaking has no effect on the oscillator frequency. Also, strong stations adjacent to weak ones do not "pull" the tuner away from the weak stations. The oscillator is carefully temperature-compensated and shows no significant frequency drift even in the very first few minutes of operation.

The four-stage if amplifier is arranged by proportioning the plate and bias voltages so that all four provide some amplification on weak signals and some degree of limiting on strong ones. The gain is so high that, with no signal input, the noise of the input tube alone is enough to produce some limiting. The tuner has an extremely steep limiting curve and suppresses noise completely on inputs as low as those needed for equivalent noise suppression with tuners of higher absolute sensitivity. Although a 3- or 4-μv signal is needed for 30-db noise suppression, only 6 μv is needed to produce a 40-db signal-to-noise ratio and about 10 μv for 50-db noise suppression. Complete limiter saturation occurs with a signal of around 25 μv and results in a 60-db noise ratio.

Tuner sensitivity is more effective because of the extremely wide bandpass of the if amplifier. It appears to be between 270 and 300 kc wide—as far as I am aware the widest bandpass in any tuner today. More remarkably, it is


SPACE FOR
DYNACO
MULTIPLEX ADAPTER

Top-chassis view of the Dynatuner.


X
Y
Z
B++
6AU6/EF94
3RD IF AMPL
260V
T3
3RD IFT
47μμf
NPO
V5
330K
.47μμf NPO
T4
4TH IFT
220K
100K
.0047
62K
6FG6/EM84
TUNING INDICATOR
68K
680K
V8
3.3MEG
.01
6AU6/
EF94
4TH
IF AMPL
V6
100K
100K
47K/1W
.0047
47K
B++
DETECTOR
DISCRIM
TRANS
T5
3.9K
47μμf
NPO
(2)
62K
5%
(2)
1.2
MEG
.01
260V
12AX7/ECC83
1ST AF AMPL
V7
2ND AF AMPL
.0047
B+
220V
V7-a
390Ω
R30
8.2K
10K
2μf
25V
C28
.0075
VOLUME
250K
27μμf
100K
100K
V7-b
.22
200V
1K
330K
B+220V
260V
B++
A
B

WITH A TWIST

It has an add-on power amplifier, a very unusual power supply and some circuitry that is rare in FM

done with undercoupled if transformers and thus produces a response curve with a single hump. This permits accurate alignment with very simple means. Thus even an overmodulated signal finds plenty of room to pass through the tuner without generating significant distortion. Signals above 5 or 6 μv have completely negligible distortion—0.5% or less. Even at the 30-db IHFM test point, distortion is only about 1% and constitutes only a third of the residual noise.

Since random noise is more tolerable than distortion, extremely weak stations, even those with poorer than 30-db noise ratio, are often more tolerable than with tuners of higher sensitivity but narrower bandpass. Such tuners provide greater noise suppression but produce higher distortion. In our tests we found that although a signal may be too far down in the noise to be intelligible, even the weakest signal is not too distorted to be intolerable.

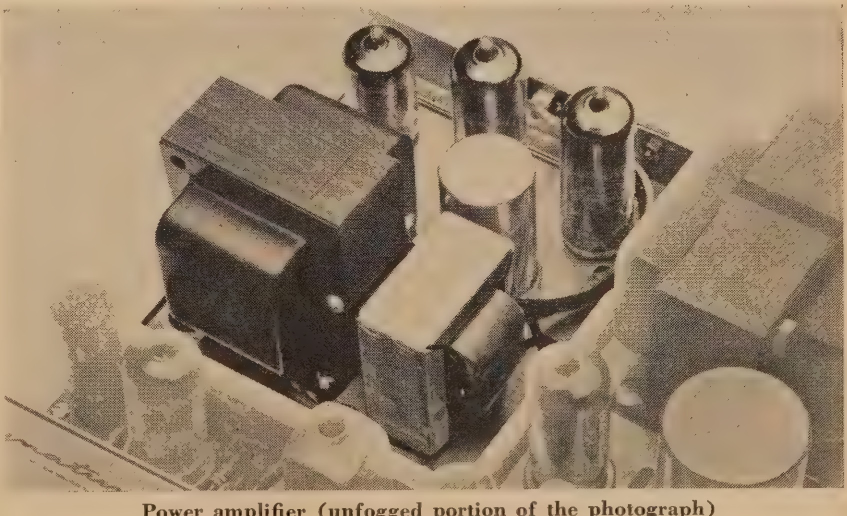
The tolerance of overmodulation —unfortunately all too common—is almost phenomenal. With a signal generator you have to exceed 200% modulation before distortion becomes audibly annoying.

Despite the wide bandpass, skirt selectivity is good. The "alternate-channel" selectivity (400 kc from resonance) is better than 50 db. Hence, there should be no trouble with interference in local areas where stations are spaced at least 400 kc apart. It is quite possible to separate two stations 200 kc apart unless one of them is many times stronger. Indeed, the 200-kc selectivity is considerably better than average because of the lack of oscillator pulling and the good capture ratio (6 db). The selectivity may be inadequate only in the case of a listener, for example, in New York who desires to hear a station in Philadelphia only 200 kc from a local station. (However, only two or three tuners, using six or seven if transformers, can give acceptable reception in such a situation.)

The detector

Although at first glance this looks like a ratio detector, it is actually a balanced-bridge discriminator using a pair of matched crystal diodes. Because of the bridge configuration, it provides a high degree of AM and noise suppression, like a ratio detector. This is true because the AM and noise divides equally between the two legs of the bridge and are cancelled in the output, whereas the FM is always unequal in the two legs and the output represents the difference. The detector bandwidth is only moderately wide—about 600 kc —but, with the very stable local oscillator and the wide passband of the if amplifier, provides uncritical tuning. A very simple and foolproof method has been devised by the designers for aligning the detector, using the tuner's own electron-ray indicator.

For years I have considered the counter the best of the FM detectors. On direct comparison, I find that the Dyna balanced-bridge is closely equal in terms of low distortion, and superior in AM and noise rejection. The counter permits the noise of the final limiter to come through; the Dyna suppresses this final noise component effectively. The Dyna detector is superior to the ratio detector in distortion



Power amplifier (unfogged portion of the photograph) is tucked away in space allotted for FM stereo adapter.

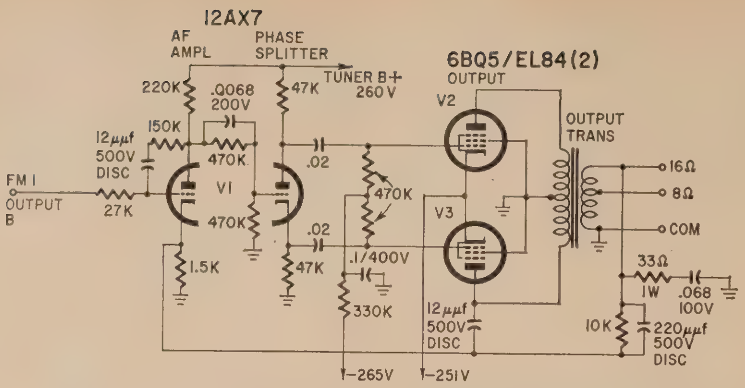


Fig. 1—You'll note that in this power amplifier the screens and plates of the output tubes are grounded.

and nearly equal in noise suppression. It is superior to other discriminators both in lower distortion and noise suppression. The use of solid-state diodes furthers the maintenance of an extremely low noise level, not only because of the inherently lower noise level of crystals over electron tubes, but also because with no heaters no hum is injected at this point. The detector's performance is further aided by its coupling to the audio stage through the high impedance of a cathode follower. This prevents loading the detector by the de-emphasis network (R30–C28).

The audio amplifier has more than 20 db of feedback. In fact, the stage gain is only 10 db. The response curve is unusually wide, running well within 1 db from below 20 to above 50,000 cycles. Overall distortion is well below ½% from 20 to above 20,000 cycles for any signal exceeding 10 μv.

As this is being written the Dynatuner MX adapter is not yet available. However, the design of the tuner forecasts exceptionally good stereo FM performance, assuming a multiplex circuit as good as that of the tuner. The very wide passband, the outstanding ability to receive weak signals with low distortion, and the flat audio response are all highly favorable for multiplex reception.

Meanwhile the manufacturer does offer a very compact 10-watt amplifier (model FMA-2) which will fit the space left for the stereo adapter and thus provide a complete FM receiver. This amplifier is also notable for the unconventional but clever way it uses the very small power transformer of the tuner to power both the tuner and the amplifier.

Built-in power amplifier

If one of these tuners is brought into your shop with the power amplifier, you may well jump to the conclusion that the chap made a terrible boner in wiring. Actually the wiring is correct (Fig. 1), and the amplifier operates with conventional voltage parameters. If you measure the voltages from cathode to plates and grids, you will find that the plates are about 250 volts positive and the grids around 14 volts negative, as they should be. And, while it is true that the power supply delivers around 70 ma to the output tubes and another 70 ma to the tubes in the tuner, the transformer is operating only some 5% above its dissipation rating, which is well within its tolerance. How is it possible to steal 70 ma from a power supply with a 100-ma rating without overheating the transformer?

Fig. 2 is a simplified diagram showing the power supply as it looks when the amplifier is added. A pair of diodes is connected across the transformer with the cathodes on the transformer side to rectify the negative half-cycle. The normal "full-wave" rectifier makes only partial use of the negative half cycle. By using it with another pair of rectifiers to feed a second load, we do increase the total load on the transformer. This is partly offset by the fact that operation is 30% more efficient in this mode. If we put a load on the negative supply equal to the load on the positive one, we increase the dissipation of the transformer only 50% instead of the 100% you would expect. Since the Dynatuner transformer was operating with a 60% factor, the addition of the 70-ma load of the amplifier merely brings the dissipation up to the rated dissipation of the transformer or perhaps 5% more. In any event, the transformer heats little or no more than it would if it were drawing the full 100 mils of current with a single full-wave rectifier.

Some adjustments have to be made to make this thieving power supply work well. The filaments of the EL84's must be fed by a separate transformer. Otherwise the heater-to-cathode potential would be around 250 volts, considerably above the permissible potential difference. The two halves of the power supply should be as closely balanced in load as possible. In this instance, the 12AX7 of the amplifier is fed by the tuner power supply, thus adding just enough drain to balance the two sides.

The amplifier circuit itself is only slightly modified from the standard Dyna configuration. The output transformer is smaller and not as linear as the bigger Dyna transformers. It will deliver 10 watts with less than 2% distortion from 30 to 15,000 cycles. Below 30 cycles and above 15 kc, the power output slopes and distortion is higher. The voltage amplifier is direct-coupled to the phase splitter through a voltage divider which is compensated with a capacitor to provide a step at the low-frequency end to make up for the slope of the output transformer and thus maintain stability at the low end. There is an inner feedback loop from the plate of the lower output tube to the input cathode to provide a step at the high end and to compensate for the frequency unbalance at the high end of the splitter. Also, there is a feedback loop around the input stage.

Although extremely compact and inexpensive, the amplifier delivers excellent performance. It was demonstrated at the Chicago and New York shows driving an AR-2 speaker to perfectly satisfactory levels even under the rather high noise levels that exist at shows. In no sense a substitute for a bigger amplifier, it does offer an economical and simple means of obtaining FM reception where space and cost are the main considerations. It is also ideal for use as a supplement to a big high-fidelity system for use in the bedroom, kitchen, porch or summer cottage.

Miscellaneous notes

The Dynatuner is available in three forms—the normal kit, a partially assembled kit and fully assembled. In the normal kit, the constructor mounts

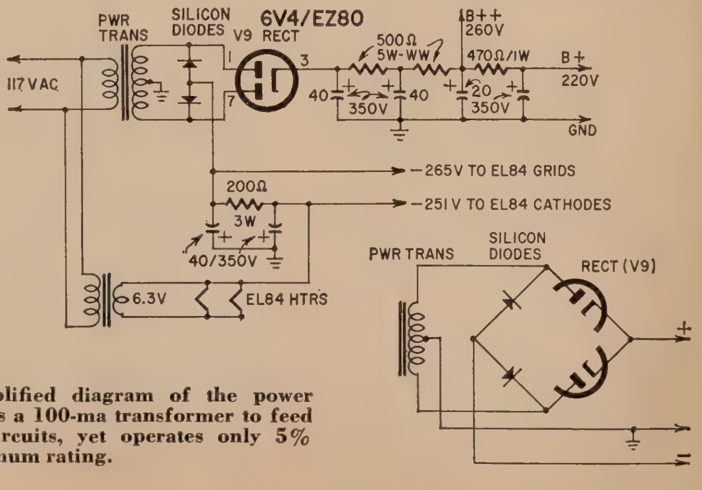


Fig. 2—Simplified diagram of the power supply. It uses a 100-ma transformer to feed two 70-ma circuits, yet operates only 5% over its maximum rating.

all the components on the two printed-circuit boards as well as on the chassis. This is not difficult and does not take much time but, as in the case of any P-C board, it does require great care in soldering each P-C joint to insure a firm contact and to avoid cold joints which may cause troubles. The semi-assembled kit comes with the P-C boards already assembled and soldered, and in this form it is possibly the simplest of all FM tuner kits to put together.

Aligning the Dynatuner offers no serious problems and can be done without any instruments whatever by using FM stations as signal sources and the tuner's own electron-ray tube as the indicator. The single-hump response of the if amplifier makes optimum peaking simple. The detector is aligned by a temporary reconnection of the tuning indicator. Optimum alignment and tracking of the front-end may be a little trickier for those who have never aligned a superhet but, if the instructions are followed carefully, it is possible to obtain very uniform sensitivity over the entire FM band since the design provides both capacitive and inductive adjustment of all three rf circuits.

Most simplified methods of aligning FM tuners without a meter of some sort produce results inferior to those with instruments in a laboratory. Much to my surprise, the Dynatuner can provide fully as good performance when aligned by the recommended method as is possible with instrument alignment. I found that a signal generator and vtvm, or a sweep generator and a scope, or even an FM generator and a distortion meter gave little improvement.

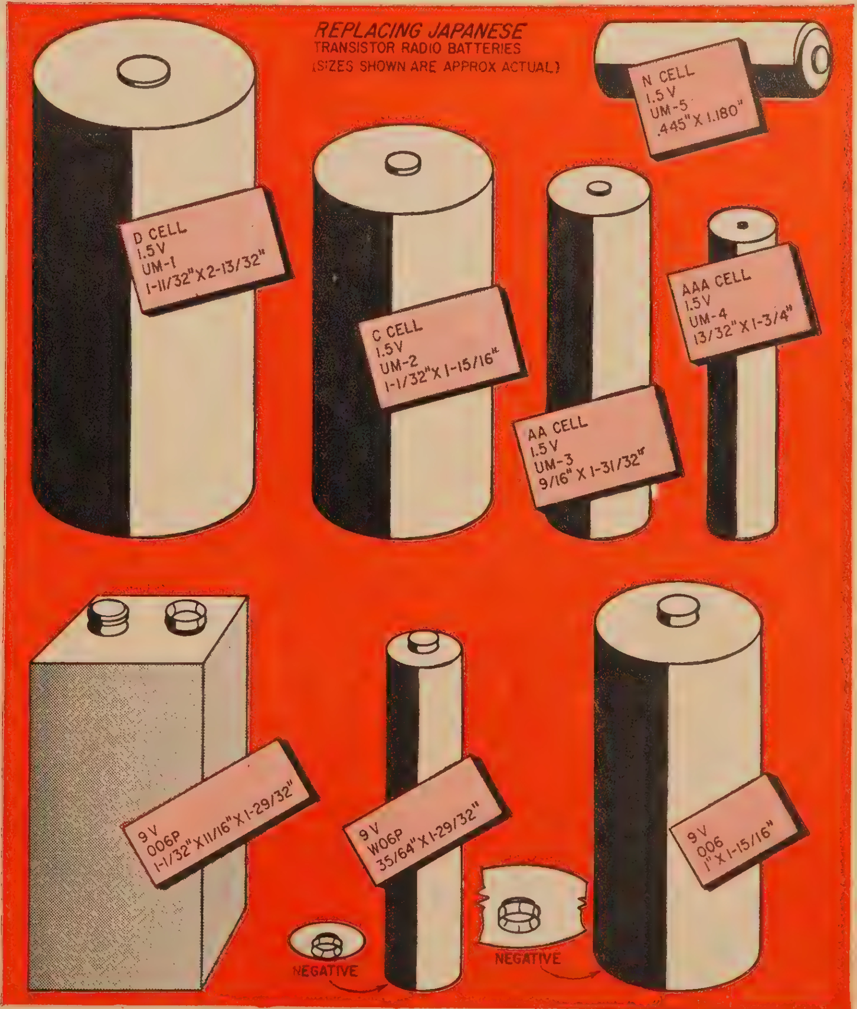
As I have already indicated, the level of performance is very high. The sample we used had a measured sensitivity of 3.8 μv with a 300-ohm input. I found this adequate to receive every FM station receivable with high-fidelity quality with *any* tuner. Two or three other tuners with sensitivities of 2 μv or better made it possible to *log* a few more extremely weak stations 250 or more miles away. But these stations cannot provide high-fidelity listening with any tuner for any period longer than a few minutes. It appears that at the edge of the ground-wave range any station weaker than about 5 μv will fade into the antenna and cosmic noise too great a proportion of the time to afford reliable high-fidelity listening.

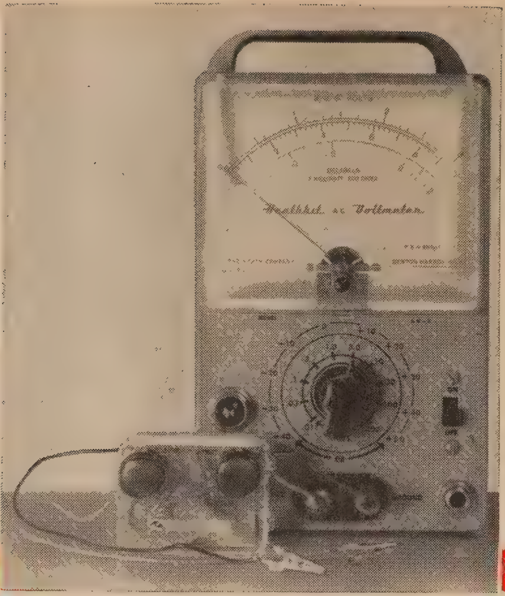
The nearest station we listen to is 40 air-line miles away and the majority are 150 or more. For example, during a 6-month period, with a Hy-Gain Log Periodic FM antenna, every FM station in Atlanta (150 air-line miles) including WABE, an educational station with only 3 kw of radiated power, was received with 100% reliability or close to it and completely high-fidelity quality. Every station within 250 miles could be logged and would provide sporadic periods of acceptable reception. No tuner we have used has done better from a high-fidelity point of view, and only two or three have permitted the logging of more stations. END

replacing Japanese transistor radio batteries

JAPANESE RADIOS USUALLY COME WITH JAPANESE BATTERIES. When these wear out and have to be replaced there is often some confusion on what US replacement to use. Perhaps this little list will help.—*Warren Roy*

	Japan	Eveready	Burgess	Ray-O-Vac	RCA
1.5-volt D-cell	UM-1	950, D-99, 100	210, 2, 230	3LP, 2LP	VS036
1.5-volt C-cell	UM-2	953, 635	1, 130	1LP	VS035A
1.5-volt AA cell	UM-3	915, 1015	Z, 930	7R	VS034A
1.5-volt AAA cell	UM-4	912	7	400	VS074
1.5-volt N cell	UM-5	904	N	716	VS073
9-volt	006P	216	2U6	—	VS312
9-volt	W06P	E177	YL6	—	VS309A
9-volt	006	226	P6M, P6	—	VS322, VS300A


REPLACING JAPANESE
TRANSISTOR RADIO BATTERIES
(SIZES SHOWN ARE APPROX ACTUAL)
N CELL 1.5 V UM-5 .445" X 1.180"
D CELL 1.5V UM-1 1-11/32"X2-13/32"
C CELL 1.5V UM-2 1-1/32"X1-15/16"
AAA CELL 1.5V UM-4 13/32"X1-3/4"
AA CELL 1.5V UM-3 9/16" X 1-31/32"
9 V 006P 1-1/32"X11/16"X1-29/32"
9 V W06P 35/64"X1-29/32"
9 V 006 1"X1-15/16"
NEGATIVE
NEGATIVE



Converter and the vtvm it is used with.

Measure dc millivolts with a dc-to-ac converter

By FORREST H. FRANTZ, SR.

Simple, low-cost unit adapts ac vtvm for low-level dc voltage measurements

THE problem of measuring small dc voltages rapidly and accurately has challenged the electronics industry for years. Many practical measurement techniques and instruments have been developed, but most of them have been beyond the practical reach of the experimenter, hobbyist and service technician. Most dc millivolt measuring instruments cost hundreds of dollars.

Another difficulty has been zero drift—a problem encountered when vacuum tubes or transistors are employed as direct-current amplifiers in the instrument. And even the comparatively simple potentiometer type of dc measuring instrument, although it is extremely accurate, is objectionable because of the time-consuming nulling procedure.

The most satisfactory approaches to the problem of dc millivoltage measurements have usually involved a dc-to-ac converter. The ac output of the conversion unit is proportional to the dc input in this scheme, and can readily be measured with an inexpensive audio voltmeter such as the Heathkit AV-2 or AV-3 or with an audio amplifier and the ac range of a multimeter (Fig. 1). The multimeter is set to a low ac volts range and connected to the amplifier's output. The converter feeds the amplifier's input. With the amplifier's gain set fairly high, use the amplifier's gain control and the converter's scale-factor control adjusted so the multimeter reading corresponds to the dc input.

The dc-to-ac converter described in this article is intended to be used in this way. Its cost is less than $10. Extremely compact—only 1⅝ x 2⅛ x 1 inch—it can be assembled in about 2 hours. Power is obtained from a

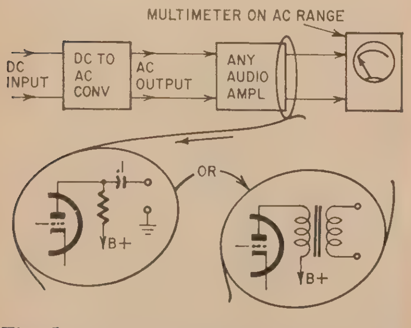


Fig. 1—Dc-to-ac converter can be used with any audio amplifier to measure dc millivolts. Just use this hookup.

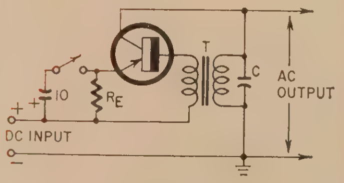


Fig. 2—Basic circuit of dc-to-ac converter.

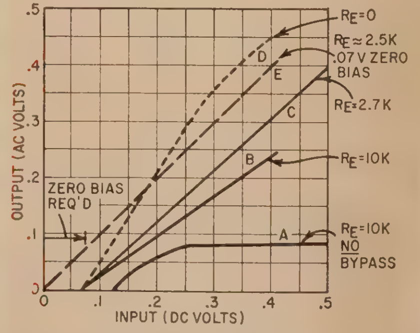
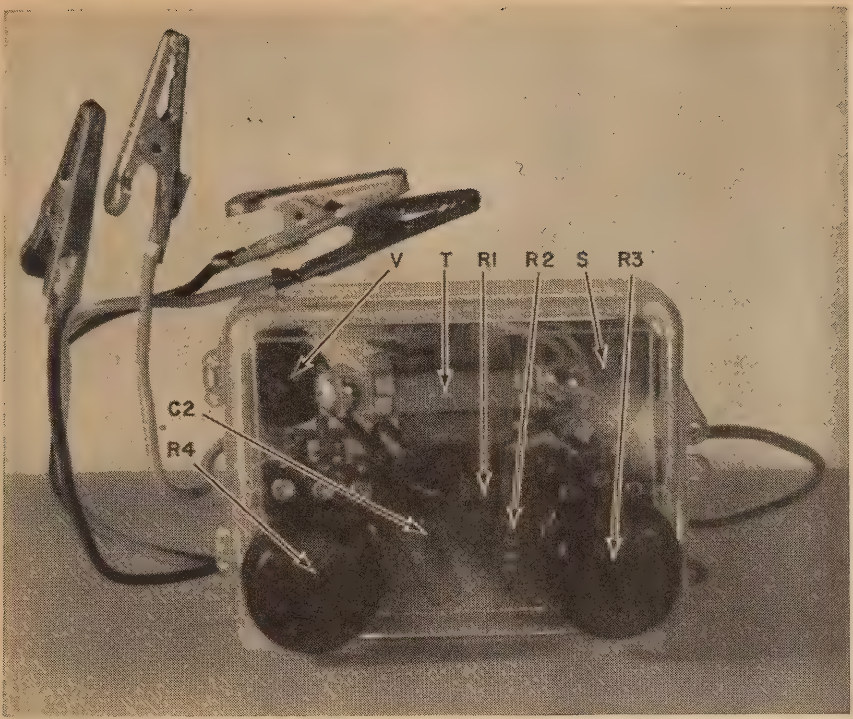


Fig. 3—Converter ac output vs dc input for various values of R_E, and bypass and bias conditions.



The entire unit fits into a small plastic case.

single self-contained inexpensive penlight cell. Battery current drain is approximately 1 ma.

How it works

The basic circuit of the audio oscillator used in the dc-to-ac converter is shown in Fig. 2. Note that the dc voltage to be measured furnishes the dc operating voltage for the audio oscillator. The desired response is an oscillator audio output voltage directly proportional to the dc voltage supplied at the input. On a graph of ac output voltage against dc input voltage, this would be a straight line.

Curve A of Fig. 3 shows that, if the emitter bias R_E is unbypassed, the audio output is not a linear function of the input, and above 0.25 volt dc input, the audio output voltage is constant. This characteristic would be highly desirable where a constant output signal is desired regardless of battery-voltage variations. But it is unsuitable for a dc-to-ac converter. Also note that oscillation does not begin till the applied dc voltage is 0.12 volt or more.

If the emitter resistor is bypassed with a 10-µf capacitor, the response is linear as shown by curve B. If R_E is decreased, the slope of the curve gets steeper as shown by curves C and D. Furthermore, oscillations begin when the applied dc voltage is only .07 volt.

Although the desired linear response has been achieved and oscillations do begin at .07 volt, the arrangement can be useful only if oscillation begins just above zero volts. This can be done by inserting a .07-volt dc bias in series with the dc input voltage. This shifts curves B, C and D in Fig. 3 to the left so they can pass through zero.

The circuit for the practical converter is shown in Fig. 4. The variable-emitter resistor R4 is the scale adjustment which varies the slope of the response curve. The battery and resistors R1, R2 and R3 provide the bias voltage for zeroing the converter. The resistance of the voltage divider is small in comparison to the converter's input resistance. The zero bias required may vary slightly from one converter to another due to transistor and component tolerances. Potentiometer R3 adjusts the bias for these and for battery aging.

R3 and R4 are adjusted when the instrument is calibrated initially and must not be readjusted each time it is used. R4 should be checked and, if necessary, readjusted about every 6 months to compensate for battery aging.

Construction and calibration

Building the unit is comparatively simple. Make the holes for the potentiometers, transformer, on–off switch, input leads and output leads first. A heated ice pick and a taper reamer will do the job nicely and minimize the risk of cracking the plastic case. Mount the potentiometers and output transformers next. A small piece of perforated board forms the chassis. After all connections are made and the unit is checked for operation, cement the perforated board to the potentiometers.

To calibrate the converter, adjust R4 to about 2,500 ohms, and connect the output terminals of the converter to the audio vtvm. Set the audio vtvm to the .01-volt range and short the input terminals of the converter. Adjust R3 till oscillation begins (evidenced by an up-scale reading on the audio vtvm). Then back off R3 to the point where oscillation just ceases.

Next, connect the converter terminals to a 0.3-volt dc source with the audio vtvm set on its 0.3-volt range. This voltage may be obtained from the circuit shown in Fig. 5. Adjust R4 for full-scale meter deflection. Disconnect the converter terminals from the voltage source and short them again. Repeat the R3 adjustment, since the change in R4 may alter the oscillator zero bias slightly.

Curve E in Fig. 3 shows the response of the completed instrument. The dc-to-ac ratio is 1 to 1. The calibration is as good as the accuracy of your calibrating voltage and the care you put into making the calibration. The range of the converter is 0 to 0.3 volt, which you can cover in four ranges—.01, .03, 0.1 and 0.3 volt—with the range switch of an audio vtvm. Since voltages above 0.3 can readily be measured with a conventional general-purpose vtvm, no provisions were made for using the converter to measure higher voltages.

R1—100 ohms, ½ watt
R2—1,000 ohms, ½ watt
R3—pot, 1,000 ohms, miniature (Lafayette VC-26 or equivalent)
R4—pot, 10,000 ohms, miniature (Lafayete VC-34 or equivalent)
BATT—1.5 volts, N cell
C1—30 µf, 6 volts, electrolytic, miniature (Lafayette CF-104 or equivalent)
C2—.01 µf (Aerovox 83Z or equivalent)
P1, P2—plugs to match vtvm input jacks
S—spst slide switch
T—miniature transformer: primary, 2,000 ohms, ct; secondary, 10,000 ohms (Argonne AR-109 or equivalent)
V—2N107
Case—1⅝ x 2⅛ x 1 inch
Perforated phenolic chassis—2 x 1 inch
Miscellaneous hardware

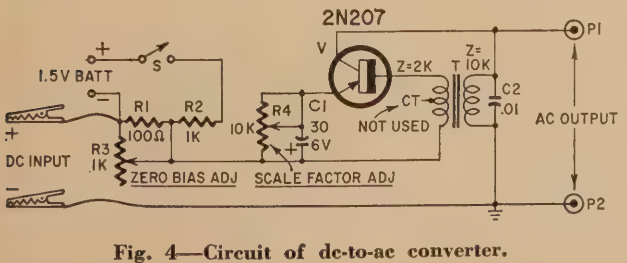


Fig. 4—Circuit of dc-to-ac converter.

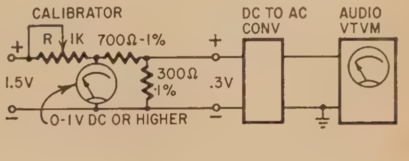
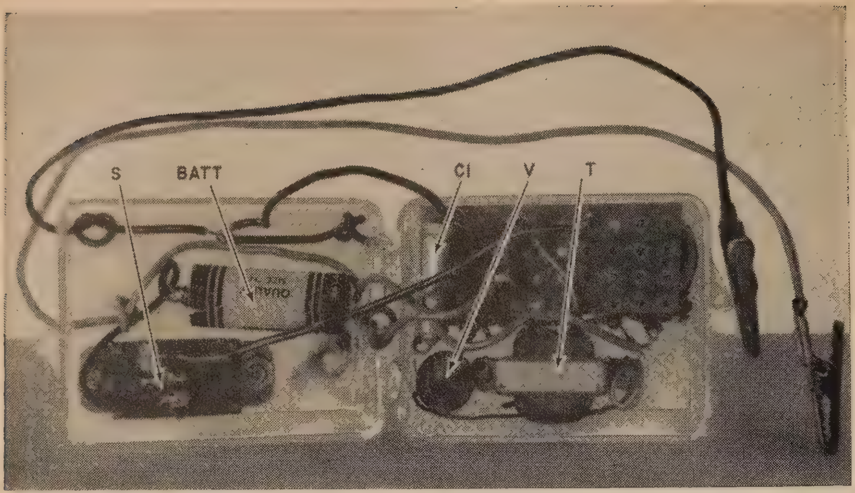


Fig. 5—Calibration circuit. Adjust R until dc voltmeter reads 1 volt.



Parts are arranged in both halves of the case.

The converter will draw approximately 8 μa from the dc circuit it measures for a 0.3-volt input and approximately 3 μa for a .03-volt input. Circuit loading is quite small, and accurate measurements may be anticipated for circuits of moderately high impedance. If a dc-to-ac conversion ratio of less than 1 to 1 is employed by increasing the value of R4, input current requirements can be reduced even further. Since the 1-to-1 conversion ratio allows direct reading from the ac vtvm meter scale and range switch, it was considered more advantageous than an arrangement which would introduce a conversion constant that had to be remembered and applied to meter readings. This way we get an easy-to-use direct-reading instrument.

The emitter resistor R4 stabilizes the circuit against drifts due to temperature changes. Any user of this circuit will be well pleased with its stability, linearity and overall performance. END

WHAT'S YOUR EQ?

It's stumper time again. Here are three little beauties that will give you a run for the money. They may look simple, but double-check your answers before you say you've solved them. For those that get stuck, or think that it just can't be done, see the answers next month. If you've got an interesting or unusual answer send it to us. We are getting so many letters we can't answer individual ones, but we'll print the more interesting solutions (the ones the original authors never thought of). Also, we're in the market for puzzlers and will pay $10 and up for each one accepted. Write to EQ Editor, Radio-Electronics, 154 West 14th St., New York, N. Y.

For answers to last month's puzzle see page 68.

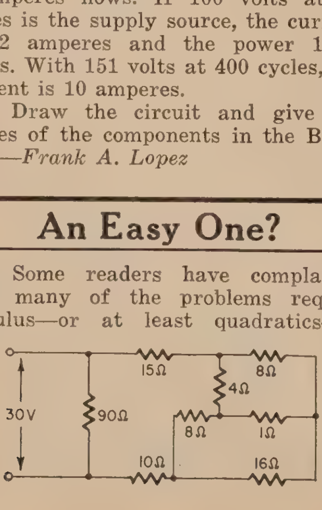
Variable-Current Black Box

This particular Black Box has two terminals. When 50 volts dc is applied, 2 amperes flows. If 100 volts at 60 cycles is the supply source, the current is 12 amperes and the power 1,200 watts. With 151 volts at 400 cycles, the current is 10 amperes.

Draw the circuit and give the values of the components in the Black Box.—*Frank A. Lopez*

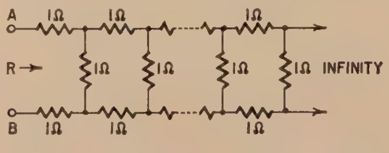
An Easy One?

Some readers have complained that many of the problems require calculus—or at least quadratics—to figure out. Here is one that can be done without calculation. Observe the circuit pattern and determine the voltage across the 1-ohm resistor.—*Albert C. W. Saunders*



Iterative Network

Engineers will recognize this problem as the very simplest type of iterative network, but it will be interesting and useful to beginners. Good training for transmission lines, too!



The circuit shown above consists of 1-ohm resistors. The lattice extends to infinity. What is the total resistance of R, looking into points A and B?—*Mordehai Arditti.*

Making Twisted Cable

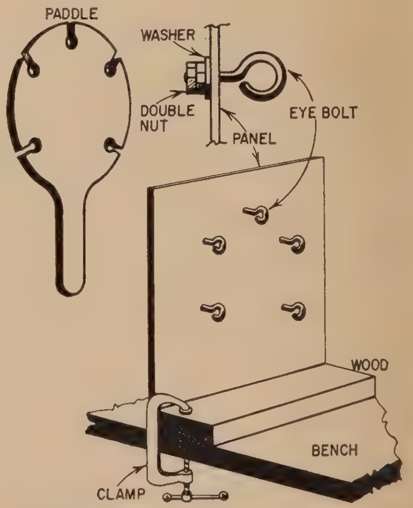
By ELMER CARLSON

LENGTHS OF TWISTED PAIRS OF WIRES for filament and power circuits can be easily made with a hook bent from 3/16-inch OD tubing or rod. It may be necessary to heat some rod or tubing while bending it.

If both wires are the same color, simply unroll a little more than twice the required length and, with the loose ends held together, tie an overhand knot. With the knot end held in the hook, loop the doubled end over some solid, stationary object (a doorknob or tightened vise handle will do), and start winding with the drill (Fig. 1). For extremely long lengths, use an electric drill.

Fabric-covered wire needs a different technique. It is necessary to provide some means for the individual wires to twist at the far end while winding. This requires a special jig consisting of two parts and for best results, an assistant.

Each wire is tied separately to an eyebolt mounted on a plate. The ring is on one side, a flat washer and two nuts on the other (Fig. 2).



When three or more wires are twisted, a separator must be used to steady the wires. This keeps them from whipping, and maintains their spacing for a smooth, even twist.

A discarded ping-pong paddle can be used. It is evenly notched around the edge with keyhole-shape slots to guide the wires. As twisting progresses, the assistant moves away from the twisting end, keeping the wires separated. END

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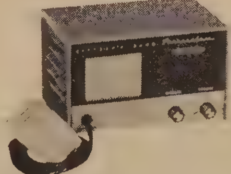

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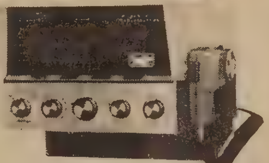

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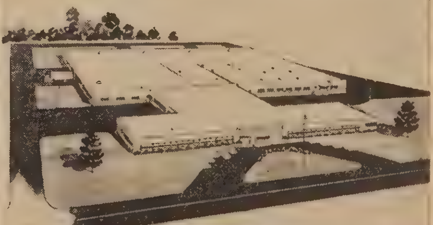

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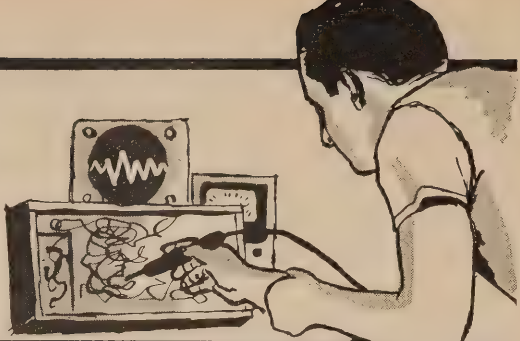

This column is for your service questions. We answer them free of charge and your name and address will be kept confidential if you wish. The main purpose is to help those working in electronics with their problems.

We've changed our target a little and are no longer restricted to TV. Radio, audio and industrial electronics problems are also grist for the mill. All letters get a prompt individual answer and the more interesting ones will be printed here. So if you have a service problem, send it here. We'll do our very best to help you solve it.

VERY SELDOM DO TROUBLES OCCUR IN TV transmitters or control equipment. However, no experienced engineer would deny that they *do* happen now and then. If the TV technician can recognize them, he may save a lot of time spent tearing down innocent TV receivers.

One of these troubles is occasional overmodulation of the transmitter. This results in an almost complete "white-out" of the screen (Fig. 1). It is caused by overmodulating the video carrier transmitter, thus *reducing* the amount of signal being radiated. Fig. 2 shows the difference between 100% and 120% modulation, which is about the level equivalent to the effect shown in Fig. 1. Note that actually *less* rf is being radiated during the overmodulated periods.

With our TV sets designed as they are, the stronger a signal is, the blacker our pictures are. In other words, our TV receivers start with a white screen. The signal extinguishes the beam of the picture tube by cutting it off. So if we receive a very weak signal, areas in the picture which should be black are gray, because the signal is too weak to make them a clean black.

This type of trouble occurs more often with smaller stations. The larger stations, and the network originating stations, have very well designed automatic devices to prevent this. Fast-acting agc circuits in the video output (before the video signals are added to the sync) maintain a constant level. At times, troubles are found in the station itself. At one station, the agc circuit was installed, by mistake, in the output of the console going to the transmitter. Here, it controlled, not only the video, but the total amplitude of the signal, sync and all. Thus, when a white burst came along, the net result was not only overmodulation, but a severe case of momentary sync clipping.

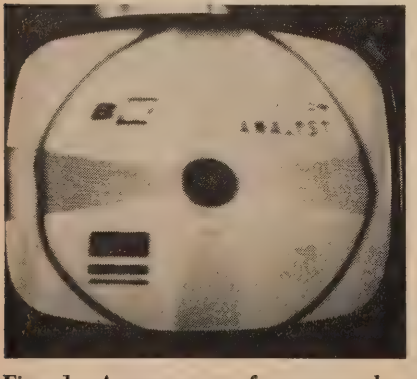

Fig. 1—Appearance of screen when transmitter is overmodulated.

One other question often heard concerns the ghost images seen on the screen after the cameras have been moved to another shot. Lettering from commercials, the newcaster's head, and other stationary objects can be seen on the screen, overlying the other subject. This is due to burning-in of the image on the mosaic of the image orthicon in the camera. It generally means that the tube has just about reached the end of its useful life. At times, even with a good tube, it is possible for an inexperienced camera operator to burn in an after-image on his screen by carrying his beam current too high. However, the chief engineer usually takes care of these gentlemen, especially after he watches a program or two.

Color shrinking

My RCA CTC4 color TV shrinks sideways on color programs only. Black-and-white reception seems OK. Width control is at its full-width position. High voltage runs about 23,000 volts.—J. I. H., Reseda, Calif.

I've run into this problem on several sets, including mine, and the answer seems to be something different each time (shrinkage, that is, not necessarily on color only).

The major cause seems to be a very slightly weak 6CB5 horizontal output tube. Try replacing this tube, also the damper, and resetting the drive and high-voltage controls. Incidentally, RCA now OK's the replacement of the 6BL4 damper tube in this series with a 6AU4-GT. Since they brought the voltage rating up on the 6AU4, it will work here.

One more cause here might be burned resistors in the high-voltage lead. Check the three 22,000-ohm resistors inside the doghouse, near the high-voltage connector. They have gone out in several sets when the focus control went bad. While you're in there, have a look at R306, R276, the two 1-megohm resistors in the focus circuit.

There is one more rather unusual prospect in this circuit, the video amplifiers. Due to the weird circuitry (for black-and-white TV practice) used in the brightness and contrast control circuits, it is also possible for a defective final video amplifier tube or stage to cause a problem along these lines. In other words, if the video amplifier can affect the brightness, it can certainly affect the width, by changing the CRT beam currents. It's worth checking out, at any rate. Look for leaky coupling capacitors and shifted resistors in the video grid circuits.

By the way, you might look at the three pots in the screen control circuits, too. These parts carry the 800-volt B-boost voltage and they can run pretty hot and burn up sometimes. This causes color-hue drifting and assorted troubles along that line. However, if your background and color temperature are OK, they're OK too.

No vertical sweep

I have an Admiral 20Z4PS TV on the bench that is giving me lots of trouble. No vertical sweep. I read about 300 volts on the 6S4 plate, but there's no pulse there at all. I've tried a new yoke, without results. The two 18,000-ohm resistors from boost to the output transformer are overheating. I ought to get 580 volts on that plate, but it isn't there.—M. S., Monterey, Tenn.

I believe this trouble is going to be found in the vertical output transformer. It sounds as if it is leaking to ground. If the two 18,000-ohm resistors between boost and the bottom of the output transformer are overheated, something is causing excessive current drain in that circuit. If the tube has been changed and the yoke checked for grounds, then there is only one thing

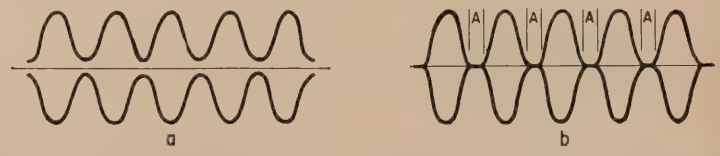

Fig. 2—Sine-wave modulation patterns. a—Note this rf output never drops below zero line. This is roughly equivalent to about 90% modulation. b—Overmodulation of carrier equivalent to about 120% modulation. Note, during intervals marked A, transmitter actually has no rf output. Therefore, total amount of energy being radiated is less and we get lower signal strength.

left—that vertical output transformer (Fig. 3).

There is one other possibility, but I expect you've checked that: the 10-μf electrolytic capacitor connected between the vertical output transformer (the red wire) and the 6S4 cathode.

Also check the 20-μf electrolytic between cathode and ground. Incidentally, if the 10-μf unit is shorted, it could have burned out the vertical linearity control, opening the cathode of the 6S4 or shorting it to ground through the bad capacitor. Both have been known to happen. Sudden opening of the cathode could have caused a spike of voltage to be fed to the transformer, causing the windings to break down to the frame.

You should read about 425 volts on the load side of the two 18,000-ohm resistors and about 410 volts on the 6S4 plate. Check the resistors for signs of changing value due to overheating.

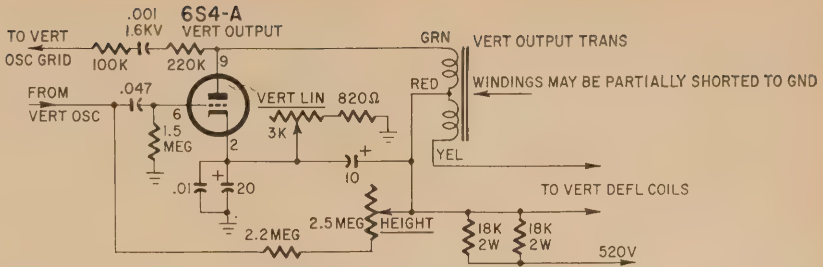

Fig. 3—No vertical sweep in this circuit may be caused by the vertical output transformer windings being partially shorted to ground.

Double-trouble

An RCA KCS-49 keeps blowing the ¼-amp fuse in the high-voltage supply. Whenever I change it, the set plays for a while (several hours to a day or two) and then it blows again. I changed the 6BG6-G and the damper tube, and it blew just as soon as the high voltage came up! The only trouble I can find is a charred resistor feeding the vertical output transformer primary from the boost. I replaced the resistor and the 6K6 vertical output tube. This time it played for about ½ hour before the fuse went out again!—K. M., Pittsburgh, Pa.

It looks as if the thing is trying to throw you a curve, with that burned resistor in the vertical circuit. From the description, I'd say that this was the result of a previous short in the vertical output tube some time ago. The only cause for this trouble (in that circuit) would be an intermittent short to ground in the vertical output transformer and this would cause a different set of symptoms. Every time this has happened to me, the immediate result has been a sudden collapse of the vertical sweep (the thin white line) followed by the fuse blowing.

I think you'll find the trouble in the horizontal output circuit. Look for excessive screen voltage on the 6BG6-G, an intermittent short in the width control or the horizontal drive trimmer.

Check plate current of the 6BG6-G. This should be 80 to 105 ma and *never* over 105 ma.

Check the dc drive voltage on the 6BG6-G. This should be about −22. I would recommend monitoring as many of these voltages as possible simultaneously while watching the set to see what happens when the fuse goes.

You might try replacing the 6W4 damper tube with a 6AU4 (which has a much higher heater–cathode breakdown rating) and clipping off the heater-cathode jumper at the socket. There is a possibility of an intermittent ground in the damper heater winding in the power transformer.

Needs a flyback

I'm working on a Crosley 10-416MU set with a burned-out flyback. The original part number is NAC 147428. I can't get one anywhere. Can

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you suggest a substitute? If so, how many changes will I have to make in the circuit?—G. S., Laurelton, N. Y.

The only replacement for this I can find is a Triad D-111. The connections are the same, as indicated on the instruction sheet you'll find in the carton.

Horizontal roll

An Admiral 14UY3C has horizontal roll. I can hold the picture still with the adjustments for a minute or two, then it falls out both horizontally and vertically.

I've replaced all parts in the oscillator; ringing coil, etc.—T. O'B., Prosser, Wash.

This trouble is in the sync circuits, not in the oscillator, since you *can* hold a picture still with the horizontal hold control.

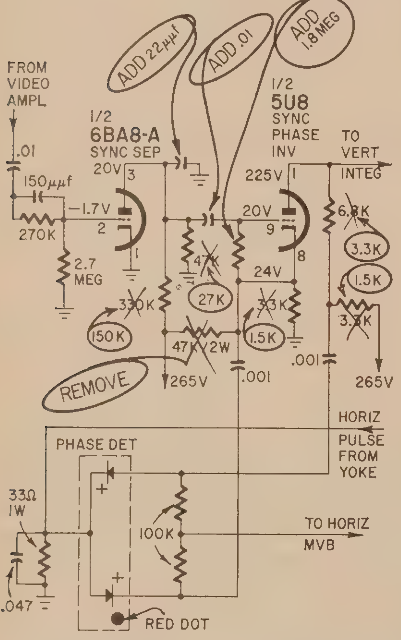

Fig. 4—Changes shown in sync circuit will improve its action.

I suggest changing the horizontal afc diodes; they are the most common cause of trouble in such complaints.

To improve sync, there have been some modifications in the sync circuits of this set. Fig. 4 shows the original parts and the changes.

Drift after warmup

I repaired intermittent horizontal drive in a Bendix TM17, then it had insufficient height, the complaint it came in for! All waveforms are OK, but brightness increases after warmup, width and linearity change, and the vertical hold is critical.—F. C., New York.

This is damper and boost trouble, apparently. Run a complete adjustment on the horizontal linearity. From the symptoms, it sounds as if the horizontal linearity is not set properly and is on the edge. Also, replace the 6W4 damper with a 6AU4, which has a higher current-carrying capacity. END

SW PROPAGATION FORECAST

April 15–May 15 **By STANLEY LEINWOLL***

This month a major change is being made in the propagation tables.

In the past we have shown for each hour the short-wave broadcast band nearest the optimum working frequency. This has restricted the use of the tables to short-wave listeners interested in international broadcasting.

To make the tables more useful to the many other users of the high-frequency spectrum (fixed, amateur, aeronautical, etc.), the tables will hereafter show the optimum *frequency*, in megacycles, for propagation of short-wave signals between the locations shown during the time periods indicated.

To use the tables, select the one most suitable for needs and your location, read down the left side to the region in which you are interested, then follow the line to the right until you are under the appropriate time. (Time is given at the top of each table in 2-hour intervals from midnight to 10 pm, *in your local standard time.*) The figure thus obtained is the optimum working frequency, in megacycles.

The best band for the particular service in which you are interested is the one nearest the optimum working frequency.

For example, a resident of New York City would use the Eastern USA table. At midnight, signals to and from Western Europe would be optimum in the 8-mc band. A radio amateur would be most likely to establish communications in the 40-meter (7-bc) band. A short-wave listener would try the 7-, 6-, and 9-mc broadcast bands, in that order.

The tables are designed to serve primarily as a general guide, since day-to-day variations in receiving conditions can be considerable. At certain hours, propagation over some of the paths given in the tables may be extremely difficult or impossible.

In general, circuits passing through the northern auroral zone will be more difficult than those over more southerly paths. In addition, circuits lying entirely in daylight or darkness will be better than those passing from daylight to darkness, or vice versa.

EASTERN US to:	Mid	2	4	6	8	10	Noon	2	4	6	8	10
West Europe	8	7	8	10	11	12	12	13	13	13	12	10
East Europe	8	7	8	9	10	11	12	12	12	11	9	8
Central America	12	10	11	14	15	15	16	17	16	15	14	13
South America	12	9	13	16	17	17	17	17	17	16	14	13
Near East	8	7	8	10	11	12	12	13	13	12	11	10
North Africa	8	7	9	11	12	13	13	14	14	14	12	10
South & Central Africa	7	9	10	14	15	16	16	16	10	14	8	7
Far East	9	8	8	8	10	11	11	11	12	12	11	10
Australia & New Zealand	12	11	11	10	10	10	9	18	18	18	18	14

CENTRAL US to:												
West Europe	8	7	9	11	12	12	12	13	13	11	10	8
East Europe	8	8	8	11	11	12	12	12	10	10	10	10
Central America	13	11	10	13	15	15	16	17	17	16	15	13
South America	9	10	15	16	17	17	17	17	15	14	13	13
Near East	8	9	10	11	12	12	12	12	11	11	9	8
North Africa	7	9	11	12	12	13	13	13	12	11	10	8
South & Central Africa	8	10	12	13	13	14	14	15	15	13	10	8
Far East	9	7	9	12	11	12	13	13	13	14	13	11
Australia & New Zealand	12	12	10	10	10	17	19	19	18	17	13	13

WESTERN US to:												
West Europe	8	8	8	10	11	11	12	12	11	10	9	9
East Europe	7	7	7	8	10	10	10	10	9	9	9	9
Central America	13	11	12	15	17	18	19	19	19	17	13	12
South America	10	8	10	15	16	17	17	17	16	16	13	12
North Africa	7	7	8	10	11	12	12	12	12	11	10	9
South & Central Africa	9	8	10	13	13	14	14	13	10	7	7	9
Far East	12	10	8	8	12	12	13	14	14	14	14	14
South Asia	12	9	8	9	12	12	12	12	12	13	13	13
Australia & New Zealand	13	13	11	10	10	14	19	20	20	20	20	16

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PUT MORE ON YOUR TAPE

By JAMES MASKASKY

Nearly all systems for multi-channel tape recording are either too complicated or too expensive for the average audiophile. There is one method you can easily experiment with at home. By taking advantage of an angular property of tape recording, you can record and play back six or more channels with one ordinary half-track tape head.

Before we go any further, one condition behind this system must be made clear. When recording, the erase head must be disabled. If you have a recorder with permanent-magnet erase, you have no problem—simply remove the erase magnet. But if you have a tape recorder with a multiple-function head, you may not be able to disable the erase head. If you have a recorder with a separate erase head, remove the head but leave it connected. Its inductance may be a part of the bias oscillator circuit. If it is and you disconnect it, you will not be able to record properly. I added an additional record–playback head on a special mount so it could be rotated as desired. Naturally, I selected a head that matched my recorder. I left the erase function on the original head.

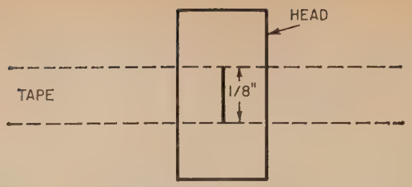


Fig. 1—A half-track record head has a gap that is slightly less than ⅛ inch high. For convenience ⅛ inch is used.

How it works

In ordinary tape recording, the record head is perpendicular to the tape and the signal recorded on the tape runs the full height of the gap in the record head (a trifle less than the ⅛ inch for half-track heads, shown in Fig. 1). Now if we rotate the record head 60° to the right, we can rerecord the portion of the tape that is now covered by the tape-head gap height.

Fig. 2-a shows this vertical height to be cos 60° times the original height: $\frac{1}{2} \times \frac{1}{8}'' = 1/16$ inch for the height of the remaining part of the first channel. A picture of the tape after this two-channel recording is in Fig. 2-b.

Before we discuss playback, let's look into some elementary tape recording theory. If a tape is recorded at one angle and played back with the head at a different angle, signal strength drops and distortion increases. This becomes increasingly noticeable as the playback angle increases relative to the record angle.

Playback problems

Now let's go back to our prerecorded tape (Fig. 2-b). The second signal, recorded at 60°, can be played back if we turn the playback head to the same angle. Since this is the only signal that crosses the tape head, it will be the only one audible.

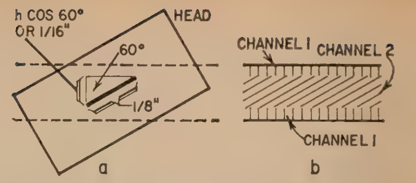


Fig. 2—Composite diagram shows the signal on the tape when two channels are recorded on the same track.

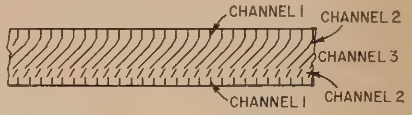


Fig. 3—Here, three channels are recorded on a single track.

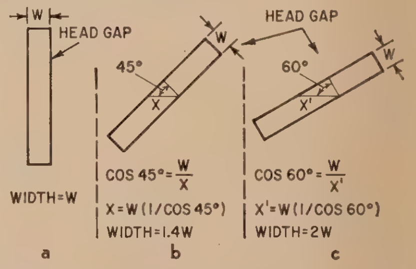
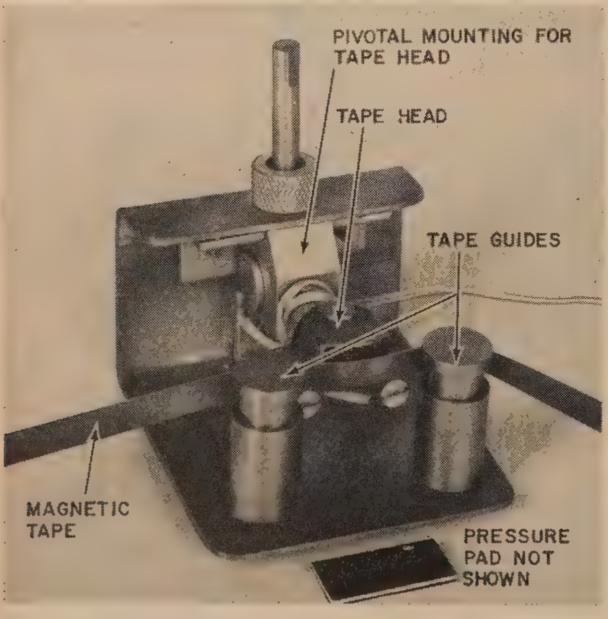


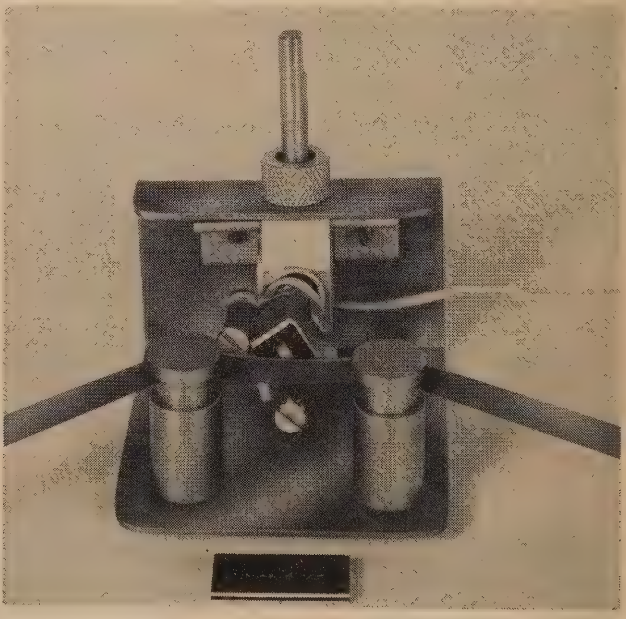
Fig. 4—How gap width is figured for various angles of tilt.

Rotating the tape head back to 0° we get the remaining portion of the vertical signal on the extremes of the tape head, and the second signal at an angle of 60° in the middle of the tape head. Since this angle is large enough to cause a significant reduction in volume of the middle signal, we hear only the signal originally recorded on the first channel.

By expanding this one more step, we can see that by choosing a number of angles, three or more signals can be recorded on each half track. The theoretical angles for three channels would be: $(\cos^{-1} 1)$, $(\cos^{-1} \frac{2}{3})$, and $(\cos^{-1} \frac{1}{3})$.



The author used this arrangement to tilt the head to the desired angle. Assembly has its own built-in tape guides.



The tape head has been rotated 60°.

In numbers, this would be approximately 0°, 48° and 70°, but for practical reasons (they're explained later) 0°, 45°, and 60° were chosen for three channels. Fig. 3 shows the magnetic pattern of this three-channel system. For four channels, the angles could be 0°, 40°, 55° and 70°.

One question some reader may be asking at this point is, "Why was 90° ruled out as a limit?" For this apparatus, it is impossible to get an adequate signal at 90° because the gap height (⅛ inch) becomes the tape-head gap width seen by the tape, which means that at 7½ ips, the top theoretical frequency is 30 cycles.

Angle vs response

This reminds us that we had best consider the effective gap width and the frequency response for the angle we intend to use. In Fig. 4 we have illustrated what happens in our three-channel system, but the same thing happens to any number of channels. As illustrated in Fig. 4-a, the vertical signal width equals W(1/cos 0°), or W, where W represents the original gap width. For the second angle, the effective width equals W(1/cos 45°), or 1.4 W. For the third channel, it is W(1/cos 60°), or 2.0 W. This is shown in Figs. 4-b and 4-c.

Since the top frequency is inversely proportional to the gap width when the tape speed is constant, the result is that the top frequency for channel 2 is 0.7 times channel 1's top. And channel 3 is 0.5 or ½ the maximum frequency of channel 1.

This novel way to increase the amount of information recorded on a magnetic tape won the author a prize in a New Jersey science-fair competition for high-school students last year. The editor and several experts in tape recording were so impressed with the originality of the idea that we asked Mr. Maskasky to write an article describing it. The author has since graduated from high school and is now enrolled at the Massachusetts Institute of Technology, the first step, we are sure, to a successful career in electronics.

A few practical experiments showed that any recorded selection with an angle greater than 70° was too poor in quality and too difficult to tune to be of any use. This is why 60° was chosen as the largest for three channels, leaving 45° as the best possible choice for the other angle.

The measured crosstalk for two channels (0° and 60°) was better than −60 db. For three channels (0°, 45° and 60°) it was −46 db between the second and third channels, and −52 db for the second and third signals on the first.

In making the pivotal apparatus to mount the tape head:

▸ Use extremely flexible audio lead to the tape head or it will break under the constant stress.

▸ Pivot the tape head around its central axis to get symmetrical recording for best results.

▸ Eliminate all play or looseness. If you don't, you will be extremely lucky to find your original signal.

▸ Locate the vertical signal in its normal position on the tape to get twice the time by flipping over the reel.

▸ Disconnect the erase head before attempting to record.

The tape head pivoting device I used is shown in the photos. It was custom built. However, there are other methods that can be used. A multi-position rotary switch might make a good replacement for the 90° drive shown. Or the spring stops could be taken out of the switch and friction used to maintain a constant setting of tape head. This would be done by placing a spring on the shaft driving a metal plate on the "free" end to form a tight clutch against the housing.

This method of recording offers simplicity of operation, saving of money on prerecorded tapes, and no need for ultra-critical factory adjustments. The system does not eliminate the need for separate tracks. Instead, it enables us to put much more information on the width of tape used for each track.

Minor improvements in the apparatus and technique can raise the quality of this system to comply with high-fidelity standards. From there, the possibilities are limitless. END

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How to avoid losing your shirt on "no raster" calls

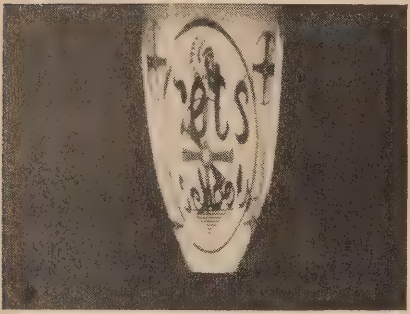

Fig. 1—This keystoned raster was caused by a shorted yoke.

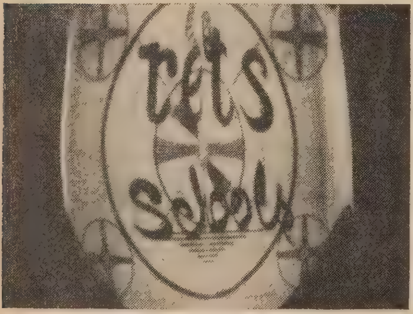

Fig. 2—Long narrow raster with a heavy drive line down the center was caused by the screen-grid resistor on the horizontal output tube increasing in value.

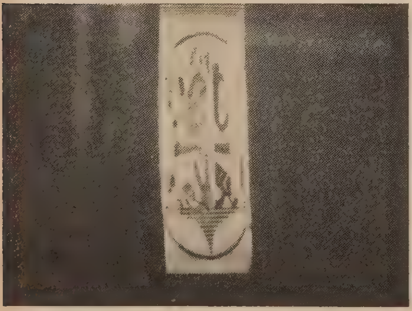

Fig. 3—Very narrow raster with an extreme case of poor horizontal linearity. Note foldover on left side of screen. A linearity capacitor (B-boost filter) had decreased in value.

By DELLROYE D. DARLING*

Ask the average service technician what's the toughest part of his business and he will say, "Estimating!"

Most customers are pretty insistent about learning the price of a repair job before they give an OK to go ahead. On some complaints a good technician can pretty well guess from the symptoms just about what the job will cost. But what do you do when the only symptom you have is no raster?

You can pull the anode lead and check for high voltage by arcing it to the chassis but, if high voltage is missing, (and it usually is in these cases), you still don't know very much.

Is it the yoke? Maybe. On the other hand, it could be the horizontal output transformer, or no B-plus, or an open screen grid resistor on the horizontal output tube, and so on. All these can kill the raster, but an estimate based on a burned resistor will hardly cover a shorted flyback transformer.

The main difficulty is that even though these troubles cause symptoms of their own which could be used to identify them, they all cut off the high voltage, so the identifying symptoms can't be seen.

Now, signal substitution from a working set to a defective one is nothing new, nor is high-voltage substitution. However, even many technicians who use this technique don't realize how much it can simplify estimating, and so don't use it often enough. Even if estimating isn't the real problem, substitution can save time, and time is money!

Case history

Let's take a typical case. You have a 21-inch Motorola on the bench. It has no raster, and the customer wants an estimate. Ordinarily, we would almost have to repair the set before we could tell all that was wrong with it. But let's do it the easy way.

Take another set — any set that has normal high voltage — and set it up alongside our dog. Plug both sets in and turn them on. Naturally, the outside man has tried tubes, so we shouldn't need to go into that. Pull the anode lead out of the pix tube connector on both sets. Connect a jumper between both chassis. Connect a *well insulated* jumper between the anode lead on the good set and the anode button on the defective one. (It's a wise idea to turn the "good" set off while making this connection.) Make sure the brightness control is turned well up on the dog. Aha! Now we have a raster. But look at its shape. (Fig. 1) It's trapezoidal, or keystoned.

Any good technician knows the one thing that can cause keystoning. This set has shorted turns in the deflection yoke. Now we have something on which to base a reasonable estimate.

Take another step

But wait, why not kill two birds with one stone? Every once in a while we make an estimate based on no raster, the customer OK's the job, then when we fix the raster problem we find the set also has video troubles that we couldn't see before. This means persuading the customer to accept an increased estimate so the job can be completed. This seldom improves his opinion of TV service technicians.

As long as we have the high voltage from the good set giving us a raster, why not connect an antenna to the defective set and have a look at the picture? Naturally, if the raster is distorted, the picture will not be completely normal, but we can at least tell if the contrast is correct, all channels present, sync OK, etc.

Other troubles

Let's see what symptoms some other no-raster troubles can cause. Suppose our high-voltage substitution reveals a narrow raster with a very bright drive line down the center (Fig. 2). This is a sign of an overdriven horizontal output tube. If the tube is good, there is one other common fault that can cause these symptoms — an increased value of the screen-grid resistor in the horizontal output tube circuit.

Ordinarily, we know that defective vertical circuits can cause a single horizontal line on the screen. However, if something has shorted in the vertical section (usually supplied from boosted B-plus), it can also cause loss of raster. High-voltage substitution will produce the horizontal line that tells us definitely that the trouble is in the vertical section.

A narrower-than-usual raster with extremely poor horizontal linearity (Fig. 3) can be caused by a shorted linearity coil. This set does not have a linearity control, but a little thought suggested that the trouble might be in a linearity capacitor (B-boost filter). Sure enough, one of them had decreased from 0.1 μf to a negligible value.

Although any technician is familiar with a horizontal white line on the screen caused by loss of vertical sweep, not many have seen a vertical line (Fig. 4), because most faults that can produce this condition also kill the high-voltage supply.

Several things can cause this line, but much can be learned from it. For

---

*Director, Industrial Electronics Radio Electronic Television Schools, Detroit, Mich.

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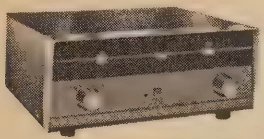

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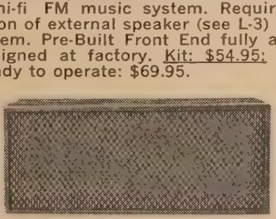

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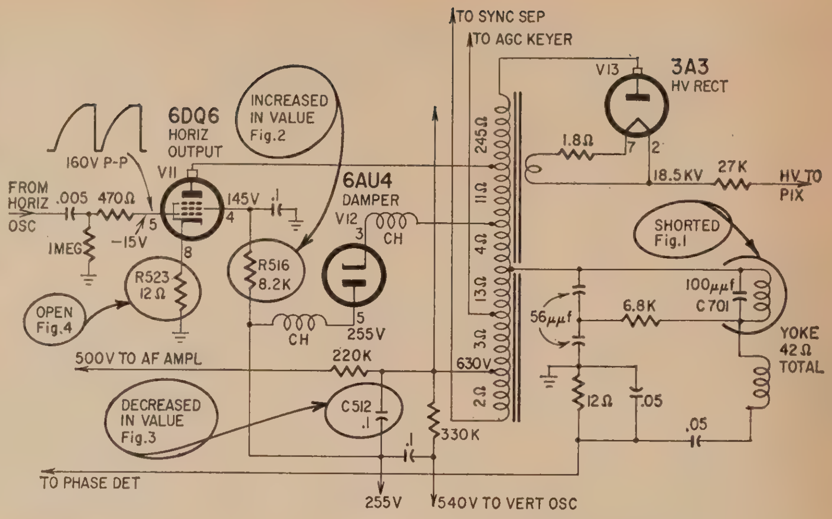

Motorola TS-544A-00 high-voltage circuit used as example in this article.

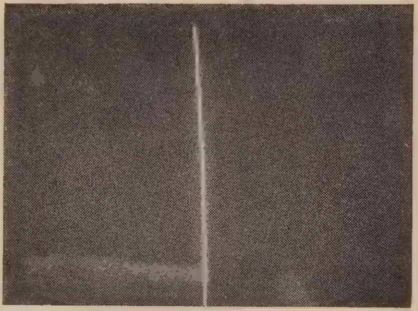

Fig. 4—Open cathode resistor in the horizontal output stage will produce this symptom of no horizontal sweep.

instance, the fact that the vertical sweep is operating to some extent indicates that the damper tube is at least conducting (in a modern series damper set). This time it was caused by an open cathode resistor in the horizontal output stage.

Now, every story has two sides, and this one is no exception. High-voltage substitution is no magic wand. Even a good man who has used the idea for some time will occasionally make a wrong diagnosis. It is a qualitative tool, somewhat like an oscilloscope. It doesn't read good–bad like a tube checker. We have to learn to interpret what we see, mix it with some experience and come up with an educated guess. However, no really good technician needs to be told that anything that will improve his guessing will improve his income and his disposition, too! END

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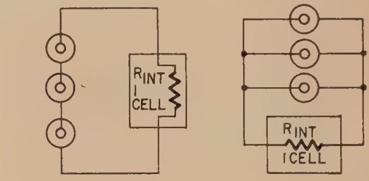
Too-Automatic Tuner

This chassis uses an ultrasonic automatic tuner circuit, operating around 45 kc or so. When horizontal hold was thrown off freqeuncy, either the fundamental or a harmonic, radiated as sonic waves by the flyback or yoke, got into the input of the automatic tuner, which is a microphone at the front of the chassis! Turning the horizontal hold control would cause the auto-tuner to react on one of its functions, depending upon the frequency being generated by the horizontal output at the time!

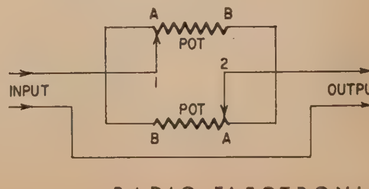
Black Box No. 4



The black box contains a resistor equal to the internal resistance of one cell, as shown in the figure. When the cells are in series, the current is equal to the total voltage divided by the sum of the resistances of each of the cells plus the resistor in the box. With the cells in parallel, the voltage of one cell is applied to the resistance in the box plus the resistance of one cell divided by the number of cells. Try it with a couple of examples!

Why the Decrease?

Let's look inside.



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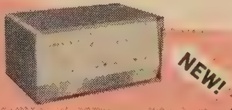

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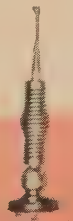

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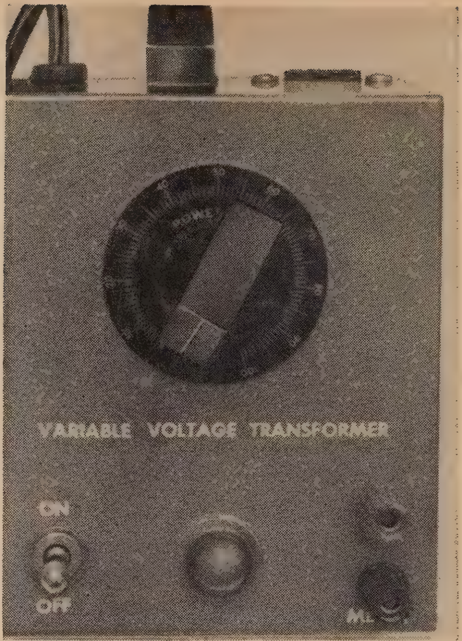


Output voltage is variable from 0 to 135 volts and may be metered from posts on panel.

By L. A. JAMES

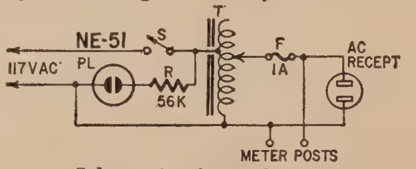
MANY pieces of equipment found in industrial and commercial electronic laboratories would be valuable in the home electronic workshop. Many of these are too expensive for once-in-a-while use, but this one isn't. One of the most often used pieces of equipment in the professional lab is a variable-voltage transformer. This type of transformer is available under such trade names as Variac, Adjust-A-Volt and Powerstat. Prices run from $8.50 to over $100.

For the average home workshop, the smallest size, 165 volt-amperes, should be adequate. It can be connected so that it will provide an output from 0 to 135 volts. For those of you who aren't familiar with the variable-voltage transformer, perhaps a word of explanation is in order.

Round laminations are used. Along one side, the enamel is removed from the wire and a contact brush rides on this scraped wire. You may remember that a toy-train transformer is made somewhat like this. Since the variable-voltage unit is round, it is hard to handle and set up for use. Several dollars can be saved (and some enjoyable hours had) by making the housing and mounting and wiring the components yourself.

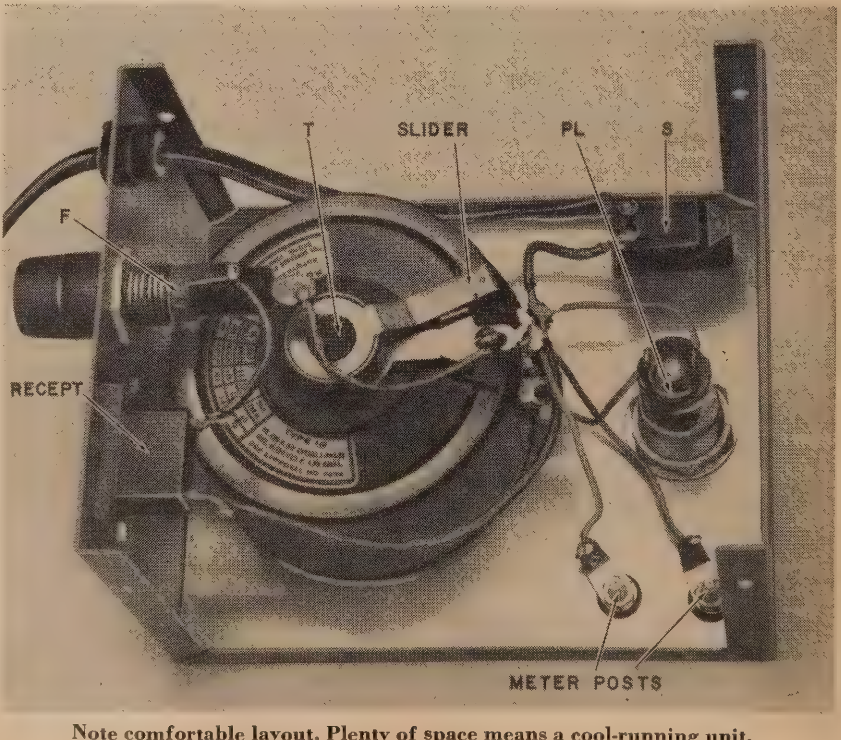
A fuse holder, pilot light, on–off switch, ac receptacle and a pair of binding posts are added to make the transformer more useful. The binding posts are very handy for connecting a meter to monitor the output voltage. The photographs show how the parts are mounted. Be sure to use as least No. 18 hookup wire, on all connections (except the pilot light and voltmeter terminals. You will note that the fuse holder is wired between the transformer and receptacle. A 1-ampere fuse gives the maximum amount of protection to the transformer (rated at slightly over 1 ampere) which is the most valuable component in the circuit.

After wiring, the unit should be tested. If you have an ac voltmeter, use it; if not, a light bulb can be connected to the receptacle. With the transformer set at zero, turn on the power. The pilot light should glow. Slowly advance the control knob and the output voltage will increase and the bulb will glow more brightly. Remember that you can get up to 135 volts from the unit, which may burn out the bulb. As you find more and more uses for this piece of equipment, you will wonder how you ever got along without it. END

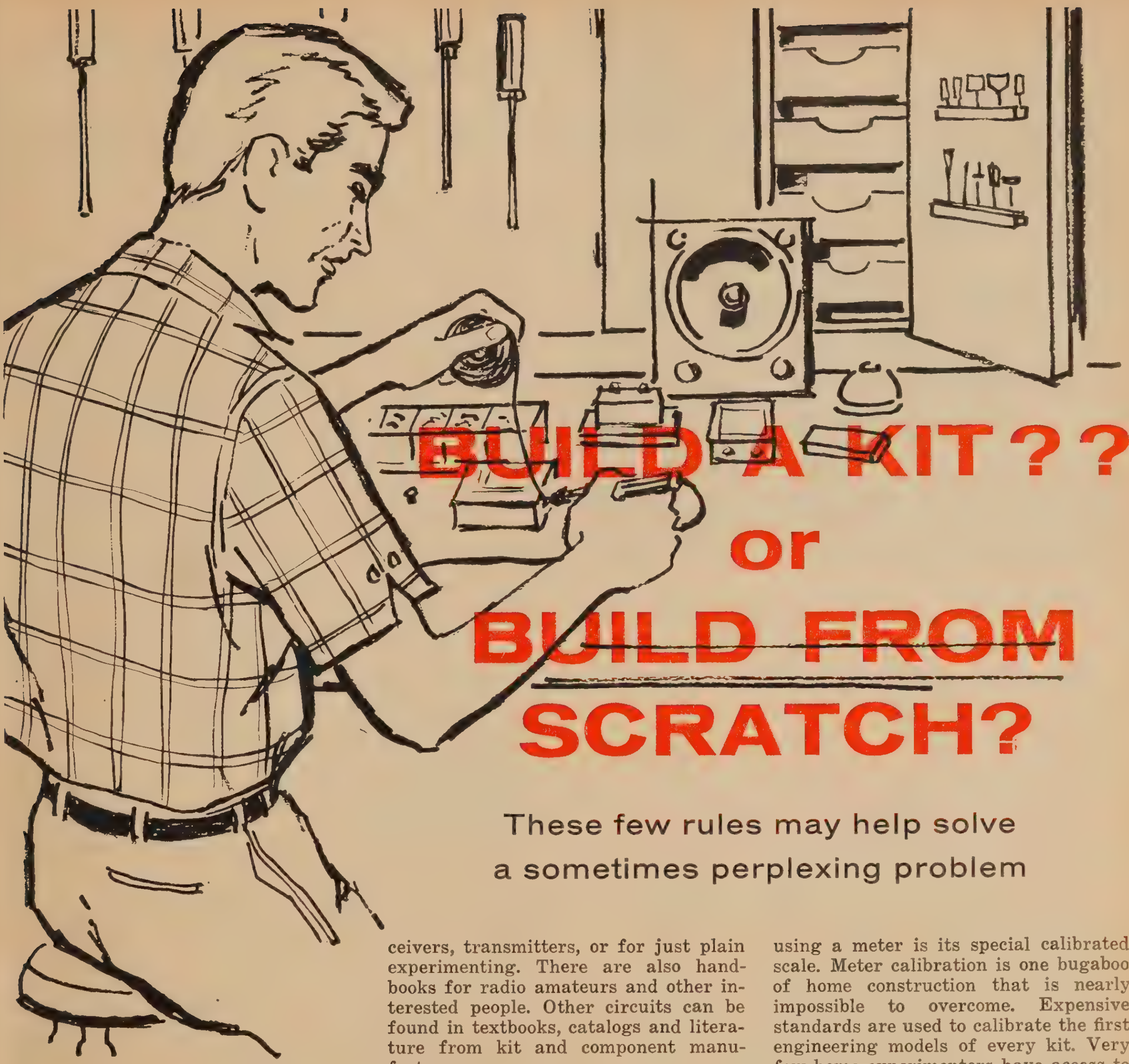


Schematic of transformer.

R—56,000 ohms, ½ watt, 10%
(use only if pilot assembly does not have built-in resistor)
T—0–135 volts, 165 volt-ampere variable transformer (Powerstat model 10 or equivalent)
F—1 ampere, 250 volts and fuse holder
S—spst toggle
PL—NE-51 and pilot assembly (Dialco 931 or equivalent)
Binding posts
Ac receptacle (Cinch 2R2 or equivalent)
Case 3 x 4 x 5 inches



Note comfortable layout. Plenty of space means a cool-running unit.



BUILD A KIT ?? or BUILD FROM SCRATCH?

These few rules may help solve a sometimes perplexing problem

By JAMES A. FRED

TO PARAPHRASE WILLIAM SHAKESPEARE, "To build a kit or not to build a kit, that is the question." The old-timers are amazed to see so many thousand kits being built, while hardly anyone builds a piece of electronic equipment from scratch. Time was when most hobbyists designed their own units, fabricated the sheet metal, mounted parts, wired, tested and finally used the item. Now the electronic enthusiast sits down with a catalog of kits and in a few minutes has made his choice and sent in the order. As one of the few survivors who like to build from scratch, I decided to examine the pros and cons of each side—see if I could find out why kits are so popular.

There is no shortage of good construction articles on almost any facet of electronics, in this and the other magazines devoted to electronics. You can find circuits for audio amplifiers (mono or stereo), test equipment, receivers, transmitters, or for just plain experimenting. There are also handbooks for radio amateurs and other interested people. Other circuits can be found in textbooks, catalogs and literature from kit and component manufacturers.

Attractive metal cabinets to house the home-built equipment are far easier to get than when everyone built from scratch. More than a half-dozen companies specialize in metal cabinets and chassis of all sizes, shapes and descriptions. They also come in several materials and colors.

More parts and components are available than ever before. You can obtain them by mail, wherever you live, at attractive prices. All the magazines carry advertisements of new and different components as soon as they become available. Meters are available to measure any value of voltage, current or resistance.

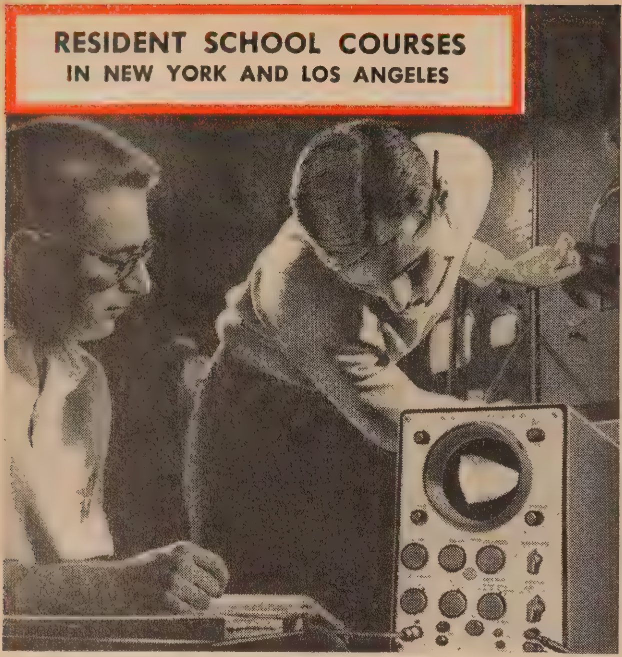
On the other hand, did you ever try to figure up the cost of all the parts in a kit? We did. The price of the parts contained in a kit would cost twice as much as the kit if they were purchased separately. There are also special parts in many kits that would be hard or impossible to purchase.

One outstanding feature of any kit using a meter is its special calibrated scale. Meter calibration is one bugaboo of home construction that is nearly impossible to overcome. Expensive standards are used to calibrate the first engineering models of every kit. Very few home experimenters have access to precision standards such as those needed for meter calibration. The printed or silk-screened meter scale is also out of reach.

One thing that sets a kit apart from home-made equipment is the front panel. Most kits use a silk-screened or etched design on the front of the cabinet. The cost of the artwork and making the screen often exceeds the cost of a complete kit.

Another desirable feature of a kit is the calibrated frequency dial. Just as in the case of the meter scales, expensive signal frequency standards are needed to calibrate the prototype dial scales. The home experimenter does not have these frequency standards.

Many experimenters have boxes of radio parts on hand in the so-called "junkbox". I know one who has been accumulating components for over 14 years. He has salvaged many war surplus parts, he has junked several TV sets and has had many items given to him. This man seldom buys a kit be-



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cause he has almost all the parts needed for any project he may decide to work on. He also enjoys the mechanical work that goes into laying out sheet metal and drilling and punching the holes.

Building a kit gives this man very little challenge. He owns only two kit instruments even though he has wired and assembled more than 30 kits for other people. He built his kit oscilloscope according to the instruction manual and it is still in its original form. His other kit, a vtvm, has been rebuilt into a panel-mounted instrument. He replaced the slide switch with a toggle switch, added a fuse holder, a pilot light, five-way binding posts and an improved type dc connector. This instrument is now the equal of any industrial type meter made.

There is another angle to remember in the kit business. Many times medium-quality parts are used because the kit must be designed to sell for a certain price. In lower-priced kits there are often no fuses or pilot lights, and the power switches may not be of the best design. If you built your own equipment using war surplus parts you would have a superior piece of equipment, since the government used the finest, most expensive parts available.

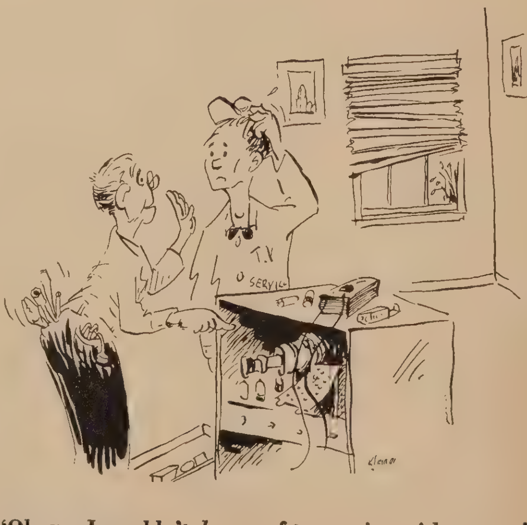
You can see there is a lot to be said on both sides of the question. If you are simply interested in having a piece of test equipment or an amplifier and don't get any special kick out of construction, a kit is for you every time. You will have less trouble and better results.

If, on the other hand, you are a designer at heart, get more kick out of building the instrument than in using it, and have had to modify the kits you have built to satisfy your requirements, kits are not for you. You would simply be bored with the work of assembling them, and not fully satisfied with them after they were built.

But if you find yourself somewhere between these two groups, these general rules may help you:

1. If you have no accumulation of parts, by all means buy a kit.
2. If the most important part of the instruments is a calibrated meter or frequency dial, buy a kit.
3. If the new parts you need, in addition to what you already have, cost more than the kit, then buy the kit.
4. If the instrument you want has no dial or meter, then you should build it from scratch.
5. If you have all the necessary parts on hand, then you should build the device from scratch.
6. If you need a piece of equipment that isn't available in kit form then you have no choice, you must plan and build it.

Many experimenters who are new at our hobby will find new joy and satisfaction from building some electronic project up from scratch. They will develop new skills as well as a deep down feeling of fulfillment in a project that they carried through from design to finished product. END



"Oh, no, I wouldn't *dream* of tampering with our set!"

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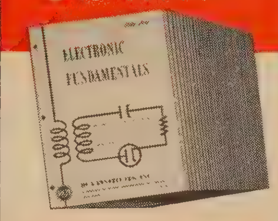

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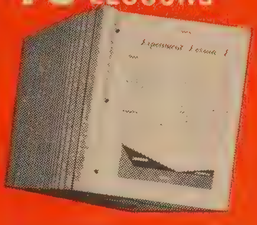

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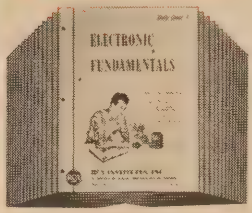

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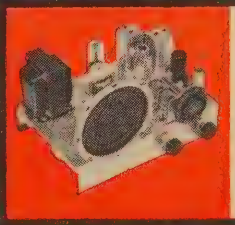

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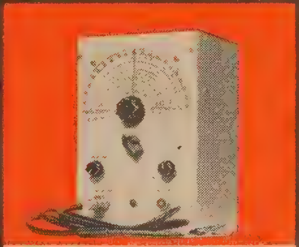

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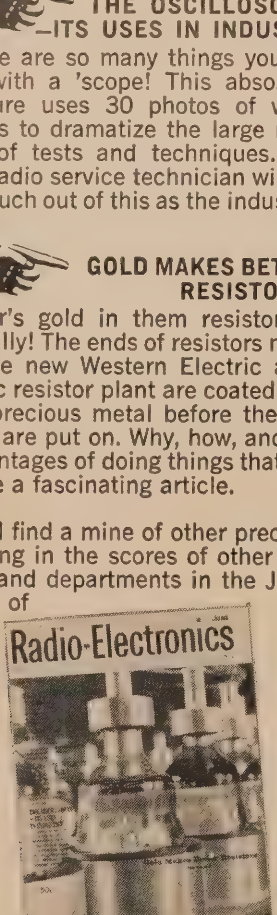
You'll find a mine of other precious reading in the scores of other articles and departments in the JUNE issue of



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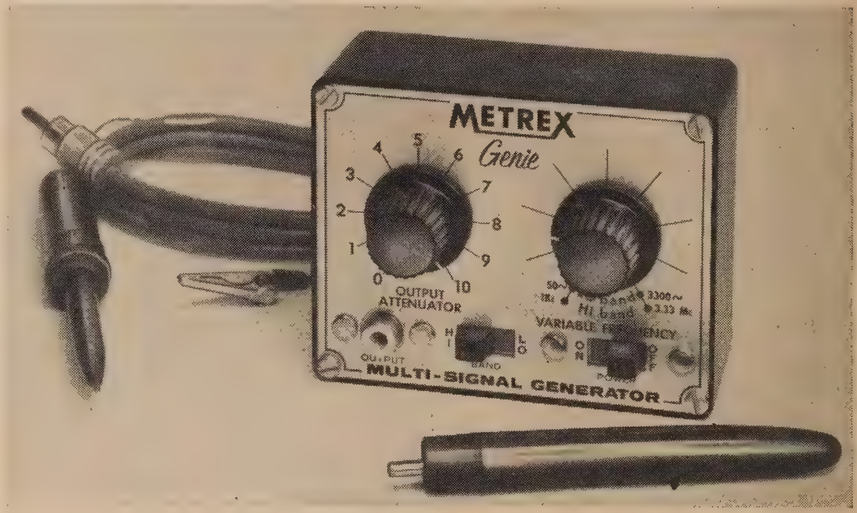


This 3½ x 1½-inch instrument is a complete transmitting station.

tool box SIGNAL INJECTOR

Pulse generator supplies signals over wide range.

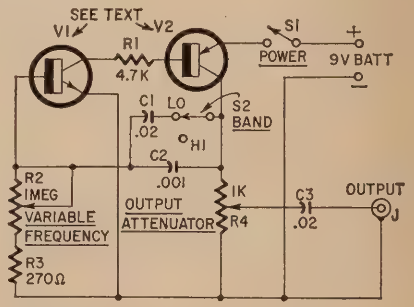
By HENRY LEVINE*

THIS LITTLE UNIT IS A COMPACT, RUGGED, battery-operated, all-transistor variable signal generator covering 50 cycles to 3.3 mc. Its output voltage is continuously variable from zero to 9 volts, peak-to-peak. This is enough to drive a speaker's voice coil directly, making the unit useful when troubleshooting transistor radios, amplifiers, tape recorders, TV, etc.

The Genie's frequency range is in two overlapping bands (fundamental square-wave pulses). The low band runs from about 47 to 3,300 cycles; the high band from 1,000 cycles to 3.33 mc. Its output consists of very short duration pulses having an excellent flat top and extremely short rise and fall times. Harmonics go well above TV channel 13, thus permitting direct injection into vhf TV tuners.

How it works

When the power switch is turned on (see Fig. 1), the current flows momentarily through R4 from V2's collector. The drop across R4 causes a positive pulse through C2 (or C1 and C2) to be applied to the base of V1. The positive pulse on V1's base creates a greatly amplified collector current, which flows through R1 into the base circuit of V2, causing the collector current of V2 to continue to rise. This ac-



R1—4,700 ohms
R2—1 meg pot, special audio taper
R3—270 ohms
R4—1,000 ohm pot, linear
C1—.02 ceramic
C2—.001 ceramic
C3—.02 ceramic, 600 volts
J—phono output jack
S1—on-off switch
S2—bandswitch.
BATT—9 volts, mercury type.
V1, V2—Transistors—1 n-p-n, 1 p-n-p.
Several types have been used. Almost any low-cost transistors with the requisite frequency range and polarity will work well here.
Miscellaneous knobs, panels, hardware, case, etc.
(The Genie is also available in wired form from Metrex 519 Hendrix St., Brooklyn 7, N.Y.)

Fig. 1—Generator uses a p-n-p and n-p-n transistor.

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*Electronics field engineer.

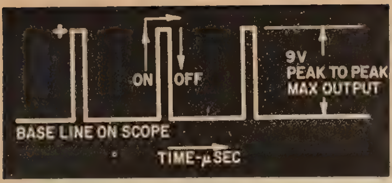

Fig. 2—The Genie output waveform.

tion is so rapid (millimicroseconds) that V2 is brought into saturation abruptly, causing a flat-top pulse.

Now there is no increase in the voltage drop across R4, V1's current drops, and an abrupt negative fall in V2 collector current causes V1 to go sharply into nonconduction and thereby cut V2 off. R1 (4,700 ohms) limits the maximum base current of V2 for a maximum collector current of 9 ma, the saturation point of V2.

C1 and C2 are chosen to permit R2 (a special-taper 1-megohm potentiometer) and R3 (about 270 ohms) to tune over the band of frequencies or pulse repetition rate.

A pulse of this type can readily shock-excite an inductance or tuned L-C circuit at its own natural resonance frequency, causing a series of damped sinusoidal waves, modulated by the repetition rate of these pulses. (Fundamentals are 50 cycles to 3.33 mc.)

A 600-volt blocking capacitor protects the instrument and the equipment being worked on. Battery life of the portable tester is equal to shelf life or about 1 year.

Four controls are available to the technician using the Genie. An ON-OFF switch (its function is obvious); an OUTPUT ATTENUATOR which varies signal strength from zero to full output; a VARIABLE FREQUENCY control which varies the frequency over the range selected with the HI-LO band switch.

As the unit uses only transistors, there is no warmup period, and no hum is introduced into the circuits being tested as a pure dc (battery) supply powers the unit. Fig. 2 shows the output waveform of the tester as seen on a scope with excellent high-frequency and square-wave response.

Now let's try some actual servicing procedures which will demonstrate how the Genie is used and what the technician can do with one.

Amplifiers, PA, hi-fi and intercoms

Complaint: Low gain or dead amplifier. B-plus is OK.

Test procedure: 1. Warm up the amplifier and turn on your Genie. Flip the bandswitch to HI and turn the VARIABLE FREQUENCY control completely counterclockwise (approximately 1,000 cycles). Turn the OUTPUT ATTENUATOR fully clockwise and clip an output cable across the woofer speaker's voice-coil lead points A in Fig. 3. If the speaker is good you'll hear a tone. No tone means an open voice coil.

Now turn the output control all the way down and clip leads to points B. Increase the output. If the output transformer is good, you will hear the tone again. Without changing the output control setting, apply the generator to point C. The tone should be louder. Go back to D. If the tone weakens, suspect the coupling capacitor.

In this way, checking back through H, it is possible to check almost every component in the amplifier as fast as you can clip and unclip the leads. An especially interesting test is at I. Any strong response here indicates a low-capacitance cathode capacitor.

If you can check back to the source (microphone cable, phonograph or tape input), shorts or opens in the cable can be picked up quickly.

Transistor radios

After checking all voltages with a voltmeter, inject a 1,000-cycle signal into the voice-coil terminals, as if checking an amplifier. Then go back through the audio section, remembering to *keep the signal down* so as not to overload the transistors. Your strongest signal level is needed for voice-coil testing only.

Check the volume control at points A and A1 (Fig. 4). Vary the volume control, noting its action.

Shift the BAND switch to HI and inject a signal between point B and ground. Adjust the VARIABLE FREQUENCY control for loudest signal. Go back through C, D and F, watching for a signal increase as you move from the collector to the base of the transistor. Point E checks the emitter bypass capacitor. If you get a strong signal, the capacitor is open. Inject a signal into G to see if the oscillator transformer is open or shorted or if the tuning capacitors are shorted.

Continue back toward the antenna, clipping the Genie from point H to ground to see if the signal is being passed on to the if circuits. It may be useful to vary the frequency again for best output. Point I checks overall if gain and also the input of the converter transistor. The rod antenna may be found useful when checking rf stages.

Aligning the rf stages

First adjust the oscillator trimmer to bring in a broadcast station near 1600 kc at the correct point on the dial. Now turn the dial to a clear spot on the high end of the dial (between 1400 and 1600 kc). Loosely couple the Genie output to the antenna coil or lead, selecting a signal of approximately 1000 kc on the high band. Adjust the rf and antenna trimmers, keeping the Genie output low so as not to activate the avc circuits of the receiver.

To adjust the oscillator padder (usually the core of the rf coil), turn the receiver to the low end (600 to 620 kc) and inject a weak signal by radiation from the rod antenna. Adjust the padder for maximum output, again being careful to keep the signal low. Recheck at the high end after the padder adjustment.

To check video circuits

Inject a strong signal into the kinescope input circuit (grid or cathode). Select a frequency from 1,000 cycles down. If the input to the picture tube is OK, bars will be seen sharply on the screen. Adjust the Genie frequency till a convenient number appears. Then work back as in an audio amplifier, watching for any sudden falling off of signal or failure to increase in gain when moving from one stage to another.

(By varying the frequency of the Genie, you can lock in the vertical or horizontal circuits for a rough sync circuit check.)

Troubleshooting tape recorders

The amplifier of a tape recorder is checked as described for audio ampli-

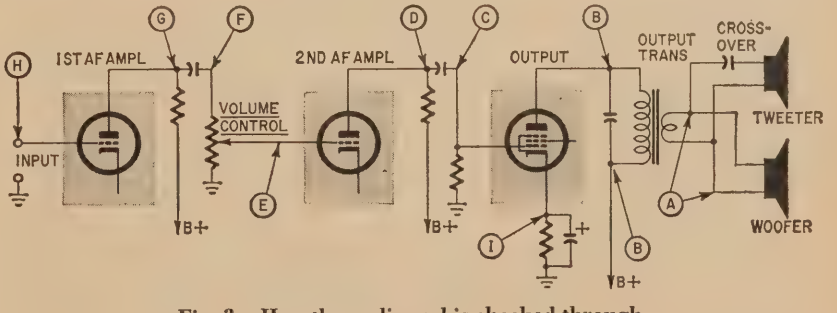

Fig. 3—How the audio end is checked through.

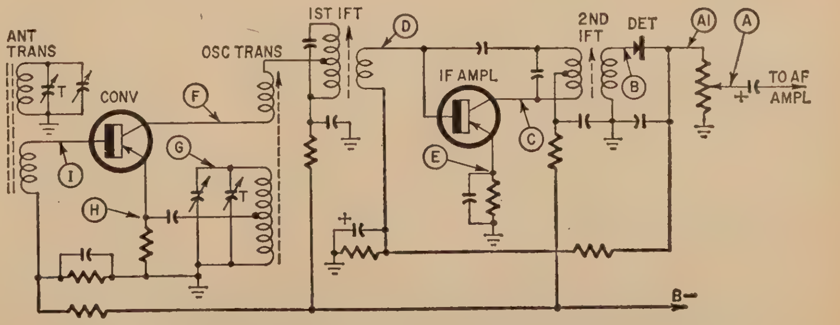

Fig. 4—Check points for a transistor radio.

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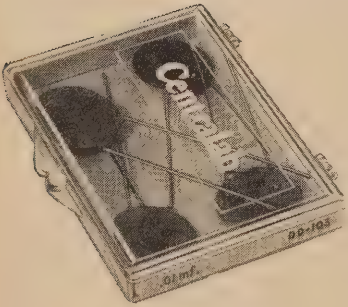

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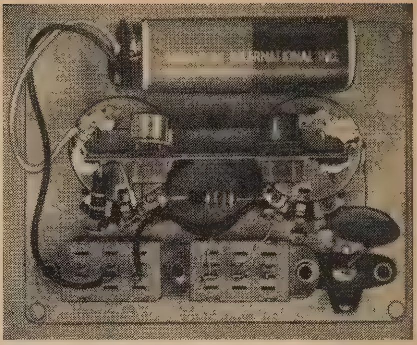


Inside view of Metrix Genie.

fiers. To check the head, make a small induction coil by winding about 50 turns of fine wire (No. 30 or smaller) on a dowel or old alignment tool with a diameter of ¼ inch or less. Leave leads about 12 or 18 inches long, solder them to an RCA type plug and plug into the Genie. Now you can couple a signal into the head by induction, as indicated in Fig. 5. Bring the coil as close to the front of the playback head as possible. If a loud tone is heard, the head is good. No sound or weak sound might indicate a defective coil in the head, broken leads or improper connections.

Other tests

The Genie has a large number of uses. Hooked up to the input of an amplifier, it can, for example, check the speakers for rattles. Simply rotate the frequency control slowly. If the speaker tends to rattle at any point, the rattle will be heard as the Genie is tuned past that frequency.

A rough square-wave test may be made by setting the Genie to produce a square wave on the scope, with scope vertical amplification at its greatest. Now turn the scope amplification down, attach the amplifier output to the vertical terminals, and apply the square wave to the amplifier input. Compare the amplifier output with the original square wave as seen on the scope.

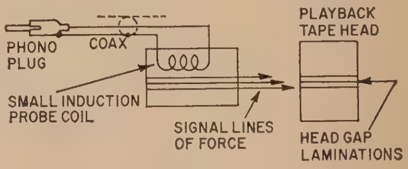


Fig. 5—Checking a playback head.

Faulty shielding or internal breaks in cables may be discovered by using them as input cables to an amplifier, then sliding the Genie rod antenna along the outside of the cable with the Genie output at maximum. As the rod is slid toward the amplifier, a sudden increase in signal indicates the point of poor shielding or the break.

Various other uses will occur to the technician. The Genie has been used for a large number of checks and tests, even including (with the help of a scope) if transformer testing. Wherever a signal ranging from low audio to high rf is needed, the Genie will do the job. END

The Marvelous Automatic Tube Bopper

I GO OUT ON THIS CALL AND THE lady starts talking. "This is a real good set. It's got written circuits."

"Written circuits?" I asked.

"Of course," she said, "the ones before printed circuits."

"Oh," I said.

"You don't seem to know much about TV sets," she said. "Do you think you can fix this one?"

"I'll try," I replied.

I checked the set and told the lady, "You have an open cathode."

She seemed highly insulted until I made it clear that I was not referring to her clothing or anatomy.

"Look," I pointed out. "When the picture gets dark, I can hit the neck of the picture tube and it gets bright again. You have an open cathode . . . in your picture tube," I hastened to add. "I can try to weld it closed but you might need a new picture tube."

This turned out to be stubborn one that wouldn't weld. "You need a new picture tube," I told her.

"I don't want a new picture tube. Just leave the back off and I'll hit the tube every time it gets dark."

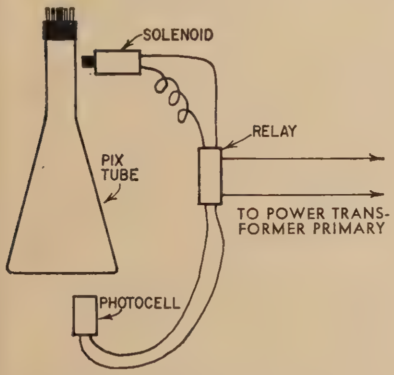
"I can't do that," I said. "You go sticking your hand back in there and you'll light up like a pinball machine."

"Well, I can't afford a new picture tube. Can't you fix it without one?"

"No new picture tube?" I asked.

"No new picture tube!"

"Well, I'll see what I can do." Reaching into my handy tube caddy, I pulled out a photoelectric cell, a relay and a solenoid which I just happened to have with me. I mounted the photocell in front of the picture tube and the solenoid on its neck and hooked up the circuit (see diagram). I set the cell so that when the picture got dark, the photocell activated the relay and the relay closed the circuit that caused the plunger of the solenoid to shoot out and bop the neck of the picture tube, making the picture bright again.



"There you are, lady," I said. "It works without a new picture tube."

"Well, I must say you really know your TV repairing," she purred.

I think I'll apply for a patent.—*David W. Cramp*

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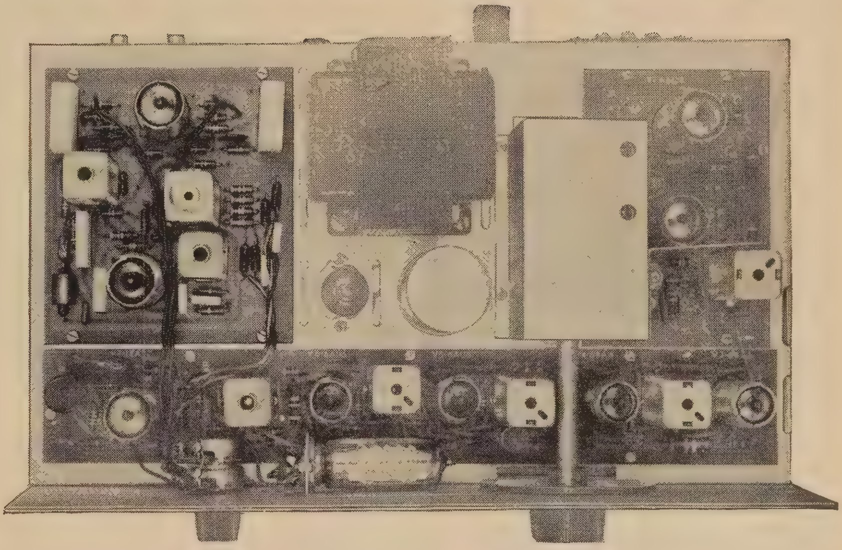

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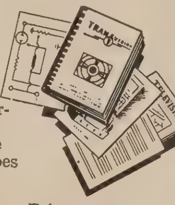

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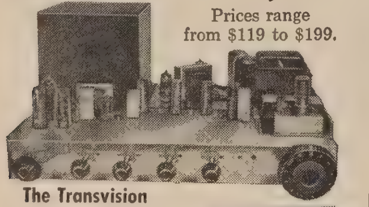

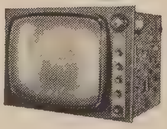

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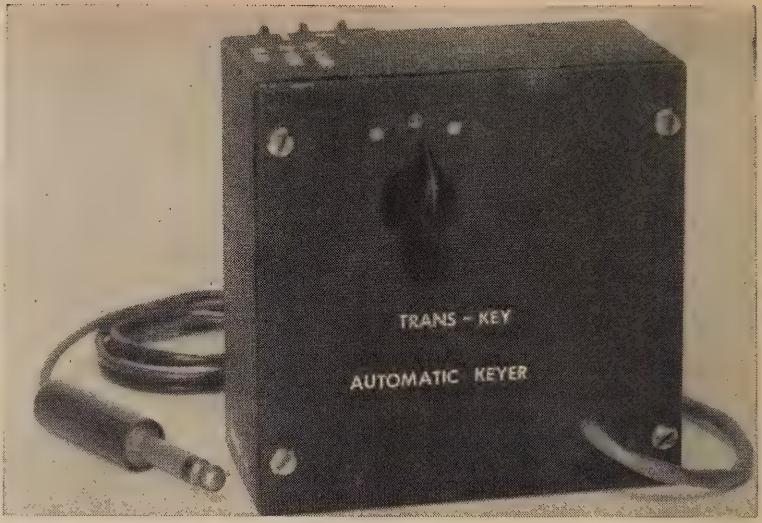


Cable at right goes to key. Cable at left of Trans-Key plugs into transmitter.

ELECTRONIC KEY

By
DAVE STONE

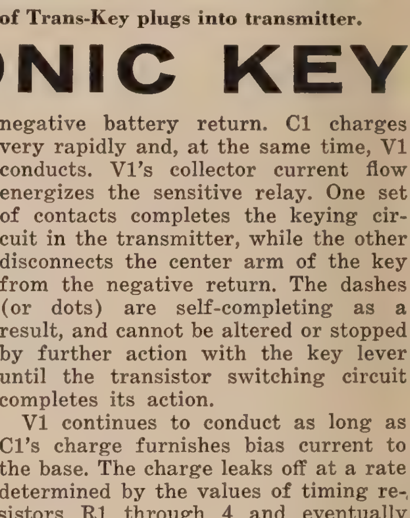
THE Trans-Key is a transistorized electronic key which will do much to provide perfect code transmission for hams. A light, compact and low-power unit, it is suitable for portable and mobile as well as fixed-station use. The speed and duration of the dots and dashes are selected with a single control. Power requirements are a modest 12 volts at 10 to 20 ma (higher current drain on the higher-speed ranges). Power can be supplied in a variety of ways—dry cells, car battery or low-voltage power supply.

Circuitry

Each transistor is connected as an on–off switch to furnish current to a sensitive relay in the collector circuit. When the key lever is pushed to the left for a dash and released, capacitor C1 is temporarily connected to the negative battery return. C1 charges very rapidly and, at the same time, V1 conducts. V1's collector current flow energizes the sensitive relay. One set of contacts completes the keying circuit in the transmitter, while the other disconnects the center arm of the key from the negative return. The dashes (or dots) are self-completing as a result, and cannot be altered or stopped by further action with the key lever until the transistor switching circuit completes its action.

V1 continues to conduct as long as C1's charge furnishes bias current to the base. The charge leaks off at a rate determined by the values of timing resistors R1 through 4 and eventually drops low enough to cut off the transistor (and release the keying relay).

The same action takes place with V2



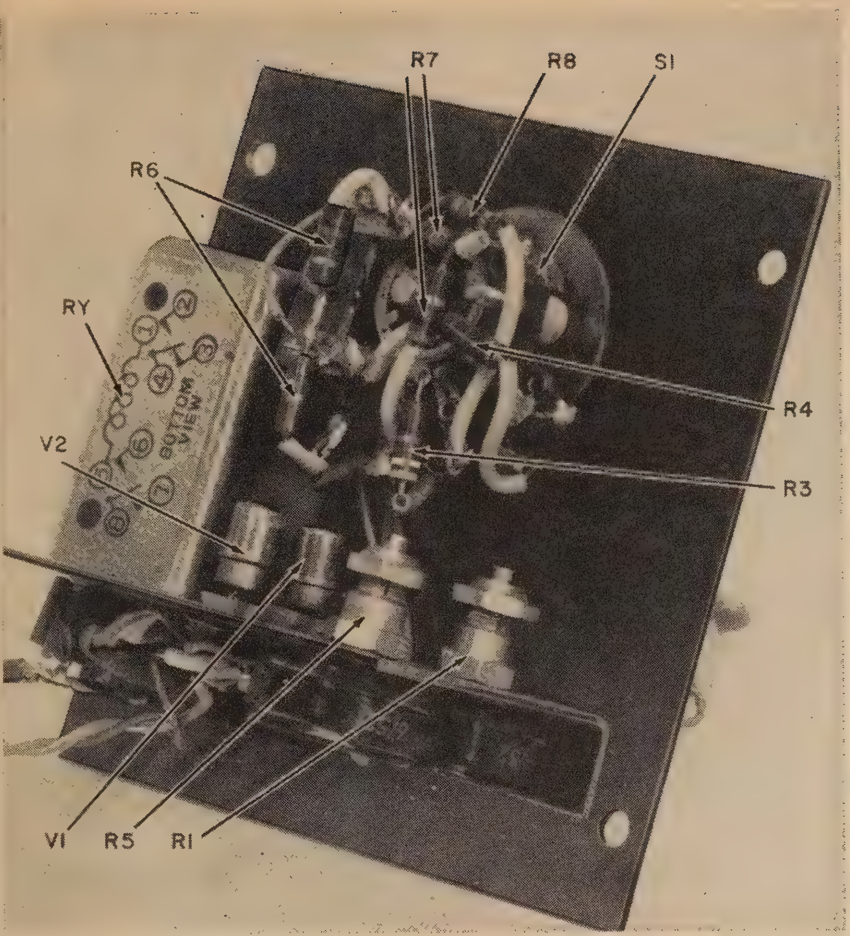
R1, 5—pot, 5,000 ohms, linear taper
R2—2,200 ohms
R3—3,900 ohms
R4—6,800 ohms
R6—820 ohms
R7—2,000 ohms, 5% (or two 1,000 ohm resistors in series)
R8—3,000 ohms, 5%
R9—2,200 ohms, if needed
All resistors ½ watt 10% unless noted
C1, 2—25 μf, 10 volts, tantalum
V1, 2—2N223 or 2N109
RY—5,000-ohm plate-circuit relay (see text)
S1—2-pole 3-position rotary switch (shorting or nonshorting)
Modified speed key, see text
Cable, 3 wires, for key
Metal box, 4 x 4 x 2 inches (Bud C-1793 or equivalent)
12-volt dc power source
Plug to fit transmitter jack (and cable)
Sockets for V1, 2

Trans-Key schematic. Use R9 when dashes can't be made long enough with R1.

BENCH TESTED

Two transistors
Three ranges—8, 12 and 15 words per minute (with given resistor values)
Draws only 20 ma at 12 volts dc

The keyer works well, dots and dashes are clean-cut and accurate. Dashes seem to be a bit short when compared with dot length, but adding R9 corrects that.



Interior of Trans-Key.

when the key lever is pushed to the right. V2 conducts approximately a third as long as V1 due to the lower values of R6 through 8. With the timing resistors shown, the speed ranges are approximately 8, 12 and 15 words per minute.

Construction

The layout and construction of the Trans-Key are not at all critical. My unit is built into a 4 x 4 x 2-inch utility box with attached shelf, and all components fit comfortably. The SPEED switch (S1) is mounted on the front panel. Two cables run from the back of the cabinet to connect to a modified speed key and the transmitter's keyed circuit. The speed key was modified to provide separate contacts on each side of the key lever, and a separate binding post was added to the key's base for the third connection. If you desire, a home-made key made from a strip of spring steel and a few pieces of hardware will do the job as well.

Most parts are readily available from the surplus-parts box. The relay was obtained from military surplus gear. Almost any sensitive type (1 to 3 ma at 5,000 to 8,000 ohms) can be used, if it has the required contacts—double-pole single-throw with one pair of contacts normally open and the other pair normally closed. I used a dpdt type with one set of contacts for the normally open pair and the other connected normally closed.

R6 and R7 are actually two resistors in series because they were readily available, but they can be replaced by single resistors of 820 and 2,000 (5%) ohms, respectively. R9 is needed only if dashes cannot be made long enough with R1.

If other speeds are desired, increase the number of switch contacts and resistance combinations. The ratio of V1's to V2's timing resistors should be approximately 2½ to 1.

Adjustments

After construction, connect the keying leads to a tone generator or a code-practice oscillator. Rotate S1 to the highest speed range and tap the key to produce dots and dashes. Listen to the duration of each and adjust R1 and R5 to get the proper time ratio. The dash should be approximately three times longer than the dot. Check these settings on the other two ranges and readjust if necessary. This is all that is necessary.

The relay's keying contacts can be used to key an oscillator or buffer stage in the transmitter as long as the contact ratings are not exceeded. The Trans-Key can also be used to key an audio generator in an alarm calling system as interrupted tones demand quicker attention. A compact code oscillator can be built in with the keying circuit in one enclosure. END

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Industrial Electronics Dictionary

from ultrasonics to X-ray tube

(concluding installment)

By ED BUKSTEIN

Ultrasonics: High-frequency vibrations above the range of human hearing. Ultrasonic generators usually employ a crystal transducer—the crystal transfers its vibrations into the surrounding medium—air, liquid, metal, etc. The magnetostrictive oscillator is sometimes used to generate ultrasonic vibrations. In this type, a metal bar inside an oscillator coil becomes alternately longer and shorter as the magnetic field alternates, transmitting vibrations into the surrounding medium.

Ultrasonic vibrations are used industrially for cleaning and "drilling" metals, for mixing liquids and for detecting internal flaws in metal structures by the echo detection (radar) method.

X-rays: A form of electromagnetic radiation of extremely short wavelength. The X-ray spectrum extends from approximately .06 to 120 Angstroms (an Angstrom is ten-billionth of a meter). X-rays are useful industrially because of their penetrating power, their ability to excite a fluorescent screen and their ability to expose a photographic film. (See Fluoroscopy and Radiography.)

X-ray tube: A tube specifically designed for producing X-rays. Electrons emitted from the tungsten filament of the tube are attracted to the target, a tungsten insert in the copper anode. The target is operated at a high potential with respect to the filament, typically about 100,000 volts. When the high-speed electrons from the filament strike the target, some of their energy is converted to X-radiation. Most of the energy, however, is converted to heat, and some means of cooling the anode must be provided. Water and oil cooling are commonly used in addition to cooling fins mounted on a copper rod extending from the anode. Some tubes use a motor-driven anode so that electrons do not continually strike the same point on the target surface.

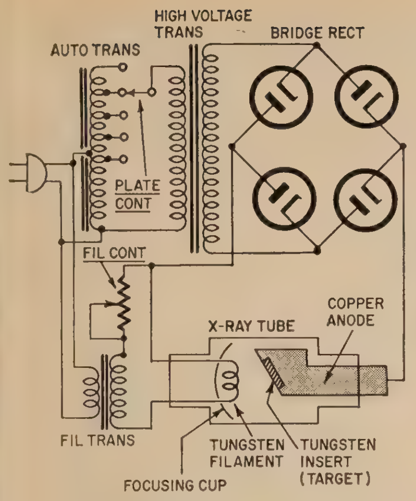
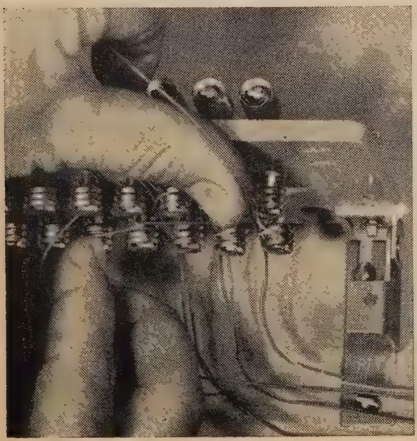


Fig. 29—X-ray circuit consists basically of high-voltage supply for anode of X-ray tube, filament supply and associated controls.

As shown in Fig. 29, the associated circuitry consists basically of a high-voltage supply, a filament supply and controls for varying anode voltage and filament current. At higher values of anode voltage, X-rays of shorter wavelength are produced. These are more penetrating and are known as *hard-X-rays.* Anode voltage is controlled indirectly by varying the input to the primary of the high voltage transformer. A rheostat in the filament circuit permits control of filament temperature and consequently of the quantity of X-rays produced. END

Coil-Spring Connectors

These coil-spring connectors replace binding posts in telephone blocks. When a wire is forced between two turns of the coil, the sharp square edges of the wire cut through the insulation and make a good electrical connection. Developed by Bell Telephone Labs, the connectors are expected to cut connecting time in half as compared with connections made to binding posts.



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ALL-TRANSISTOR MOTOR-CONTROL RELAY

By **HOWARD T. BAILEY**

Using transistor amplifiers to control reversible shaded-pole motors reduces the size and weight of the control unit, and cuts operating costs. Also, a properly designed transistor unit should improve the reliability of the control system. One such unit is described here.

The control-system principle is the same as that of a vacuum-tube amplifier. The direction of rotation is set by the relative phase of the control signal and field current. Speed is controlled by the magnitude of the input signal.

A transistor amplifier for motor control must provide high gain without phase shift and supply enough power to feed the shading coils of the motor being controlled.

The first requirement can be met by suitable circuit design, while the problem of enough power may be overcome by using high-wattage power transistors.

A typical motor-control circuit is shown in the diagram. It uses four p-n-p transistors and provides a maximum stall torque of .05 lb/in for a 0.62-mv input with a Barber-Colman DYAE continuous-duty motor. The input is an ac signal from a bridge circuit that detects physical conditions in terms of voltage differences.

Circuit action

The input signal from the bridge is applied via C1 to V1's base. V1 is a common-emitter amplifier. R1 provides constant emitter-current bias to help stabilize the stage against current changes caused by temperature variations. This resistor is bypassed by C3 for maximum gain. V1's output is fed to V2, another common-emitter amplifier. R2 provides constant emitter-current bias for temperature stabilization, C4 being a bypass capacitor. A small amount of negative feedback is applied to V1's base from the voltage drop across R3 to improve the operating stability, the gain of the first two stages being high. C2 and C5 also supply some negative feedback to reduce harmonic distortion in the first and second stages, respectively.

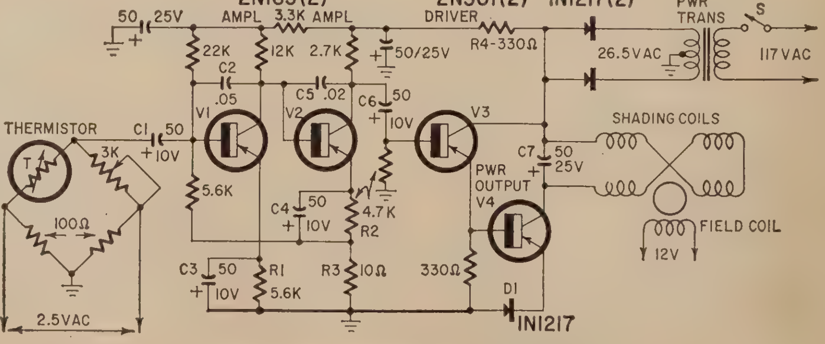
The driver stage, V3, is a power transistor operated as an emitter follower. This stage gives no voltage amplification but provides a large current to drive output stage V4. It also provides correct impedance matching to the output stage. The full negative supply is connected to the collector and the base is biased in a reverse direction by returning it to ground. C6 is a dc blocking capacitor in the feed from V2's collector. The output current from V3's emitter is applied directly to the base of output transistor V4.

The current from V4's collector flows through the shading windings of the reversible motor. A control signal applied to the unit causes an amplified signal voltage to be set up across the shading coils, and the motor then turns in a direction determined by the relative phasing of the signal voltage and the reference voltage in the field winding. The amplitude of the signal voltage decides the speed of the motor in either direction.

Temperature stabilization of V4 is provided by diode D1. This is preferred instead of a resistor in the emitter feed as its stabilizing effect is more constant at various values of emitter current. The larger capacitor, C7, absorbs high-voltage peaks set up across the shading coils at the moment of switching off. Without C7 such peaks could damage the output transistor.

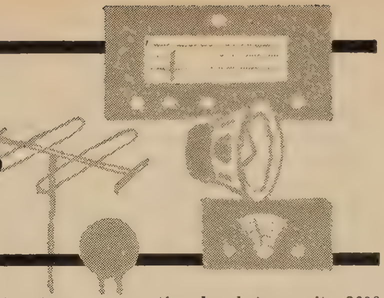
The negative supply for the transistors is obtained by full-wave rectification of a 26.5 center-tapped supply across the secondary of transformer T1.

Many devices can be used as the detecting element of the bridge—temperature-sensitive resistances, light-sensitive cells, humidity-sensitive chemicals, etc. In general, any means of varying a resistance can be used as a detection device if it can be incorporated in a bridge circuit. **END**



Circuit of the transistorized control device.

NEW PRODUCTS



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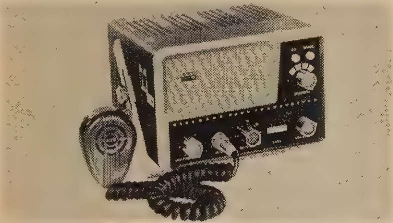

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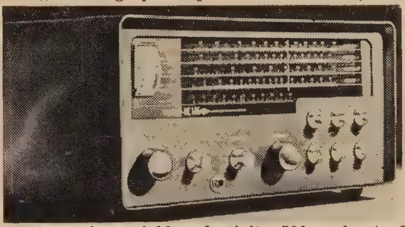
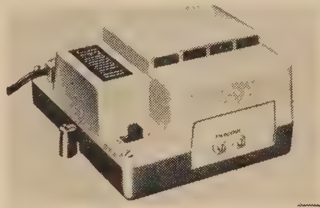


WALKIE-TALKIE, *model CB-901.* 9 transistors. Variable-reluctance mike, 2¼-in. PM speaker, fingertip volume control. Weighs 1 lb. range 6 miles. Powered by 8 penlight cells. Meets class-D specs.—**Sony Corp. of America,** 514 Broadway, New York 12, N. Y.

FM ANTENNA AMPLIFIER, *Range Extender, model FMX.* Doubles primary reception of FM tuners and radios. One-tube unit has 20-db minimum gain over entire FM band. Installs anywhere between antenna and FM tuner or radio; mounted on any flat surface where 117-volt 60-cycle outlet is available. With manufacturer's *MF-2* or *MF-4* multi-set couplers, *FMX* can feed signal to 2, 3 or 4 FM receivers, 6DJ8 frame-grid tube, shut-off switch.—**Jerrold Electronics Corp.,** 15th & Lehigh Ave., Philadelphia 32, Pa.



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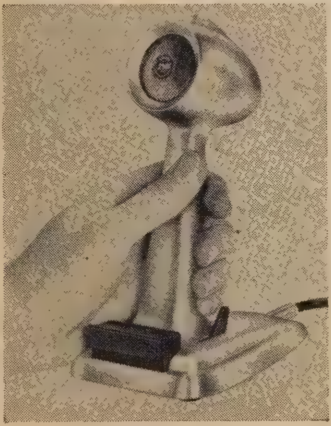

MODEL 254C

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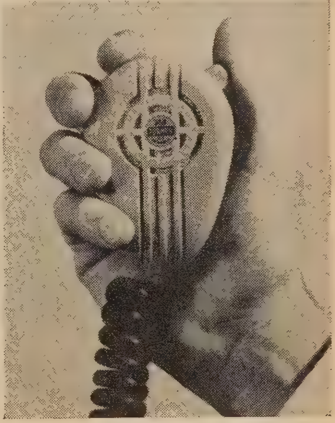

MODEL 350C

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The Turner Combo

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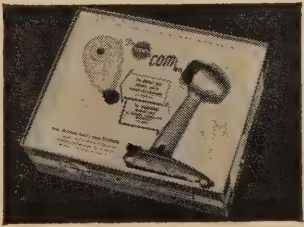


THE TURNER MICROPHONE COMPANY
933 17th St. NE Cedar Rapids, Iowa

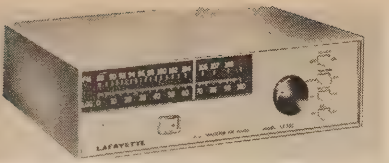
Gentlemen:
Please send me complete information and specifications on the ☐ Turner Mobile Model 350C ☐ the Turner Base Station Model 254C ☐ the Turner Combo.

NAME __________

ADDRESS __________

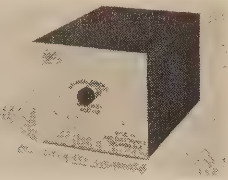
CITY ______ ZONE ______ STATE ______

THE TURNER MICROPHONE COMPANY
933 17th Street NE, Cedar Rapids, Iowa
In Canada: Tri-Tel Associates, Ltd., 81 Sheppard Ave. West, Willowdale, Ontario



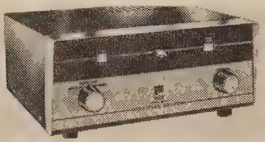
separation 1 mc. Noise level 66 db below 100% modulation. Synchronous-gate separation of channels from composite signal reproduces 20–20,000 cycles ±1 db. Afc, signal-strength meter, interstation muting. 20 transistors, 9 diodes. Consumes 4 watts.—**Lafayette Radio Electronics Corp.**, 111 Jericho Turnpike, Syosset, N. Y.

MULTIPLEX ADAPTER, *ABCO model 650.* Attaches to all discriminator-type FM tuners and radios. Tubes: 2—12AU7, 1—6C4, 2 diodes. Input 1-volt rms approximately; output 2.5 volts rms per channel; power 117 volts ac.



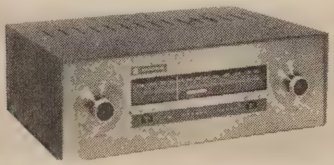
Approximately 20-db separation.—**A B C Electronics**, 440 Boone St., Orlando, Fla.

STEREO MULTIPLEX ADAPTER, *model MX-100.* 28-db separation, 1.5-volt output, less than 1% third harmonic distortion. Response +1 db, 15 cycles to 15 kc. Tube complement: 1—ECC85, 2—12AX7, 1—6X4, 2—1N541 diodes. Dual inputs, left and right stereo outputs. Power



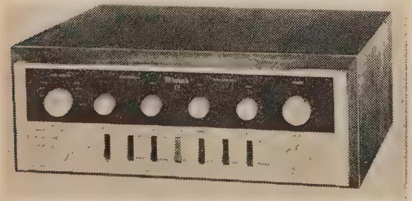
consumption 117 volts, 30 watts. Built-in noise filter, front-panel separation control or maximum separation adjusted at factory.—**PACO, Div. Precision Apparatus Co., Inc.**, 70-31 84th St., Glendale 27, N. Y.

FM STEREO TUNER, *model TP50.* Flat frequency response to 75,000 cycles; sensitivity 0.9 μv, 20-db quieting. Agc maintains ± 0.5-db audio-output level; signal-variation range 10



to 10,000 μv. Built-in tape recording filter. Hum and noise level: —60 db, 100% modulation.—**Bogen-Presto Div., Siegler Corp.**, PO Box 500, Paramus, N. J.

STEREO PREAMP, *model C-11.* 3-dimensional illuminated front panel. Response ±0.5 db, 20–20,000 cycles, distortion less than 0.1% full rated output. 5 high-level stereo inputs for tuners, tape units, auxiliary signal sources and tape monitor. Impedance 250,000 ohms, sensitivity 0.25 volt. 2 phono inputs 2 mv, 47,000 ohms; tape head 2 mv, 1 meg; mike 2.5 mv, 1



meg. Additional mono line for remote amplifier and speaker. Main output 2.5 volts at rated input, tape output 0.25 volt at rated input. 8-position input selector, 7-position mode selector, separate channel controls, stereo balance control, master volume control.—**McIntosh Laboratory, Inc.**, 5 Chambers St., Binghamton, N. Y.

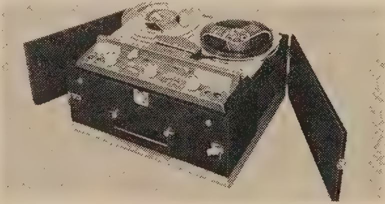
TRANSISTOR STEREO SYSTEM, *Astro.* AM and FM tuners, FM multiplex, dual preamps, dual amplifiers. 55 watts, response 1 db, 20–20,000 cycles. Harmonic distortion less than 1% at 20 watts. Channel separation 30 db. Headphone receptacle, index-locked balance and

tone controls, source selector, instantaneous signal playback. Loudness contour, channel reverse, phase reverse, rumble filter, afc, AM bandwidth adjustment.—**Altec Lansing Corp.**, 1515 S. Manchester Ave., Anaheim, Calif.

FM STEREO TUNER, *Citation III-X.* Built-in multiplex adapter. Front panel single control for mono, stereo and stereo SCA filter to eliminate stray noise in multiplex broadcasting of background music. SCA filter defeat for stereo. Sensitivity 0.65 μv, 20-db quieting. Selectivity: 240-kc bandwidth; 6 db down. Discriminator

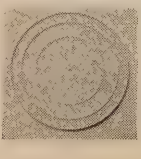
peak-to-peak separation 1 mc. Image rejection 65 db; i.f. rejection 90 db. Response ±0.5 db, 1–52,000 cycles. Distortion unmeasurable at 30% modulation, less than 1% at 100% modulation. Hum 65 db below 100% modulation; output level 2 volts at 100% modulation, adjustable by front-panel control. Adapter: separation —30 db, 10–15,000 cycles; ±½ db, 10–15,000 cycles; harmonic distortion less than 1% at 100% modulation; hum and noise —60 db. Kit or factory-wired.—**Harman Kardon Inc.**, Ames Court, Plainview, N. Y.

4-TRACK TAPE RECORDER, *Statesman Stereo 4, model 350.* Records and plays back stereo. 2 speeds, eight hours recording time on 7-inch reels. Pushbutton controls, automatic tape lifters, constant-speed hysteresis motor, digital tape counter. 2 full-range dynamic mikes, two 4 x 6 oval dynamic speakers, 2 VU meters. Auxiliary inputs and outputs, sound-deflecting baffle wings. Power requirements 85 watts, 110–117 volts ac only, 60 cycles. Tube complement: 2—12AX7, 2—6BMB, 6AR5, SM150C (selenium



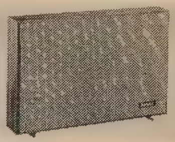
rectifier). Response 50 – 14,000 cycles, 7.5 ips. Flutter and wow 3% at 7.5 ips. Signal-to-noise ratio better than 45 db per channel. Output power 5 watts per channel. Input impedance 500,000 ohms for auxiliary inputs using AM/FM multiplex tuner, stereo record and tape; 50,000 ohms for dynamic mike. High output impedance for external main amplifier connections. External speaker or headphone connections for hooking up to 4- or 8-ohm speakers. Tape, reels, patch cords.—**International Products Co.**, 1289 S. La Brea Ave., Los Angeles 19, Calif.

12-INCH TURNTABLE MAT, *model PC-22,* to protect record grooves, reduce wow and



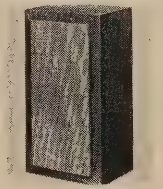
flutter. Replaces worn mats, fits over existing one. 3 ridges provide support for 7-, 10- and 12-in. records.—**Robins Industries Corp.**, 36-27 Prince St., Flushing 56, N. Y.

HI-FI ENCLOSURE, *Petite.* Cone-construction woofer, overhanging voice coil. Woofer matched to tweeter through crossover network



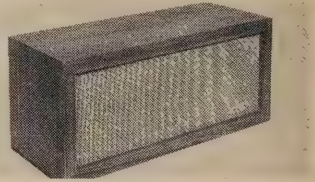
with volume control. Input 8 ohms, power rating 6 watts.—**Argos Products Co.**, 301 Main St., Genoa, Ill.

3-WAY SPEAKER SYSTEM, *model S-4.* 8-in woofer, separate mid-range and high-frequency drivers. Multiple crossover network with



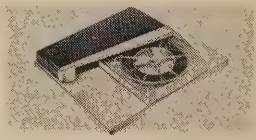
separate controls for mid-range and tweeter drivers.—**H. H. Scott, Inc.**, Dept. P, 111 Powdermill Rd., Maynard, Mass.

BOOKSHELF SPEAKER SYSTEM. 24 x 10 x 9 inches British speaker. For amplifiers 8 to 50 watts, response 45–16,000 cycles. 3-inch hardened tweeter diffusion cone, 8-inch high com-



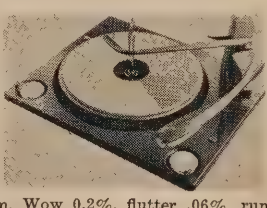
pliance woofer with almost ¾-inch cone displacement.—**Anglo American Acoustics Ltd.**, 129 Maryland Ave., Freeport, N. Y.

AUTOMATIC TAPE DECK, companion to Automatic Tape Cartridge. Instantaneous stop and start; automatic cartridge lock; remote-control operation; adaptable for rack mounting;



heavy-gauge steel construction. Pressure roller drops away from capstan when not in operation to protect roller. Speed accuracy with 4-pole induction motor, +3%, —2% or better. Multi-belt drive system for 3 speeds. 4-pole shaded-pole induction motor dynamically and statically balanced, shock-mounted, less than 40°C heat rise in continuous operation. Wow and flutter 25% or better, maximum average 3¾ cycles.—**Conley Electronics Corp.**, 1527 Lyons St., Evanston, Ill.

AUTOMATIC RECORD CHANGER, *model UA16.* Dynamically balanced motor. Self-lubricating, lifetime bearings, mounted with full rubber suspension. One-piece aluminum die-cast



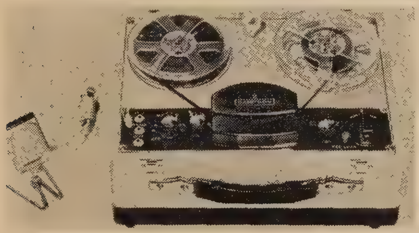
tone arm. Wow 0.2%, flutter .06%, rumble —56 db. 4 speeds, plays all record sizes of same speed intermixed. Concentrically weighted turntable.—**BSR (USA) Ltd.**, 115-10 14th Rd., College Point 56, N. Y.

MINIATURE TAPE RECORDER, *Phono Trix Executive 88-B.* Battery-operated. Immediate playback through mike while connected to

input jack. Used with manufacturer's desk amplifier, 88-B, becomes PA system, records and amplifies simultaneously. Pushbutton-operated, top controls.—**Matthew Stuart & Co., Inc.**, 156 5th Ave., New York 10, N. Y.

PORTABLE TAPE RECORDER, *model TK-40.* 4-track monaural pushbutton unit records and plays back 3 speeds. Equipped for dual sound effects. Built-in permanent dynamic speaker. Input jacks for microphone, radio, phonograph, telephone adapters. Output jacks available for external loudspeaker, remote control, earphones, playback through radio, 8-mm film projectors or connection to second tape recorder. Built-in splicing rule, tape counter, magic-band recording level indicator, flywheel drive and tone and monitoring controls.—**Majestic International Sales, Inc.**, 743 N. La Salle St., Chicago, Ill.

MONAURAL TAPE RECORDER, *model SFC62N.* Automatic 2-speed control, tone control operates on record and playback. Neon-recording level indicator; pause and edit control; separate jacks for mike, external speaker and radio-phono. Safety interlock. Precision braking; wow and flutter less than 0.35%. Patch cord, professional desk stand mike, two 5-in reels, 600 feet of tape. Accommodates up to 7-in reels.—**The Sampson Co., Electronics Div.**, 2244 S. Western Ave., Chicago 8, Ill.



ALL-PURPOSE MICROPHONE, *model D55.* Response 70-15,000 cycles. Two sound entrances at back of diaphragm provide unidirectional polar characteristics for this dynamic mike. Correct positioning of unit controls program feedback, etc., in PA systems. Moving a wire alters impedance from 50 to 40,000 ohms. 11-oz. unit equipped with 18-foot, two-conductor shielded cable. Available in phased, matched pairs.—**American Microphone Mfg. Co. (Div. G. C. Electronics**, 400 S. Wyman St., Rockford, Ill.

TRANSISTORIZED POWER CONVERTER, *Continental 50-191.* Changes 12-volt battery current to 110-volt 60-cycle ac. Capacity 275 watts continuous, 300 watts intermittent. For operating tape recorders, TV sets, sound cameras, amplifiers, test equipment, hand-power tools and

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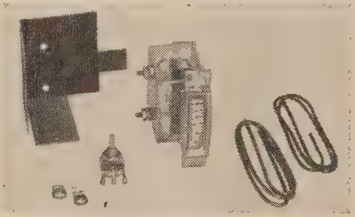

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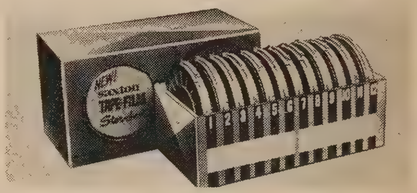
universal type ac–dc motors to ¼ hp. Remote control, cables, battery leads.—**Terado Corp.,** 1060½ Raymond Ave., St. Paul 8, Minn.

INDEXED STORAGE CHEST, for film and recording tape. Holds 12 styrene containers, accommodates all 5- and 7-in recording tape plus 8-mm home movie film. Swivel-twist lock.—**Saxton Products, Inc.,** 4320 Park Ave., Bronx 57, N. Y.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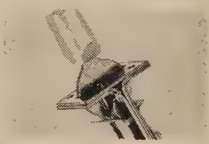
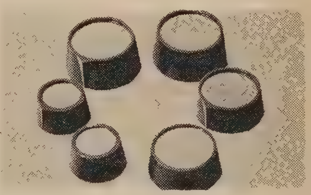
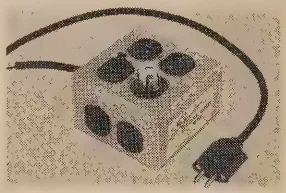
SWITCH KNOBS, contoured top and bottom, tapered sides, for Lev-R and Telever switches. Red, black, milky white.—**Switchcraft, Inc.** 5555 N. Elston Ave., Chicago 30, Ill.



REPLACEMENT KNOB HEADS. 6 types to fit stems currently in stock. Also 21 new stems, assorted lengths, to fit various shafts.—**Colman Electronic Products,** 1017 N. E. 3rd Ave., Amarillo, Tex.



OUTLET BOX, *Safcord, model W-1.* For quick installation of multiple electric outlets. 6 heavy-duty standard receptacles, on–off switch, pilot light. 10 feet heavy-duty appliance cord. Both sides of line fused. 120-volt unit rated at 10 amps, 1,200 watts.—**R. Moranski, Dept. RE-1,** 61 Trudy Lane, Buffalo 25, N.Y.



CHEMICAL SPRAYS. 6-oz aerosol spray cans contain *Super Freeze Mist* for pinpointing bad components through quick cooling. *Spra-Kleen* lubricates and eliminates noise caused by dust and corrosion on switches, relays, and sliding contact devices. *Super Contact Cleaner,* heavy-duty spray with silicone compound, protects all controls.—**GC Electronics, Div. Textron,** 400 S. Wyman St., Rockford, Ill.

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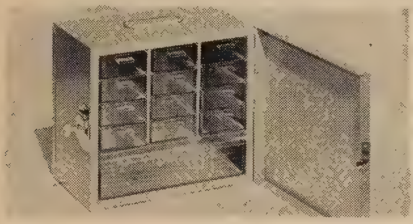
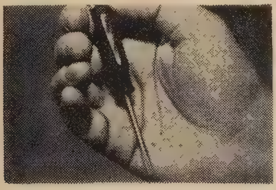
SOLDERING KIT, *model 8250AK*. Includes 250-watt heavy-duty soldering gun with twin spotlights, smoothing tip, cutting tip, wrench, supply of solder. Self-hinged polypropylene case.—**Weller Electric Corp.**, 601 Stones Crossing Rd., Easton, Pa.

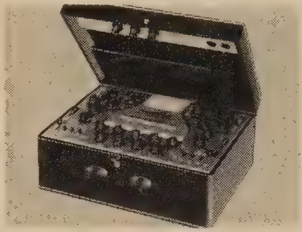
PORTABLE CABINET, *Atlas*. Plastic compartments hold electronic parts for the radio-TV service technician.—**Akro-Mils, Inc.**, 820 E. Market St., Akron 9, Ohio.



MIDGET-SIZE SCREWDRIVER, *cat. no. BR181*. Beryllium-copper, nonmagnetic, nonsparking. For electrical and electronic assembly and service. ⅛ x 2-inch beryllium-copper round blade in plastic handle fitted with pocket clip. Overall length 4¼ inches.—**Xcelite, Inc.**, Orchard Park, N. Y.

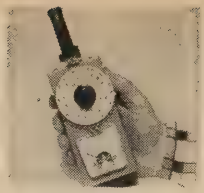


MUTUAL-CONDUCTANCE TUBE TESTER KIT, *model TT-1A*. Built-in adapter for testing compactron, nuvistor, Novar and 10-pin miniature types. Checks G_m and grid current in multi-element tubes; diodes, rectifiers, voltage regulators, low-power thyratrons, electron eye-tubes. Indicates G_m to 24,000 micromhos. Individual selector switches: disconnect switch; built-in, switch-operated calibration circuit. All tube test data on built-in roll chart.—**Heath Co.**, Benton Harbor, Mich.

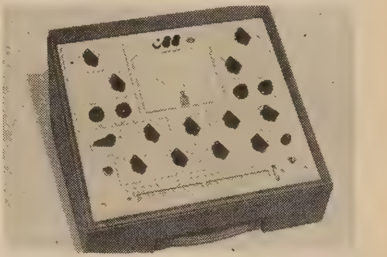


TRANSISTORIZED SIG GEN, *model 36-564*. Signal injection device for af and rf/if. Variable output level 400-cycle audio signal generated. 18-inch leads, insulated alligator clip, thin test probe. 16-oz. 6-volt battery, 2 transistors, on/off switch on control potentiometer.—**GC Electronics, Inc., Div. Textron Electronics, Inc.**, 400 S. Wyman St., Rockford, Ill.

PORTABLE GRID-DIP METER. Fully transistorized. 14-oz. 1-hand operation. Measures resonant frequencies, checks antenna resonance; locates parasitic frequencies as rf detector, absorption wavemeter and sig gen. Epoxy-coated plug-in coils, banana plugs. 5 coils (3.1–180 mc), phone jack, battery. Kit or assembled.—**PEL Electronics**, PO Box 555, Ridgewood, N.J.



BETA TRANSISTOR TESTER, *model 1800*. Tests silicon or germanium transistors, diodes, Zener diodes, accuracy ±3%. Measures ac, dc beta, leakage, other transistor characteristics. Built-in roll chart lists data for beta and leakage tests on more than 1,550 transistors. 7 leakage ranges cover 0–0.05 μa full scale to 0–25 ma full scale. Chopper and high-gain amplifier for leakage current measurement on low-current scales. Instruction manual gives manufacturer's data for I_{CEO}, I_{EBO}, input resistance, output conductance, mutual conductance and collector saturation voltage. Continuously variable V_{CE} and I_C provide tests based on user's special requirements. — **RD Instruments, Div. Hickok Electrical Instrument Co.**, 10514 Dupont Ave., Cleveland 8, Ohio.



If you can't afford a Fisher tuner...

build one!

Introducing the newest Fisher StrataKit: the KM-60 FM-Stereo-Multiplex Wide-Band Tuner. Fisher FM tuners have always been reasonably priced considering their unsurpassed sensitivity and matchless overall design—but, even so, not everyone can afford them. If economics have thus far deterred you from buying the very finest, the new Fisher KM-60 StrataKit solves all your problems in exchange for a few evenings of entertaining and instructive work. It incorporates Fisher FM engineering at its most advanced, including built-in Multiplex and sophisticated wide-band circuitry—yet it costs almost one-third *less* than the nearest equivalent Fisher-built tuner.

This spectacular saving involves absolutely no risk, even if you are 'all thumbs.' The StrataKit method of kit construction has eliminated the difference between the expert technician and a totally unskilled person as far as the *end result* is concerned. You assemble your StrataKit by easy, error-proof stages (strata), *each* stage corresponding to a *particular* page in the Instruction Manual and to a *separate* transparent packet of parts. Major components come already mounted on the chassis, and wires are *pre-cut* for every stage—which means every page!

In the KM-60 StrataKit, the front-end and Multiplex circuits come pre-aligned. The other circuits are aligned by you after assembly. That is accomplished by means of the tuner's laboratory-type d'Arsonval signal-strength meter, which can be switched into each circuit *without soldering*.

This is the world's most sensitive FM tuner kit, requiring only 0.6 microvolts for 20 db quieting! (IHFM-standard sensitivity is 1.8 microvolts.) Capture ratio is an unprecedented 2.5 db; signal-to-noise ratio 70 db. The famous Fisher 'Golden Cascode' RF stage, plus *four* IF stages and two limiters, must take most of the credit for this spectacular performance and for the superb rejection of all spurious signals. Distortion in the audio circuits is virtually non-measurable.

An outstanding feature of the Multiplex section is the exclusive Stereo Beam, the Fisher invention that shows at a glance whether or not an FM station is broadcasting in stereo. It is in operation at all times and is completely independent of the tuning meter. Stereo reception can be improved under unfavorable conditions by means of the special, switchable sub-carrier noise filter, which does not affect the audible frequency range.

Everything considered, the KM-60 is very close to the finest FM tuner that money can buy and by far the finest you can build. Price $169.50.*

The Fisher KX-200 80-watt stereo control amplifier StrataKit, $169.50.*

*Walnut or Mahogany cabinet, $24.95. Metal cabinet $15.95. Prices slightly higher in the Far West.

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. . . and it is lightweight and compact enough to make it ideal for field work, despite the fact that it is in the category of the finest laboratory equipment by performance standards.

Whether you are working with transistorized circuits, hybrid tubes, or are involved in any test, maintenance or design work requiring 0 to 15 volts of d.c. at up to 3 amps, you will be delighted with this new Harmon Power Supply. The full wave filtered output will supply "lab-type" power at continuous current loads and the .1% regulation at inputs varying from 105 to 125 volts A.C. (55 to 65 cycles) insures 100 microsecond recovery time during voltage surges. This compact package weighs but 5¼ pounds and measures 8⅜" x 6⅞" x 5⅜".

SPECIFICATIONS

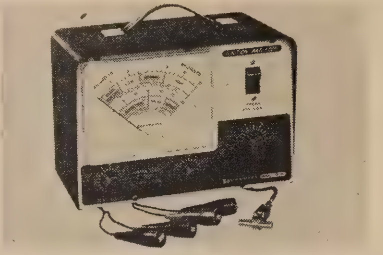
Input	115 volts a.c., 55-65 cps.
Voltage Regulation	±1% at 115 volts. Input voltage may vary from 105 to 125 volts.
Output	0-15 volts d.c., fully regulated, at up to 3 amperes.
Circuitry	Solid-state. 4 power transistors, heat-sink mounted.
Ripple	10 mv. RMS at 50% load current; 30 mv. RMS at full load.
Fusing	All components short-circuit protected.
Recovery Time	Less than 100 microseconds after full load surge.
Voltage Control	Precision Potentiometer

* INTRODUCTORY PRICE 99⁵⁰

Available through your electronic distributor. Write for technical brochure and name of nearest distributor.

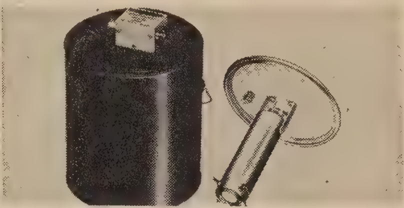
GEORGE HARMON Company Inc.
18141 Napa St. • Di 5-1620 • Northridge, Calif.

IGNITION ANALYZER, *model TE-40.* Locates trouble in coils, spark plugs, points, capacitors. Direct-reading meter. Vtvm section measures to 30,000 volts without circuit drain.

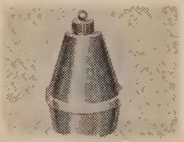


Capacitance clip for shock-proof high-voltage measurements, including surges. Power derived from 12-volt car battery; may be used on all 4-, 6- and 8-cylinder engines. Variable resistance-loading circuit simulates heavy engine load.—**Lafayette Radio Electronics Corp.,** 111 Jericho Turnpike, Syosset, N. Y.

TRANSMITTER DUMMY LOAD, *Cantenna.* Handles power to 1 kw, less than 1.5 vswr to 300 mc. Impedance 50 ohms. Coax input connector for transmitter, phono jack for dc output to vom or vtvm. Oil-cooled temperature-stable resistive element. Oil capacity 1 gal.—**Heath Co.,** Benton Harbor, Mich.



TRANSISTORIZED FISH ATTRACTOR, *Son-r-lure, model 4000.* Sonic-impulse device attracts predatory game fish from as far as 2 miles away to vicinity of user. Use in fresh or salt water.—**H. McCune Co.,** 16255 Ventura Blvd., Encino, Calif.

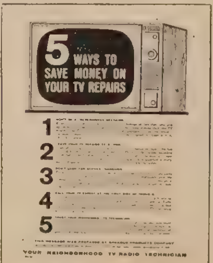


All specifications are from manufacturer's data

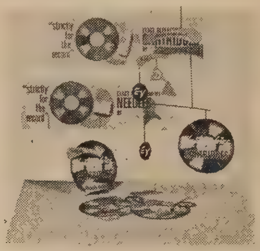
NEW BUSINESS GETTERS — NEW LITERATURE

REPLACEMENT NEEDLE WALL CHART listing replacement needles by cartridge number, illustration of needle replacement, record speed, and needle number in either diamond, jewel or osmium.—**Duotone Co.,** Keyport, N.J.

WINDOW POSTER for service technicians. The 17 x 22-inch poster urges people to stop tinkering and trust TV repairs to the professional. When writing ask for Form Rp-26.—**Sprague Products Co.,** 81 Marshall St., North Adams, Mass.



CARTRIDGE/NEEDLE SALES AIDS include wall charts, cartridge dispensers, storage bins, counter displays, mobiles, banners and plastic tray merchandisers.—**Electro-Voice, Inc.,** Buchanan, Mich.



SERVICE SELECTOR. 40-page catalog describes capacitors, vibrators, rotors, decades, test instruments, other components. Includes illustrations, design features, temperature ranges, material construction, application and price.—**Cornell-Dubilier Electronics Div., Advertising Dept., Federal Pacific Electric Co.,** 50 Paris St., Newark, N. J.

TEST ACCESSORIES—patch cords, cable assemblies, socket savers, test-socket adapters, moldel test plugs—shown in 12-page *Catalog 7-62* is illustrated with many photos, offers complete technical data.—**Pomona Electronics Co., Inc.,** 1500 E. 9th St., Pomona, Calif.

POWER PENTODE 6GB5 presented in 10-page illustrated booklet. Includes photos, diagrams, graphs of cavitrap plate, plus operation data on 6GB5. Request on company letterhead.—**Amperex Electronic Corp., Semiconductor & Special Purpose Tube Div.,** 230 Duffy Ave., Hicksville, N. Y.

AMATEUR BAND RECEIVER NC-155 described in data sheet, with technical information and photos.—**National Radio Co., Dept. RP,** Melrose 76, Mass.

TRANSISTORIZED VOLTAGE REGULATORS, *ICE-254, Application Guide.* Describes design procedures and solution to sample design problems for series, shunt and combination series-shunt regulators.—**Semiconductor & Materials Division, RCA,** Somerville, N.J. 25¢

CLIPS AND INSULATORS detailed in *Catalog No. 250.* Gives sizes, materials, characteristics and capacities of 66 products.—**Mueller Electric Co.,** 1567Y E. 31 St., Cleveland 14, Ohio.

BARRY'S GREEN SHEET, 31-page Feb.–Mar. 1962 Catalog. Features electronic tubes, semiconductors, transformers, chokes, meters, wire, test equipment, etc., for the industrial market.—**Barry Electronics Corp.,** 512 Broadway, New York 12, N. Y.

METAL FASTENERS outlined in *Catalog PL-NL.* Lists complete line of staples, Lock Nails and wire for use with any type of manufacturer's industrial tackers, staplers, etc. Detailed selection data and specifications are included in the catalog.—**Heller Roberts Instruments Corp.,** 6115 Carnegie Ave., Cleveland 3, Ohio.

LEVER TYPE SWITCHES described in 4-page *Catalog No. S-307.* Engineering drawings, specs and operating features, plus colored illustrations.—**Switchcraft, Inc.,** 5555 N. Elston Ave., Chicago 30, Ill.

CLIPS AND INSULATORS offered in 8-page *Catalog No. 250,* with description and illustration of approximately 70 items. Also included are display material and other sales aids. **Mueller Electric Co.,** 1583 E. 31st St., Cleveland 14, Ohio.

Any or all of these catalogs, bulletins, or periodicals are available to you on request direct to the manufacturers, whose addresses are listed at the end of each item. Use your letterhead—do not use postcards. To facilitate identification, mention the issue and page of RADIO-ELECTRONICS on which the item appears. UNLESS OTHERWISE STATED, ALL ITEMS ARE GRATIS. ALL LITERATURE OFFERS ARE VOID AFTER SIX MONTHS.

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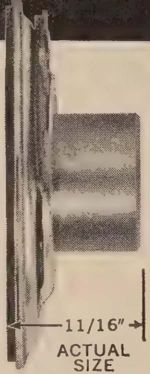

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Here's the solution for replacing speakers in transistor radios. With this complete line of midget speakers (American made with American parts) Utah provides a dependable source for replacements. Wafer-thin baskets, 12 ohm V.C. impedance—for performance equal or better than original speakers.

Model No.	Size	Total Diam.	Basket Depth	Total Depth
SP2T	2" Round	2"	7/32"	11/16"
SP22T	2¼" Round	2¼"	¼"	¾"
SP25A	2½" Square	2½" Square	½"	1 5/16"
SP25T	2½" Round	2 19/32"	⅜"	27/32"
SP27T	2¾" Round	2 25/32"	11/32"	13/16"
SP27A	2¾" Round	2¾"	13/32"	1 3/16"
SP3T	3" Round	3"	11/32"	13/16"

utah
ELECTRONICS CORP.
HUNTINGTON, INDIANA

new PATENTS

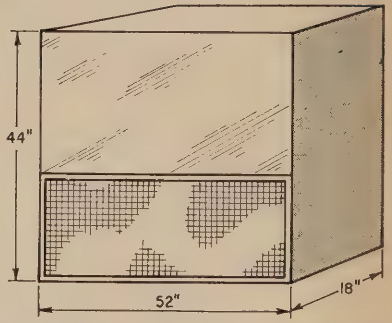
SPEAKER ENCLOSURE

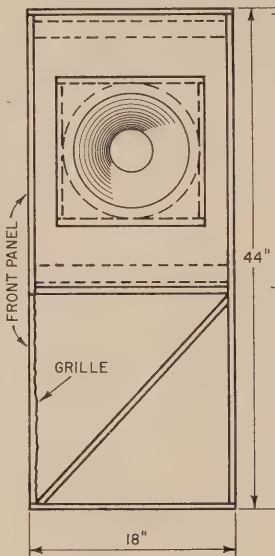
Patent No. 2,969,848

Claude C. Farwell, 6 School St., Groton, Mass.

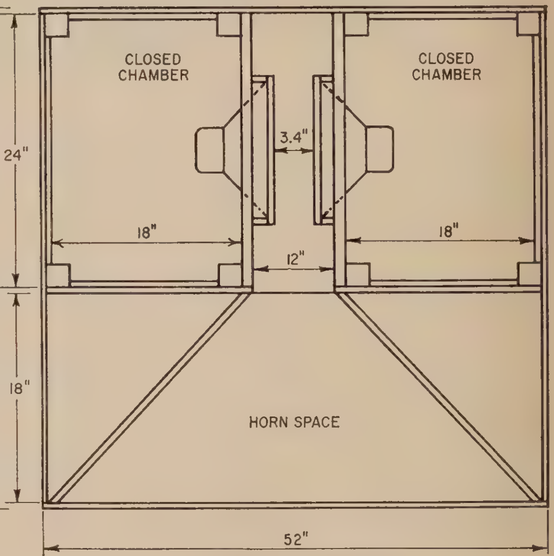
Close coupling between speakers is known to increase fidelity and efficiency. Here is an enclosure designed to couple two 12-inch speakers fed in the same phase.

The space between speakers opens into a "throat" and into a "horn space" which transmits the sound into the room. The chambers are lined with sound-absorbing material, and their joints are reinforced with blocks. The cabinet is made of ¾-inch plywood.





SIDE SECTIONAL VIEW



FRONT SECTIONAL VIEW

NO-WIND CLOCK

Patent No. 2,957,116

Edwin W. Hurd, Leo Goran, Jr., and Charles E. Fischer, Detroit, Mich. (Assigned to Hurd Lock & Mfg. Co., Detroit)

This clock is regulated by a spring and balance wheel. A transistor circuit feeds a pulse of energy to the wheel at regular intervals to compensate for friction loss.

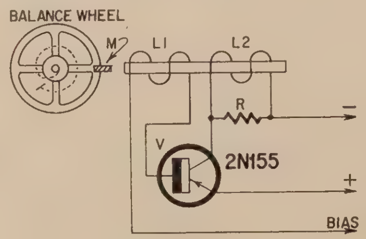


Fig. 1

The transistor circuit (Fig. 1) is energized by dc. Its base is reverse-biased by about 0.3 volt to keep it nonoscillatory. Resistor R damps out any oscillations that may tend to arise.

Magnet M is mounted at the rim of a balance wheel. L1, L2 are wound over a magnetic core and poled for regenerative action. With the core not energized, M is attracted to it. As M passes the core, it generates a negative pulse which is fed to the base of V. The pulse is regenerated until full collector current flows through L2. It energizes the core with polarity that repels M. The collector pulse quickly decays.

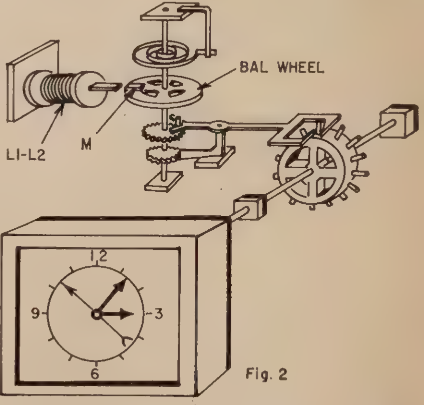


Fig. 2

After the wheel has completed its swing, the spring reverses its motion and again the core attracts M. An instant after M passes the core, it is again repelled by it. Thus the balance wheel oscillates as long as dc is applied to the transistor.

Fig. 2 shows mechanical details of the clock as suggested by the inventor. Also, he describes an unbalanced bridge using temperature-sensitive resistors (not shown) for maintaining a constant dc input to the transistor. END

TECHNICIANS' NEWS

TRI-STATE ELECTION

Camden, N. J.—Members of the Tri-State Council of TV Service Associations elected the following officers:

Tony deFranco, president; Wm. Jordan, vice president; Arnold Zenker, secretary, and Joseph Eberhardt, re-elected treasurer. Carl Welk was appointed publicity director. The Tri-State Council is made up of members of the Allied Electronic Technicians Association of New Jersey, Television Service Dealers Association of Delaware; Television Service Dealers Association of Delaware County, Inc., (Pennsylvania) and the Radio Servicemen's Association of Trenton, N. J.

ACTSA ELECTS

Ashtabula, Ohio—Election and installation of officers was the business at hand at a recent meeting of the Ashtabula County Television Servicemen's Association. The new officers are:

Edward Cimorell, president; Nick Notter, vice president; Jack Stranahan, secretary; Frank Abbott, Treasurer; Joe Horvath, director of NATESA and TESA; Ed Laatu, Carl DeMarco, and Joe Turk, junior vice presidents, and John Campagne, historian and sergeant at arms.

The group's goal for 1962 is to make the ACTSA technician the best technician available.

NEW TECHNICIANS GROUP

Columbia City, Ind.—Technicians from Churubusco, South Whitley and here met at City Hall to organize a new service association. One of the first steps taken by the group was to elect officers. They are: David F. Martin, president; Joe Weaver, vice president; I. C. Ohlwine, secretary, and Marshall Sevits, treasurer.

MULTIPLEX MEETING

Detroit, Mich.—Radio Distributing was packed with 65 TSA members and their technicians for a service meeting on FM multiplex stereo. A smorgasbord dinner was served at 7 pm and the service meeting got underway at 8 and lasted till 10:30.

Zenith field engineer Ed Kob was speaker and proved to be a capable talker and instructor. As a part of his presentation he pointed out that the circuit and tubes had been used before, but in other applications. He also stressed that, while ghosts on TV might be lived with, they were intolerable in FM stereo because they show up as distortion. It was a very profitable evening for those attending.

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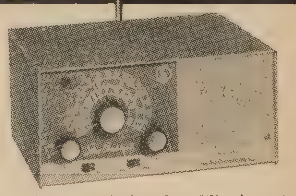
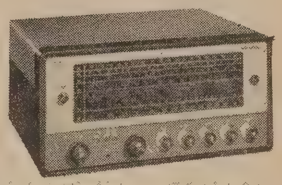
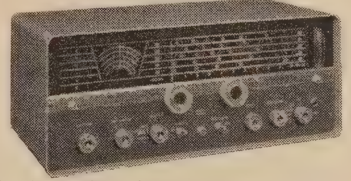


S-119K Sky Buddy Receiver Kit—$39.95. S-119 (factory wired and tested) $49.95. Standard broadcast. Two short wave bands (2-5.5 Mc. and 5.7-16.4 Mc.). Superheterodyne circuit. Transformer-type power supply.

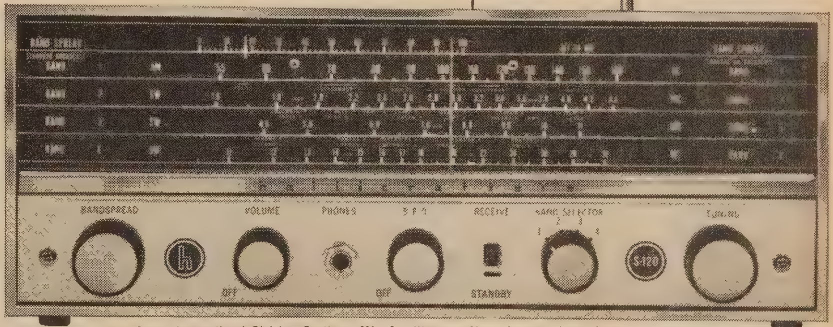


SX-62A Receiver—$395.00. Standard and FM broadcast. Three short wave bands. (1.62 Mc-109 Mc). Excellent audio. Slide rule dial. Single tuning control. Automatic noise limiter. Uses R-48 speaker. ($19.95)



SX-110 Receiver—$169.95. Standard broadcast. Three short wave bands (1550 kc-34 Mc). Slide rule electrical bandspread dial. Built-in "S" meter, antenna trimmer, crystal filter. Uses R-48 speaker ($19.95).

S-120 Receiver—$69.95. Standard broadcast plus three short wave bands (1650 kc-31 Mc). Three-way antenna system. Slide rule electrical bandspread dial. B.F.O./selectivity control.



Export Sales: International Division, Raytheon Mfg. Co., Waltham, Mass. Canada: Gould Sales Co., Montreal, P.Q.

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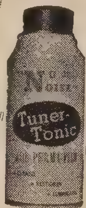

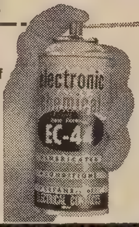

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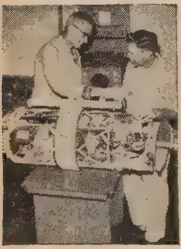

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CSEA BANQUET

Los Angeles, Calif.—The 1962 Annual Banquet of the California State Electronics Association was the setting for a talk on "The Importance of the Independent Service Technician—Today and Tomorrow." The speaker was R. H. Bowden, president of Sencore Inc. His talk revealed his conviction that the future can be bright if the technician will keep abreast of the newest developments in testing methods and concentrate on sound business principles and improved public and customer relations.

INDIANA CIRCUIT

Kokomo—First business was to distribute copies of the association's constitution and bylaws. Next came elections. Ernest H. Golieb is the new president; Joe Martin, vice president; Robert F. Cripe, secretary, and Harold Crume, treasurer.

Ernie Golieb and Joe Martin tied on two successive ballots for president. It was moved and carried that the winner be decided by the toss of a coin, with the runner-up being vice president. Golieb won by a head.

Evansville—RTSA held its 17th Annual Combination Ladies Night and Installation Banquet. Official installation ceremonies were preceded by a family-style banquet dinner. Games and other entertainment followed.

J. Paul Wurtz turned over the president's chair to Charles F. Wilhelm. Gerald Joe Julian is the new vice president; Jerold K. Sweeny, secretary, and Don Wurtz, treasurer.

Logansport—And more election returns—president, Bill Boller; vice president, Frank Pickens; secretary, John E. Hill, and treasurer, Glenn Ogle.

Elkhart—Here too election news is the important item for the month: President, Wayne L. Clem; vice president, Arden Gaerte; secretary, Dean R. Moch, and treasurer, Hubert McAllister.

NO TV SERVICE ON SUNDAY

Kansas City, Mo.—It's against the law to do any TV servicing on Sundays, and TESA is backing it—unanimously. Under the state's Sunday Sales Law (TV service is included), TV service shops are required to close, along with most other retail businesses.

PRICE LIST

Wisconsin—The following price list appeared in the February 1962 issue of *TESA-Wisconsin News*. The prices shown apply to that particular service area and may differ from state to state and even from city to city.

These suggested fees cover diagnosis of trouble, location, installation or repair of component or circuit including mechanical defects. Parts are additional. They are based upon a survey of operational expense of leading service companies, time studies and cost analysis of time required to accomplish the listed service operation on a wide variety of television receivers with operations performed by competent technicians.

Basic Service Fee—Tube Check—Cleaning chassis—Remove and replace—Setup	$ 4.00
1. Ac input circuit	7.25

2.	Audio circuit	15.45
3.	Afc system	18.90
4.	Agc system	19.10
5.	Control: Single unit	6.75
	Dual unit	9.75
6.	Damper circuit	11.60
7.	Deflection yoke and circuit	9.35
8.	Filament circuit	11.65
9.	Focus circuit	9.80
10.	Horizontal oscillator circuit	17.85
11.	Horizontal output circuit	14.55

90-DAY PARTS GUARANTEE

12.	I. F. amplifier circuit	13.75
13.	Picture tube: replacement	9.50
14.	Power supply circuit (hi voltage):	14.20
15.	Power supply circuit (low voltage):	12.45
16.	Power transformer	10.45
17.	Speaker	4.75
18.	Selenium rectifiers	12.25
19.	Sync circuit (vert or horiz):	17.60
20.	Tuner (turret type):	12.50
21.	Tuner (wafer type):	19.50
22.	Tuner cleaning and lubrication (turret type):	4.25
23.	Tuner cleaning and lubrication (wafer type)	6.25
24.	Tuner replacement or removal:	12.50
25.	Vertical oscillator circuit	14.20
26.	Vertical output circuit	12.20
27.	Video circuit	12.55
28.	Retrace blanking circuit	8.10
29.	Printed circuits (concealed type)	Add $8.50 to above price
30.	Clean picture tube (removal)	3.85

Alignment of Tuned Circuits

31.	Video (complete)	12.50
32.	Sound (complete)	8.75
33.	Afc Circuit	7.75
34.	Sound discriminator circuits	4.25
35.	Tuner: local oscillators only	2.00
36.	Uhf tuners	Hourly Rate
	"Local-zone" average service fee	7.00
	Additional TV shop fee—per hour or portion thereof	8.40
	Analysis and location of trouble when estimate is given and set is not repaired	10.00
	IWP (In warranty parts exchange fee) 50c per part—Minimum fee	1.20
	Storage after 30 days: per month or portion thereof	2.00

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"It's probably just a condenser."—Freely translated means—I've just spent $14.00 on tubes and now the thing won't work at all.

"How much do you charge to replace a fuse?"—I was looking for a loose connection when something started smoking.

"I just had the set overhauled."—A friend put in some tubes last month.

"He didn't get it adjusted just right."—The antenna blew down last night.

"Can you just drop it off? I only live around the corner."—We live in a fourth-floor walkup. — *TSA Service News* END

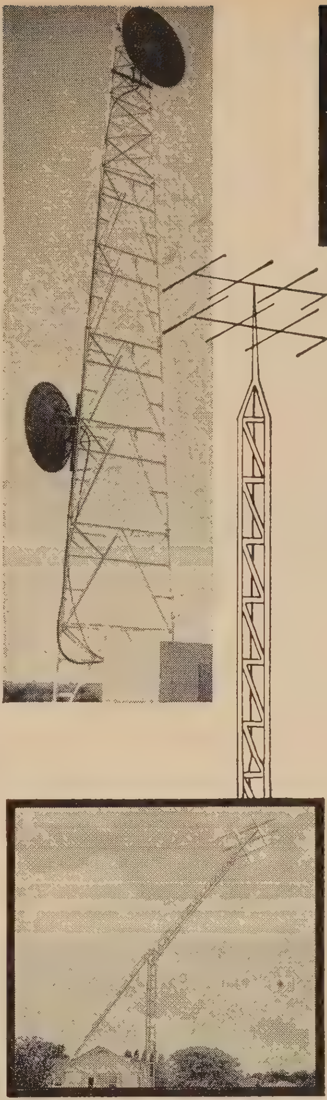
◆

CORRECTIONS

On page 51 of the March issue, the Amperex tube using Cavitrap construction was erroneously designated as the 6BG5 in the caption. The tube, as the photo indicates, is a 6GB5. We thank Mr. George C. Loud, of Eastport, Me., for calling this to our attention.

There is an error in the heater circuit of the multiplex adapter on page 31 of the December 1961 issue. The heater pins of the 12AU7's are numbered 3, 4 and 9. The correct pin connections for the heaters are 4, 5 and 9.

We thank Mr. Robert Volino of Brooklyn, N. Y., for this correction.



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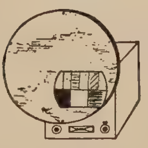

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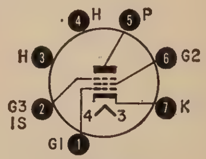
NEW TUBES and SEMI-CONDUCTORS

NEW ITEMS ARE NOT AS NUMEROUS THIS month, but interesting just the same. There are a couple of sharp-cutoff pentodes for FM limiter and i.f. amplifiers; a solid-state negative resistance element; a Novar type TV damper; a subminiature voltage regulator; a group of "universal" picture tube replacements, and a triode nuvistor.

6HS6, 19HS6

Two 7-pin miniature sharp-cutoff pentodes for use in i.f. amplifier and limiter stages of FM receivers. They have extremely high transconductance (9,500 μmhos) and extremely low capacitance between grid 1 and the plate (.006 μμf). Both also feature a "dark heater" which functions efficiently at operating temperatures 350°K below those of conventional heaters. Except for their heater ratings the two tubes are identical.



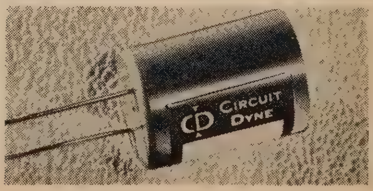
IS=INTERNAL SHIELD
6HS6,19HS6

Characteristics of these RCA tubes when used as class-A1 amplifiers:

V_{HTR} (6HS6)	6.3
(19HS6)	18.9
I_{HTR} (6HS6) (ma)	450
(19HS6) (ma)	150
V_P (supply)	300
V_{G2} (supply)	300
V_{G1} (pos bias value)	0
(neg bias value)	50
P_P (watts)	3
P_{G2} (input) (watts) (for V_{G2} to 150)	1

Solid-state negistor

This semiconductor device is capable of operating as a negative-resistance element. It can be used as a switch, bilateral amplifier, or loss corrector in wave filters. It can also be used in mul-

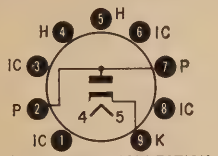


tivibrators, switching circuits and linear amplifiers to reduce cost and complexity and improve overall operation.

A 2-terminal device, the Circuit-Dyne built Negistor is available in resistance values from 10,000 to 100,000 ohms in 5% increments. Resistance tolerances—2%, 5% or 10%—may be specified. The units are epoxy encapsulated and have either coaxial or single-ended leads.

6DW4

This Novar tube is a half-wave vacuum rectifier designed for damper service in horizontal-deflection circuits of color and block-and-white TV sets.



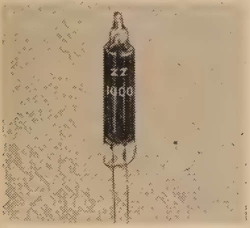
IC=INTERNAL CONNECTION
6DW4

Maximum ratings of the RCA 6DW4 in TV damper service are:

P_{PIV}	4,500
I_P (peak ma)	1,300
I_P (dc ma)	210
P_P (watts)	6.5
V_{H-K} (htr neg with respect to cath)	4,500
(htr pos with respect to cath)	300

8228/ZZ 1000

Subminiature voltage reference tube designed to be the most stable device now available. It has a temperature coefficient of 3 mv/C° (.004%/C°) over a temperature range of −55 to 70° C. Its nominal reference voltage is 82 at an average current of 2 ma. The tube's variation in regulating voltage is less than 100 mv, due to its semi-hollow cathode and it is guaranteed for 30,000 hours of use. The Amperex 8228/ZZ 1000 is 1.2 inches long and ¼ inch in diameter. It has leads which can be soldered into the circuit.



"Universal" Picture Tubes

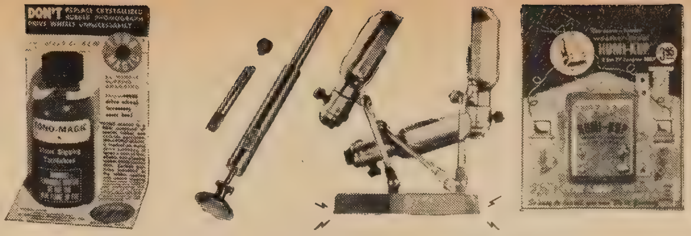
RCA has announced 4 "universal" type picture tubes that will replace 33 existing types. The 4 tubes are said to take care of one out of two picture tube replacements handled by the service technician today.

The 21CMP4-A replaces:

21ALP4 21ALP4-A 21ALP4-B
21ANP4 21ANP4-A 21ATP4
21ATP4-A 21ATP4-B 21BAP4
21BNP4 21BTP4 21CBP4
21CBP4-A 21CBP4-B 21CMP4
21CVP4 21CWP4 21DNP4
21FLP4

The 21AMP4-A replaces:

21ACP4 21ACP4-A 21AMP4
21AMP4-A 21AQP4 21AQP4-A
21BSP4 21CUP4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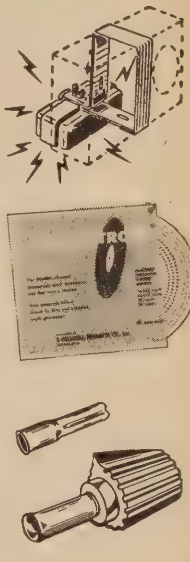

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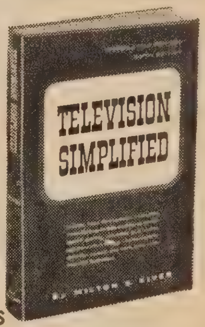

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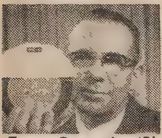

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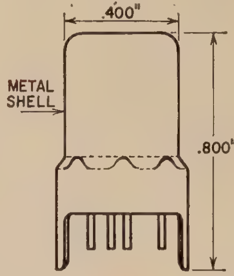

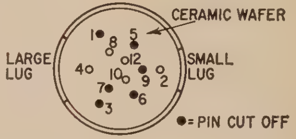

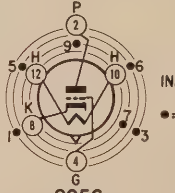
P
2
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G
INDEX = LARGE LUG
● = PIN HAS INTERNAL CONNECTION & IS CUT OFF CLOSE TO CERAMIC WAFER – DO NOT USE

8056

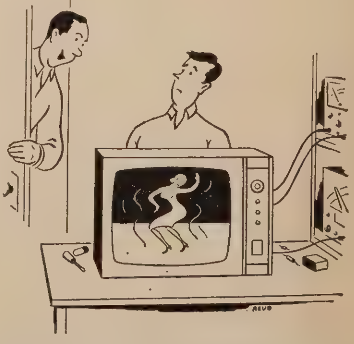
Maximum industrial service ratings for the RCA 8056 are:

V_P	50
V_G (neg bias value)	55
(peak pos value)	2
P_P (watts)	0.45
I_G (ma)	2
I_K (ma)	15

Typical operating characteristics:

V_P (supply)	12	24
V_G (supply)	0	0.7
R_G (k ohms)	33	—
μ	12.5	12.5
R_P (approx k ohms)	1.56	1.56
GM (μmhos)	8,000	8,000
I_P (ma)	5.8	10

END



"Forget the 120-cycle ripple, Sam. She's doing the twist."

Technotes

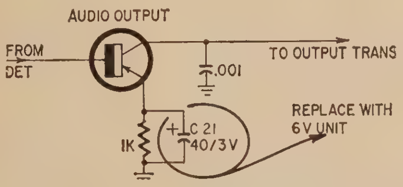
SHIFTING CONVERGENCE

When a color TV receiver is first turned on, the alignment of the gun structure of the picture tube may change slightly because of heating. The normal effect of this heating will vary the static convergence of the receiver, unless some allowance is made for the warmup period. Therefore, it is wise to let the set warm up for about 15 minutes before you converge it. In this way, when the customer turns his set on, instead of it drifting out of convergence, it will drift into convergence.—*RCA Television Service Tips.*

REGENCY TR-1

The set came in with severe audio distortion. We connected a high-impedance headset across the volume control. Sound was satisfactory here. Then we clipped the headset across the base of the audio output transistor to battery positive. Some slight distortion was noted here.

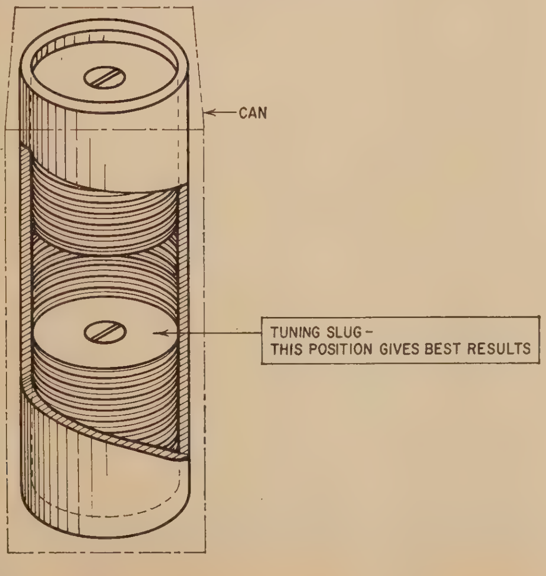
Components in the audio output stage were resistance-checked next. No off-value units were spotted. Voltage tests followed and revealed nearly zero voltage on the emitter.



When capacitor C21 (40 μf at 3 volts) was clipped, voltage on the emitter increased. We replaced the unit with a 6-volt capacitor and had no further trouble.—*Chester S. Lawrence*

HEATH CB TRANSCEIVER

Noting a decided drop in receiver gain when switching from crystal to variable tuning in a Heath GW-10 on the bench, I mistakenly thought the 6C4 oscillator tube was weak. Further troubleshooting turned up an interesting kink. There are two positions of the slug in the oscillator coil which allow tracking of the 22 channels. However, with the adjustment in the lowest position (closest to the chassis),



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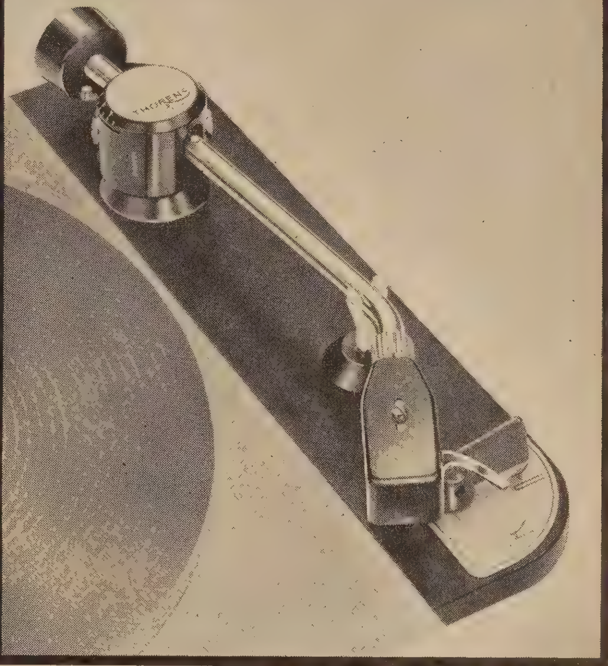
BTD-12S Tone Arm



Here's the *first* 12″ tone arm to match the wealth of features made available on the now famous Thorens "TD" turntables!

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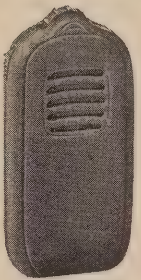

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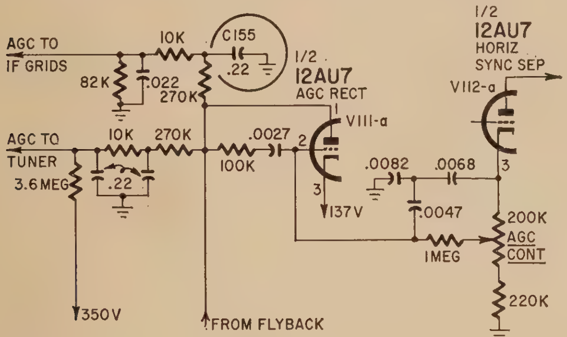
the injection signal from the variable oscillator is much stronger than when it is set closer to the top. This results in a 50% or better gain in reception, raising the level of the variable receiver to that of the lock-in. Subsequently I have run across a relatively large number of GW-10's with this same complaint. Screwing this slug into the lower position cured every one.

Another suggestion while on the subject of alignment. An ordinary signal generator will not give a precise enough alignment of the 455-kc if strip. It is best to use the signal from an accurately calibrated source, such as the Lampkin frequency meter. Using an attenuated signal from another CB transmitter is an alternate but less reliable method.—*Charles B. Randall*

RCA 21D305

The complaint was intermittent black horizontal bars. The sync would lose control or the picture would pull whenever the bars appeared. The trouble was located by a long process of shunting suspected capacitors with known good units. This showed that agc capacitor C155 (0.22 μf) was intermittent. A quick replacement was the cure.—*Chester S. Lawrence*



POWER SUPPLIES FOR TRANSISTOR DEVICES

Commercial power supplies often use a resistance to drop the voltage for the lower output ranges. The low-voltage taps may not be bypassed enough to allow the ac signal to return to chassis. When this kind of supply is used to power a transistor set, audio distortion may arise which is not caused by a circuit fault.

When operating from a low-voltage tap on such a test supply, shunt the output to the radio with a capacitor. Use a 25-μf unit rated at a greater voltage than delivered by the power unit.—*Joe Shane*

AUTOMATIC SEARCH TUNER STALLING

Automatic signal-searching tuners in car radios sometimes stop for no apparent reason when they reach the low end of the band. The actuator bar has to be pushed again to restart it.

When this happens, try the search with the antenna pushed down. If it does not stop now, the search mechanism is OK. Do not alter the sensitivity of the search unit. The problem is caused by the if acting as a station signal at high settings of the sensitivity control in strong station areas. A touch up of the i.f. will usually fix things up; the i.f. may be tuned a trifle too broad.—*Mark Sturgeon* END

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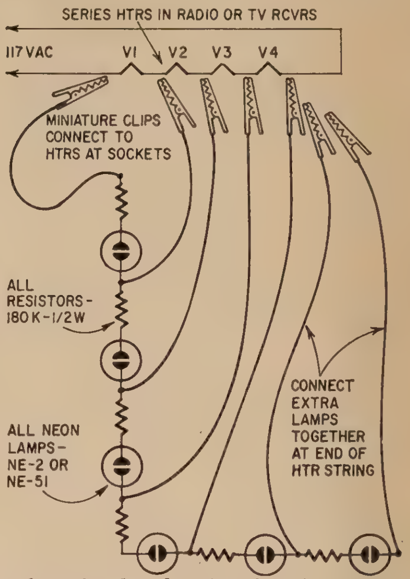
An intermittent heater in a series-string circuit can be a real time waster if the defective heater stays open for only a few seconds, as sometimes happens. The foolproof tester in the diagram can be made up for about $1 or so. It consists of a number (any number) of neon lamps with series-limiting resistors—one for each heater in the set. Miniature clips connect to the junction between tube heaters in the same series sequence as the tubes. Connect unused clips across corresponding unused lamps if you have more lamps than tubes.

Check operation by removing the tubes from the radio, one by one, to see that each neon lamp lights when its corresponding tube is removed. When they are OK, their low resistance across the individual lamps prevents any lamp from lighting. When the defective heater opens, the lamp across it receives the full line voltage and lights up.

Another way to tackle this problem is to make up the tester for use independent of the radio. Mount tube sockets in the chassis with the heaters connected across the neon lamps. A seven- and nine-pin miniature and an octal socket in parallel at each lamp position will take care of nearly all tubes. The 117-volt ac line is connected across the entire string. Now the tubes are removed from the radio and plugged into the sockets, and an inexpensive spst slide switch across each position



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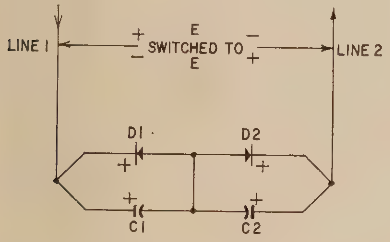
We occasionally need a nonpolarized capacitor with fairly high voltage and capacitance ratings for a circuit where voltage polarity is reversible. When the required capacitor is unavailable or takes too much space, this trick works nicely in many applications. The space required is a fraction of that needed for a nonpolarized component.

Take two ordinary electrolytics with the required voltage and capacitance ratings. Connect them back to back and shunt each with a rectifier diode as shown. When line 1 is positive, D1 blocks while D2 conducts to short out C2. When line 2 is positive, D2 blocks and D1 conducts, thus leaving only C2 in the circuit.



The piv rating of the diodes must be higher than the maximum working voltage. Their current ratings must be higher than the surge current if sudden polarity reversals are expected.—*John H. Hughes, Jr.*

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Occasionally a service technician or experimenter requires a voltage higher than his bench supply delivers. This simple circuit modification, taken from *The Radio Constructor* (London, England), shows how a simple dpdt switch can be added to double a typical supply's output voltage. Figs. 1 and 2 show modifications for semiconductor and vacuum-tube rectifier, respectively.

When the switch is in the NORMAL position, the power supply uses conventional full-wave rectification and delivers a dc voltage equal to around half the transformer's rms secondary voltage. In the HIGH position, the circuit is converted to a half-wave rectifier delivering twice the voltage at *half* the rated current.

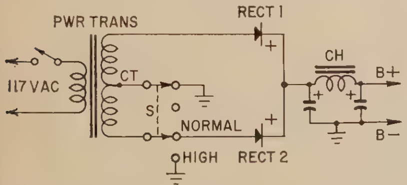

Fig. 1

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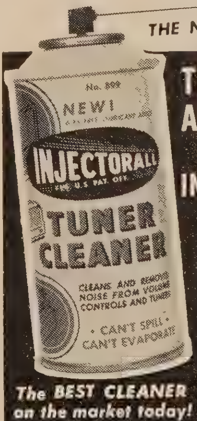
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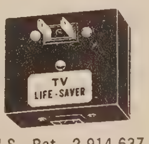

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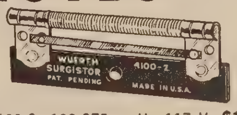

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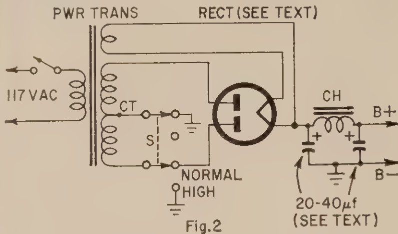

Fig.2

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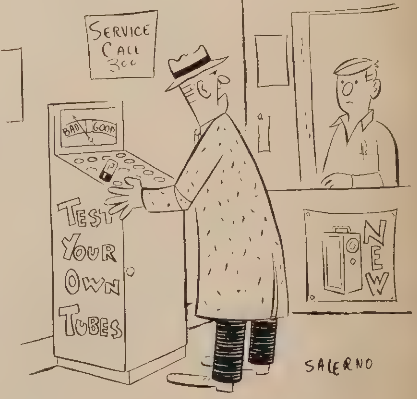

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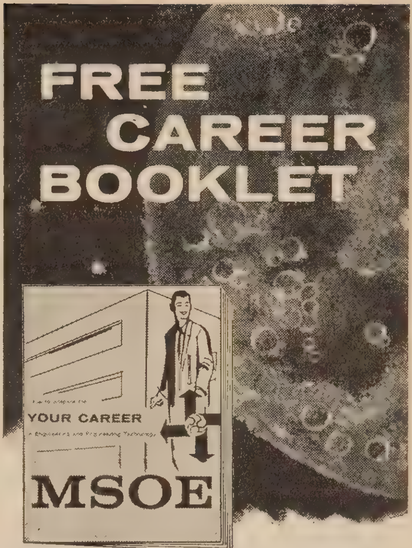

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FOLDED DIPOLES LAST LONGER

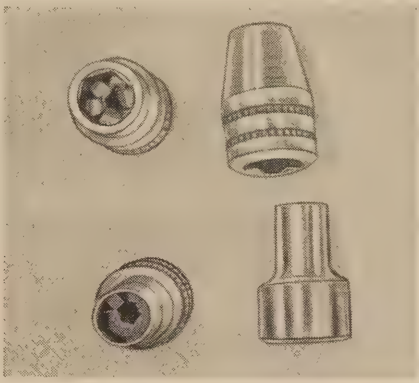
When folded dipole antennas fashioned from 300-ohm ribbon line break from flexing and wind vibration, eliminate the trouble by suspending the antenna from a messenger cable.

Measure a length of nonmetallic core plastic clothesline about two feet longer than the antenna. Fasten it at a convenient height under slight tension and attach the antenna to this line every few feet with plastic insulating tape.

Also, tape the lead-in cable to another length of clothesline tied to the center of the antenna supporting line, then tie the clothesline to the insulators on the supporting halyards and haul it up. Such rigging makes for minimum maintenance and antenna failure.—*Harry J. Miller*

THIN-WALL SOCKET WRENCHES

The inexpensive variety of socket wrench sold by auto supply and mail-order houses can be easily ground or filed down to the thin-walled type often needed for meter repairs where nuts are recessed. If a power grinder and an electric drill are available, the job is that much easier. Chucked in an electric drill or drill press, a final polish can be applied that is better than the original finish on the sockets.—*E. C. Carlson*



TESTING SELENIUM RECTIFIERS

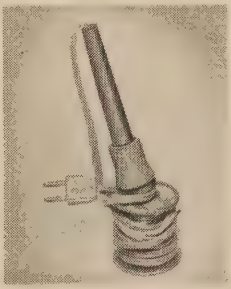
Set your tube checker for a 35Z5 and connect test leads between socket pin 8 (cathode) to the positive terminal of the rectifier and from socket pin 5 (plate) to the negative terminal of the rectifier. Then continue checking as if testing a 35Z5 for emission. If the meter indicates anything other than good, the rectifier should be replaced.—*W. A. Auiler*

CUTTING RUBBER GASKETS

Using a razor blade to cut a rubber gasket for an appliance by following around a templet of the gasket often turns out a gasket that has jagged or distorted edges. We avoid this by cutting a slot in the copper tip of a soldering iron, inserting the razor blade in the slot and locking it with set-screws tapped into the tip. Then, by maintaining a steady heat on the razor blade, it makes the cleanest kind of cut.—*H. Josephs*

HOT-PENCIL HINT

You can store a hot soldering pencil in your tool kit without danger of fire by putting the pencil in a spool of solder as shown. Remember this handy time-saving hint next time you are out on a service call.—*Scott Mack* END



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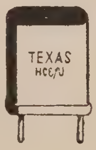

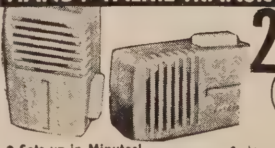

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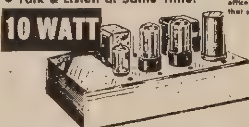

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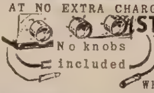

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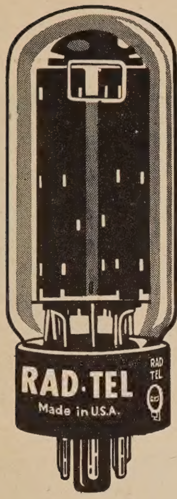

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	7S7	1.01
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	8AW8	.93
	8BQ5	.60
	8CG7	.62
	8CM7	.68
	8CN7	.97
	8CS7	.74
	8CX8	.93
	8EB8	.94
	8SN7	.66
	9CL8	.79
	11CY7	.75
	12A4	.60
	12AB5	.55
	12AC6	.49
	12AD6	.57
	12AE6	.43
	12AE7	.94
	12AF3	.73
	12AF6	.49
	12AJ6	.46
	12AL5	.45
	12AL8	.95
	12AQ5	.60
	12AT6	.43
	12AT7	.76
	12AU6	.51
	12AU7	.60
	12AV6	.41
	12AV7	.75
	12AX4	.67
	12AX7	.63
	12AY7	1.44
	12AZ7	.86
	12B4	.63
	12BA7	.84
	12BD6	.50
	12BE6	.53
	12BF6	.44
	12BH7	.77
	12BK5	1.00
	12BL6	.56
	12BQ6	1.06
	12BR7	.74
	12BV7	.78
	12BY7	.77
	12BZ7	.75
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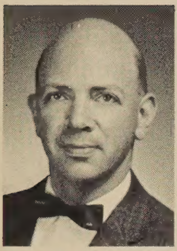

JULIAN D. HIRSCH
of Hirsch-Houck
Laboratories

Summing up his report for HI-FI STEREO REVIEW, Julian D. Hirsch wrote: *"In my opinion, the UNIVERSITY CLASSIC MARK II . . . is one of a limited group of speakers to which I would give an unqualified topnotch rating."*

"Despite the popularity of bookshelf-size speaker systems, the big speaker system is far from extinct. There is still a great deal to be said for the sound quality of a really good large speaker system, one of which is University's new Classic Mark II.

In operation, the Classic Mark II handles low frequencies up to 150 cps through a 15-inch high-compliance woofer that is installed in a ducted-port cabinet. The bulk of musical program content, however, is handled by an 8-inch mid-range speaker, which covers from 150 to 3,000 cps. Above 3,000 cps, a Sphericon super tweeter takes over.

The measured indoor frequency response of the Classic Mark II was remarkably uniform. As a rule, such response curves are so far from flat that I do not attempt to correct them for the slight irregularities of the microphone's response. However, the measurements for the Classic Mark II prompted me to plot the microphone response also. This further emphasizes the uniformity of the system's frequency response. A 5-db increase in the setting of the tweeter-level control would probably have brought the range above 3,000 cps into nearly exact conformity with the microphone-calibration curve.

The low-frequency distortion of the woofer, even at a 10-watt input level, was very low, and it actually decreased at 20 cps, where the output was beginning to rise . . . Any good amplifier of 10 watts rating or better should be able to drive it satisfactorily.

In listening tests, the Classic Mark II sounded very clean . . . there was an undercurrent of bass, more often felt than heard, that was completely lacking in some other quite good speaker systems that I compared to the Classic Mark II. The speaker sounded at its best (to my ears) at moderate listening levels. At high levels the bass tended to be overpowering. A different listening room, of course, could easily alter this situation completely. Over-all, the sound was beautifully balanced, with wide dispersion and a feeling of exceptional ease. There was never a hint that three separate speakers were operating; the sound seemed to emanate from a large, unified source.

In my opinion the University Classic Mark II justifies the substantial claims that its manufacturer has made for it. It is one of a limited group of speakers to which I would give an unqualified topnotch rating. Anyone who is in a position to consider a system of its size and price would be well advised to hear it. The price of the system is $295.00."

WRITE TODAY FOR THE COMPLETE JULIAN HIRSCH HI-FI STEREO REVIEW REPORT on the new CLASSIC, as well as the documented CLASSIC brochure and "Informal Guide to Component Stereo High Fidelity." Simply write: Desk P-4, University Loudspeakers, 80 S. Kensico Ave., White Plains, New York.

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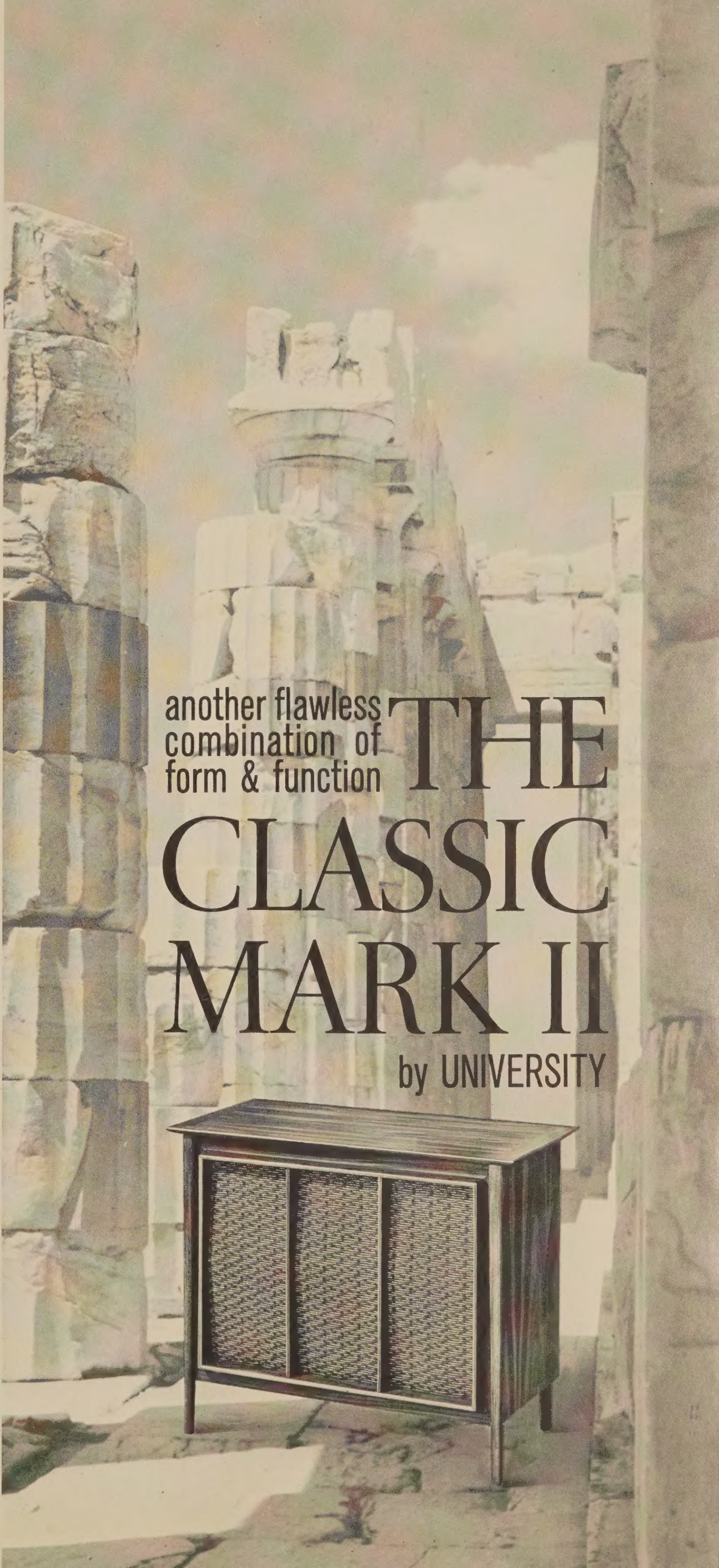

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